

Topics in Autonomous Robots (ENG615)

Small-scale Robotics

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Lecture Overview

- Introduction to Small Scale Robotics
- Actuation and Locomotion Strategies at Microscale
- Applications

- Part 1: Tethered Systems, Part 2: Untethered Systems, Part 3: Magnetic robots and bioengineered systems

- Summary of the state-of-the-art
- Emphasis on open problems and biomedical research directions

Instructor: Selman Sakar

- Ph.D. in Robotics (Grasp Lab, Uni of Pennsylvania)
 - Single cell manipulation, Bacteria-powered microrobots
- Postdoc in Bioengineering (M.I.T.)
 - Biological machines from living muscle
- Research Scientist in Medical Robotics (IRIS, ETH Zurich)
 - Bacteria-inspired adaptive microswimmers, Robotic microsurgery
- Assistant Professor at EPFL
 - Research: Microrobotics, mechanobiology, self-organization
 - Website: microbs.epfl.ch

Grand Vision

- Many of the cells are very tiny, but they are very active; they manufacture various substances; they walk around; they wiggle; and they do all kinds of marvelous things all on a very small scale. Also, they store information. Consider the possibility that we too can make a thing very small which does what we want that we can manufacture an object that maneuvers at that level!

There is Plenty of Room at the Bottom, Richard Feynman 1959

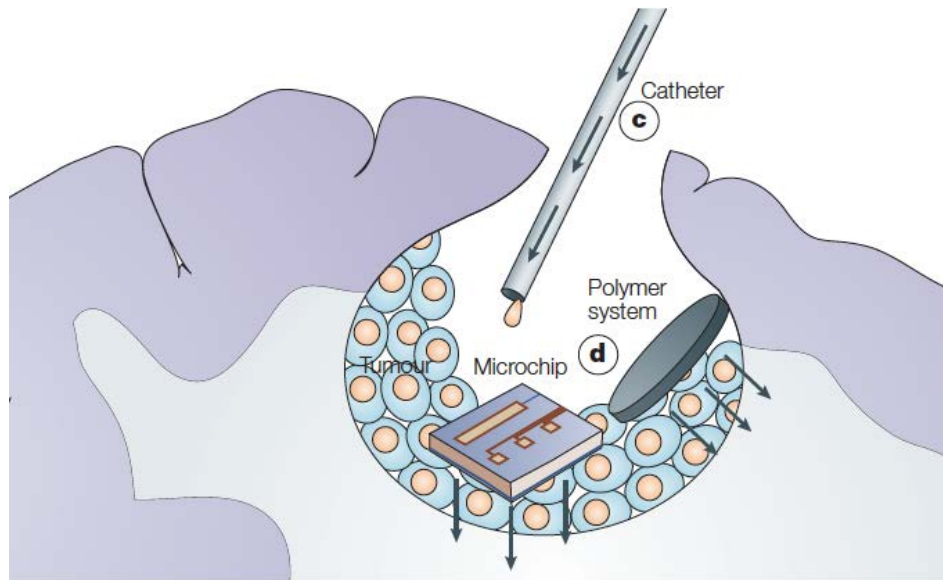
Grand Vision

- ...although it is a very wild idea, it would be interesting in surgery if you could swallow the surgeon. You put the mechanical surgeon inside the blood vessel and it goes into the heart and “looks” around. It finds out which valve is the faulty one and takes a little knife and slices it out. Other small machines might be permanently incorporated in the body to assist some inadequately functioning organ.



Targeted Therapy

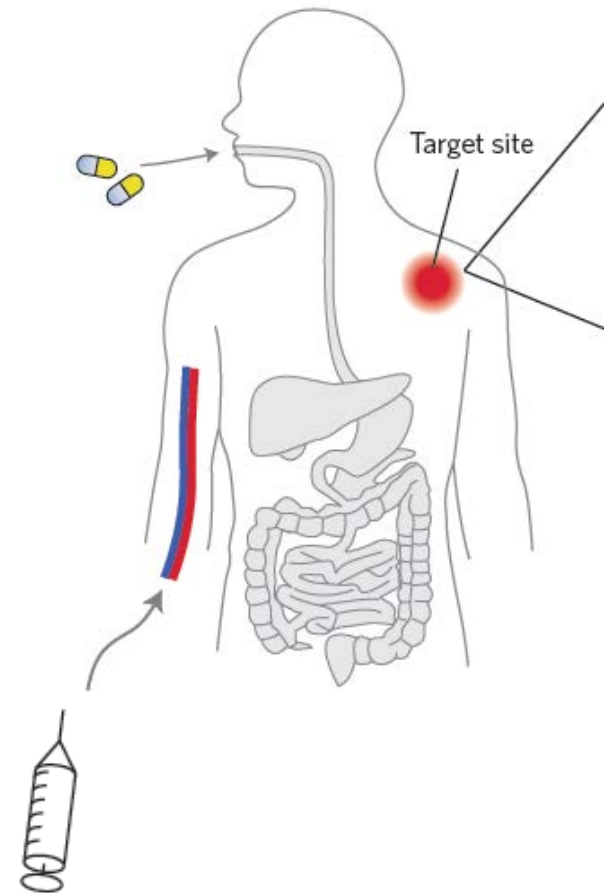
- Targeted and Triggered Drug, Cell and Gene Therapy
 - The importance of spatiotemporal control over release
 - Minimizing off-target effects and maximizing efficacy
 - Advances in RNA-silencing, genome engineering and reprogramming



