

Problem 1:

The attenuation law is given by:

$$I(x) = I_0 e^{-\mu x}$$

This function is most sensitive to changes in μ where its derivative:

$$\frac{\partial}{\partial \mu} I(x) = I_0 (-x) e^{-\mu x} \text{ is steepest or}$$

has the highest value.

The value of x where this derivative has its maximum can be found according to standard analysis by calculating the first derivative and setting it equal zero:

$$\begin{aligned} \frac{\partial}{\partial x} \frac{\partial}{\partial \mu} I(x) &= \frac{\partial}{\partial x} I_0 (-x) e^{-\mu x} \\ &= -I_0 e^{-\mu x} + I_0 x \mu e^{-\mu x} \end{aligned}$$

This expression equals zero if:

$$I_0 e^{-\mu x} = I_0 x \mu e^{-\mu x}$$

This is equivalent to

$$\boxed{\mu x = 1} \quad \therefore$$

Problem 2:

The mass of ^{241}Am is simply obtained by ⁽²⁾ dividing its activity by the specific activity S of ^{241}Am . The specific activity of a radionuclide is the activity per gram mass of the radionuclide. As 1g of a nuclide ^AX contains $\frac{6.022 \times 10^{23}}{A}$ atoms and as

$A(t) = \lambda \cdot N(t)$, the specific activity can be calculated from the half-life by:

$$\begin{aligned} S &= \lambda \cdot N(t) / 1\text{g} \\ &= \frac{\ln 2}{T_{1/2}} \times \frac{6.022 \times 10^{23}}{A} / 1\text{g} \\ &= \frac{1}{A} \times \frac{1}{T_{1/2}} \times 4.175 \times 10^{23} / 1\text{g} \end{aligned}$$

with the half-life $T_{1/2} = 432.2\text{a}$ of ^{241}Am , we obtain

$S \approx 1.3 \times 10^{11} \frac{\text{Bq}}{\text{g}}$, and the mass m of ^{241}Am turns out to be $m = \frac{A}{S} = \frac{30\text{kBq}}{S}$

$$\Rightarrow \boxed{m \approx 0.23\mu\text{g}} \therefore$$

Problem 3:

- The number of tracer particles that are injected as an instantaneous pulse @ point A (see figure on slide 6 of lecture week 186/~~186/~~) and @ $t=0$ is denoted N_T ③
- And we assume that $dN(t)$ is the number of tracer particles that pass through the point B (the exit of the system, where the detector is located) within the time interval from t to $t+dt$ after injection.
- The time t corresponds to the transit time of the particles between A and B.
- As not all particles will have identical transit times, the function $\frac{dN(t)}{dt}$ will vary as a function of t and describes the distribution of the transit times.
- If we divide (or normalize) $\frac{dN(t)}{dt}$ by N_T

we obtain the quantity

$$E(t) = \frac{dN(t)/dt}{N_T}$$

and $E(t) dt$ then corresponds to the probability that a tracer particle will have a residence time between t and $t+dt$.

- As \underline{t} is also the residence time that the $dN(t)$ ⁽⁴⁾ tracer particles have spent in the system, the response $E(t)$ @ point B forms a probability distribution known as the residence time distribution (RTD). The radiotracer concentration $C(t)$ measured by the detector is related to $dN(t)$

by:
$$\boxed{dN(t) = C(t)dV = C(t)Q dt} \quad (1)$$

Here dV is the volume of liquid flowing past B in the time interval between \underline{t} and $\underline{t+dt}$, and Q is the flow rate (assumed to be constant). The fraction of the tracer particles passing B between \underline{t} and $\underline{t+dt}$ can be written as $\underline{E(t)dt}$ or $\frac{dN(t)}{N_T}$ (see above/earlier).

Now, inserting Eq. (1) for $dN(t)$, we get:

$$E(t)dt = \frac{dN(t)}{N_T} = C(t)Q dt / N_T \quad (2)$$

or, after "dividing by dt ":

$$\boxed{RTD = E(t) = C(t)Q / N_T = \text{const.} \times C(t)} \quad (3)$$

In summary: the detector response @ B to an instantaneous injection @ A is the RTD of the tracer particles in the system, provided that:

- the tracer is injected as an instantaneous pulse, and
- the flow rate Q through the system is constant.

Problem 4:

As we neglect nuclear decay of the ⁽⁵⁾ tracer in the system, all N_T tracer particles injected must pass by the detector @ point B (i.e., mass balance is given, no particle is lost):

$$N_T = \int_0^{\infty} dN(t) = Q \int_0^{\infty} c(t) dt \quad (4)$$

where we have used Eq. (1); see Problem 3! Also, no activity ($A = \lambda \cdot N$) is lost, and we may rewrite Eq. (4) as:

$$A_T = \int_0^{\infty} dA(t) = Q \int_0^{\infty} C_A(t) dt \quad (5)$$

with the activity concentration $C_A(t) = \lambda C(t)$
(in units of Bq/l)

In the total sample method the sample is taken @ a constant rate q (in units of liter/second) for a time ΔT which includes the whole pulse. Again, due to mass (or better activity) balance, we have:

$$\int_0^{\infty} C_A(t) dt = c \Delta T = \frac{a}{q} \quad (6)$$

where c (in units of Bq/liter) is the average concentration of tracer in the total sample and a (in Bq) is the corresponding activity.

Substituting Eq. (6) in Eq. (5) gives:

(2)

$$Q = q A_T / a \therefore$$

In the total count method the registered count rate is proportional to the radioisotope concentration seen by the detector (immersed in the liquid or located externally). Therefore, the # of total counts N recorded (after correction for background) is proportional to the integral $\int_0^{\infty} C_A(t) dt$.

If we denote the proportionality (or calibration) factor by F , we have:

$$N = F \int_0^{\infty} C_A(t) dt$$

Combining this result with Eq. (5) gives

$$Q = A_T F / N \therefore$$

Problem 5:

In a rapidly stirred tank of volume V , an injected pulse of radiotracer will be instantaneously dispersed uniformly through the liquid in the tank.

Thus, the concentration will rapidly adopt the value:

$$C_0 = A_T / V, \text{ where}$$

A_T is the activity of the injected tracer. Assuming a constant flow rate through the tank, the change dC in the tracer concentration between t and $t+dt$ is given by the difference between the inflow (which is zero after the instantaneous pulse) and the outflow, which is equal to $\frac{C(t)Q dt}{V}$

$$\text{Thus, } dC = C(t) - C(t+dt) = -\frac{C(t)Q}{V} dt = -\frac{C(t)}{\tau} dt$$

with the mean residence time $\tau = \frac{V}{Q}$.

This differential equation can easily be integrated with the result:

$$C(t) = C_0 e^{-\frac{t}{\tau}} \therefore$$

Problem 6:

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As, mathematically, the average, or MRT,
is given by:

$$\text{MRT} = \int_0^{\infty} t E(t) dt$$

Recall Eq. (3) of the Problem 3!

$$\text{RTD} = E(t) = \frac{C(t)Q}{N_T} = \text{const.} \times C(t)$$

We immediately obtain:

$$\boxed{\text{MRT} = \frac{Q}{N_T} \int_0^{\infty} t C(t) dt} \quad \therefore$$