

## Renewable Energy: Solution 04 (Geothermal)

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1. (a) The mass of the air to be heated is :

$$m_{air} = V \cdot \rho_{air} = 8000m^3 \cdot 1.29 \text{ kg/m}^3 = 10320 \text{ kg}$$

The required energy change:

$$\Delta = m_{air} \cdot c_{air} \cdot \Delta T = 10320kg \cdot 1000 \frac{J}{kgK} \cdot 7.3 \cdot 10^{-3}K = 75336J$$

$$\text{Installed heating capacity: } P_n = 75.3 \text{ kW}$$

- (b) COP of heat pump = 4.2

$E$  = Electrical energy (for pump)

$Q_n$  = Useful heat

$Q_u$  = Ambient heat

$$Q_n = Q_u + E$$

Coefficient of power for heat pump is defined as  $COP = \frac{Q_n}{E} = \frac{P_n}{P_{el}}$

This implies electrical power  $P_{el} = 75.3 \text{ kW} / 4.2 = 17.9 \text{ kW}$

Heating power of the probe corresponds to the  $Q_n$  and hence  $P_n = P_u + P_{el}$  implying  
 $P_u = 75.3 \text{ kW} - 17.9 \text{ kW} = 57.4 \text{ kW}$

- (c)  $l$  is the length of the probe. Using  $P_u$  from part b we get:  $l \cdot 52 \frac{W}{m} = 57.4 \text{ kW}$  implies  
 $l = 1104m$

$$\text{we also have : } \frac{Q_u}{l} = \frac{Q_n - E}{l} = \frac{Q_n - \frac{Q_n}{COP}}{l}$$

Insertion of annual heating demand  $Q_n = 135000 \text{ kWh}$  gives:

$$\frac{Q_u}{l} = 93.2 \frac{kWh}{m} < 110 \frac{kWh}{m}$$

- (d)  $E = \frac{Q_n}{COP} = 32143 \text{ kWh}$

implies the electricity cost =  $32143 \text{ kWh} \cdot 0.1367 \text{ Fr./kWh} = 4393.95 \text{ Fr.}$

- (e) Oil heating:

Annual heating demand in MJ equal to  $135000 \text{ kWh} = 486.10^3 \text{ MJ}$

Volume of oil required is  $V_{oil} = \frac{486.10^3 MJ}{42.6 MJ/kg \cdot 0.86 kg/l} = 13266 \text{ litres}$

The price of the oil would be  $13266 \text{ litres} \cdot 0.86 \text{ Fr./litre} = 11408.75 \text{ Fr.}$

(f) CO<sub>2</sub> emission geothermal heat pump :  $E \cdot 0.13 \frac{kg}{kWh} = \frac{Q_n}{COP} \cdot 0.13 = 4179 \text{ kg}$   
 CO<sub>2</sub> emission oil heating :  $486 \cdot 10^3 \text{ MJ} \cdot 0.074 \frac{kg}{kWh} = 35964 \text{ kg}$   
 Hence reduction in CO<sub>2</sub> emission is  $\frac{(35964 - 4179)}{35964} = 88.4\%$

2. (a) Available heat in the geothermal source:  $\dot{Q} = \dot{m}c_p(T_{in} - T_{out}) = 50 \cdot 4180 \cdot (190 - 85) = 21.945 \text{ MW}$

Exergy available in the geothermal source:

$$T_{logmean} = \frac{T_{h,in} - T_{h,out}}{\ln \frac{T_{h,in}}{T_{h,out}}} = \frac{463 - 358}{\ln \frac{463}{358}} = \frac{105}{0.2572} = 408.25 \text{ K}$$

$$Ex_{source} = \dot{Q} * \left(1 - \frac{T_a}{T_{logmean}}\right) = 21.945 * \left(1 - \frac{287}{408.25}\right) = 21.945 * (1 - 0.703) = 6.52 \text{ MW}$$

Exergy for district heating:

$$T_{logmean} = \frac{T_{h,in} - T_{h,out}}{\ln \frac{T_{h,in}}{T_{h,out}}} = \frac{333 - 313}{\ln \frac{333}{313}} = \frac{20}{0.06194} = 322.9 \text{ K}$$

$$Ex_{heating} = \dot{Q} * \left(1 - \frac{T_a}{T_{logmean}}\right) = 12 * \left(1 - \frac{287}{322.9}\right) = 12 * (1 - 0.889) = 1.334 \text{ MW}$$

Energy Efficiency:

- summer:  $3.2 \text{ MW}_e / 21.945 \text{ MW} = 14.6\%$

- winter:  $(2.4 \text{ MW}_e + 12 \text{ MW}_{th}) / 21.945 \text{ MW} = 65.6\%$

Exergy Efficiency:

- summer:  $\epsilon = \frac{Ex_{electrical} + Ex_{heating}}{Ex_{source}} = \frac{3.2 + 0}{6.52} = 49.1\%$

- winter:  $\epsilon = \frac{Ex_{electrical} + Ex_{heating}}{Ex_{source}} = \frac{2.4 + 1.334}{6.52} = 57.3\%$

(b) The marginal electrical efficiency in winter is the elec. production from the residual heat  $(21.945 \text{ MW} - 12 \text{ MW}_{DH} = 9.945 \text{ MW})$ , thus  $2.4 / 9.945 = 24.1\%$