M. Lesniak, *Nat Rev Drug Discov*, 2004

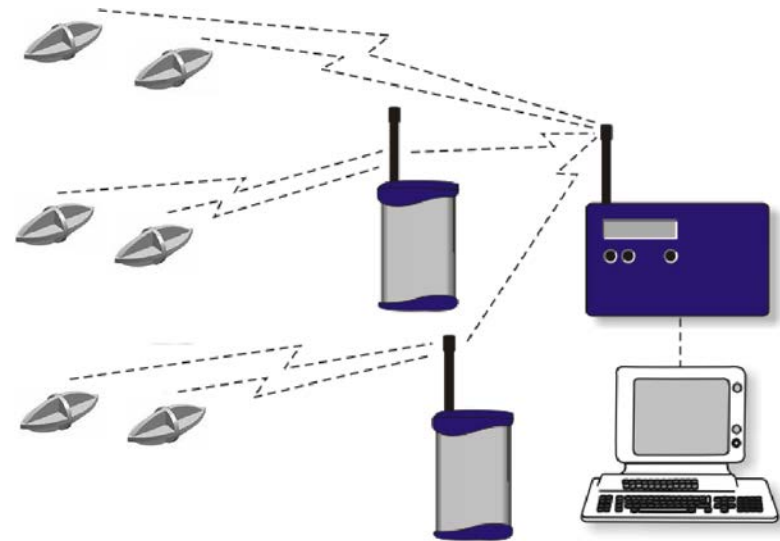
Targeted Therapy

- Localized delivery of chemical and biological substances
- Localized application of energy
- Drug delivery
 - Currently, the whole body is subjected to the drug through the blood stream
 - Increased chances of side effects
 - A microrobot carrying a small amount of drug
 - Decreases side effects,
 - Subjects the tissue to high drug concentration



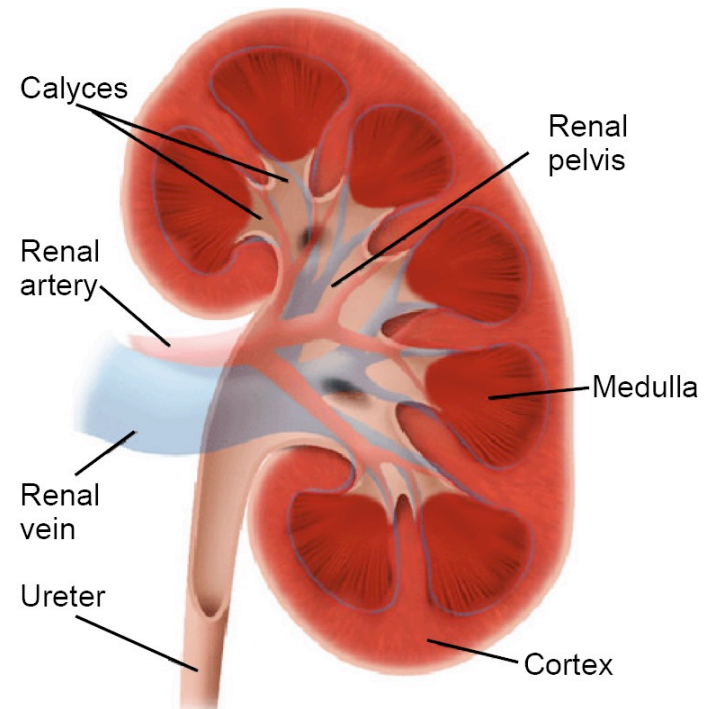
Telemetry

- Micromachines can be used for transmitting information from a specific location which is difficult to obtain
 - pH and temperature of digestive track
 - Oxygen concentration in the eye
 - Urea and glucose concentration in blood
 - Detection of internal bleeding
- This information can be sent back in various ways, using
 - Radio waves
 - Visible light
 - Acoustic waves



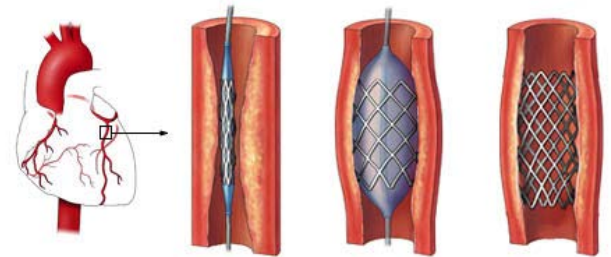
Material Removal

- Micromachines can be used to remove material by mechanical means
- Lithotomy and Lithotripsy
 - Kidney stone removal (lithotomy)
 - Kidney stone destruction (lithotripsy)
- Excision
 - Removal of tumor or blood clot
- Biopsy sampling



Deployable Structures

- Another application area for biomedical microrobots, is that of a passive controllable structure
- Scaffolding
 - The microrobot can act a support frame, for example in
 - Nerve regeneration
 - Development of artificial organs
 - Blood vessel regrowth
 - Microrobots can be used instead of catheter-based stents
 - They would be the stent
 - They would navigate in the correct location
 - And then they would deploy

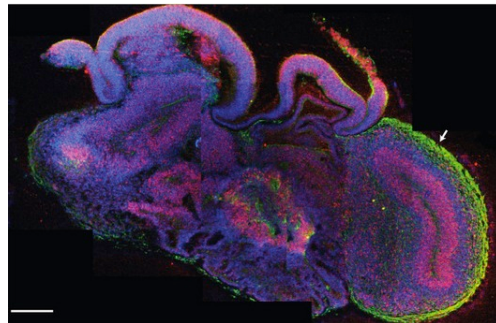
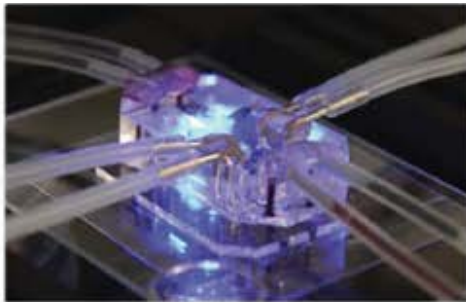


Specifications

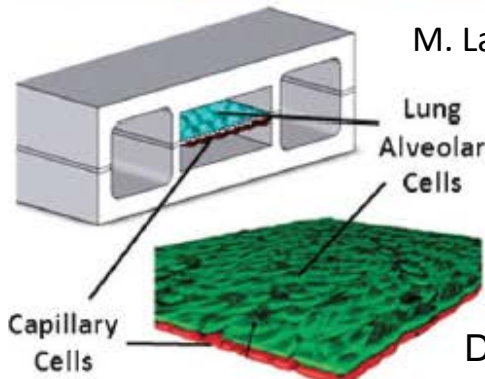
- To access remote locations, the size of the robot should be in the millimeter or micrometer range.
- Power and control signals must be transmitted from a distance
- Flow can be a significant issue
- Most of the body parts are not visible (special methods for localization) and have complex shapes (navigation)
- Lumens and cavities are filled with viscoelastic fluids

Microfluidic Manipulation Technology

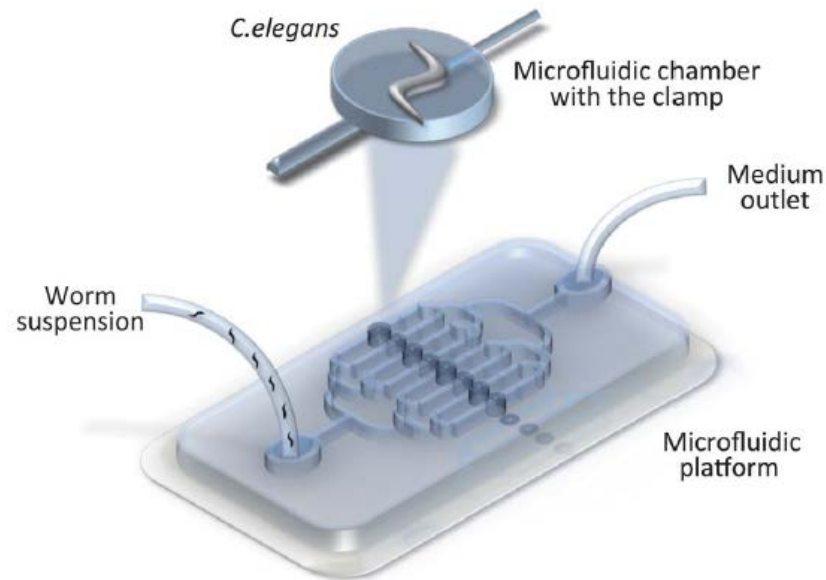
- The emergence of engineered tissues/organs and organoids to recapitulate physiology and pathology
 - Two-dimensional culture assays are limited and sometimes misleading
- Advanced microfluidic platforms for high-throughput screening with embryos and small model animals



M. Lancaster *et al.*, *Nature*, 2013



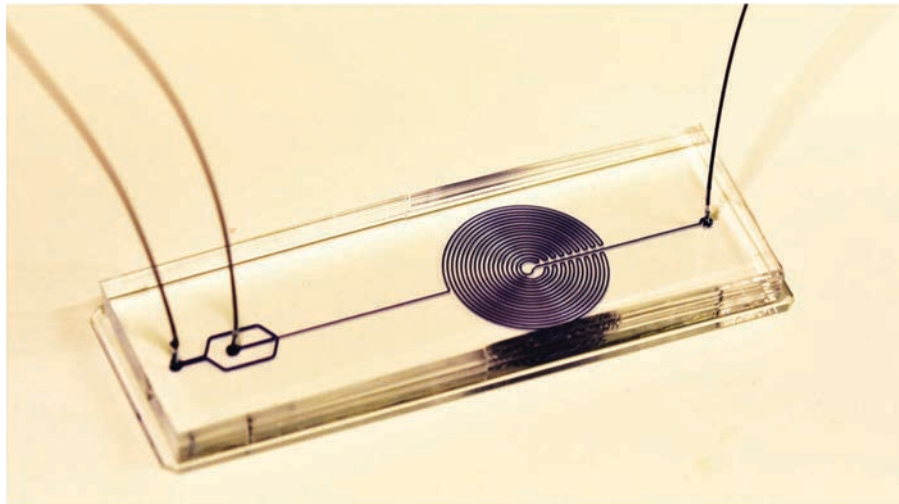
D. Huh *et al.*, *Science*, 2012



N. Bakhtina *et al.*, *RSC Adv*, 2014

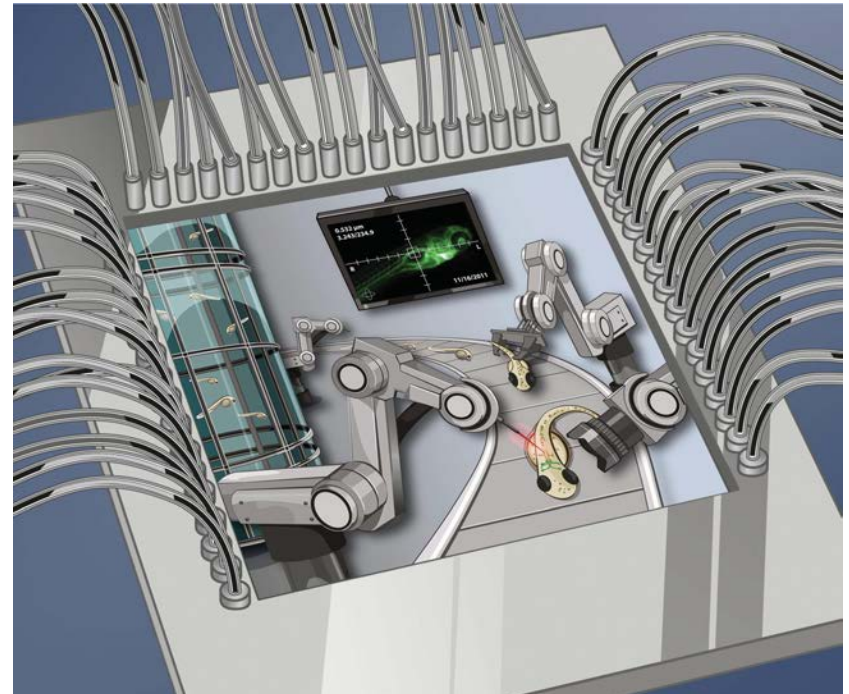
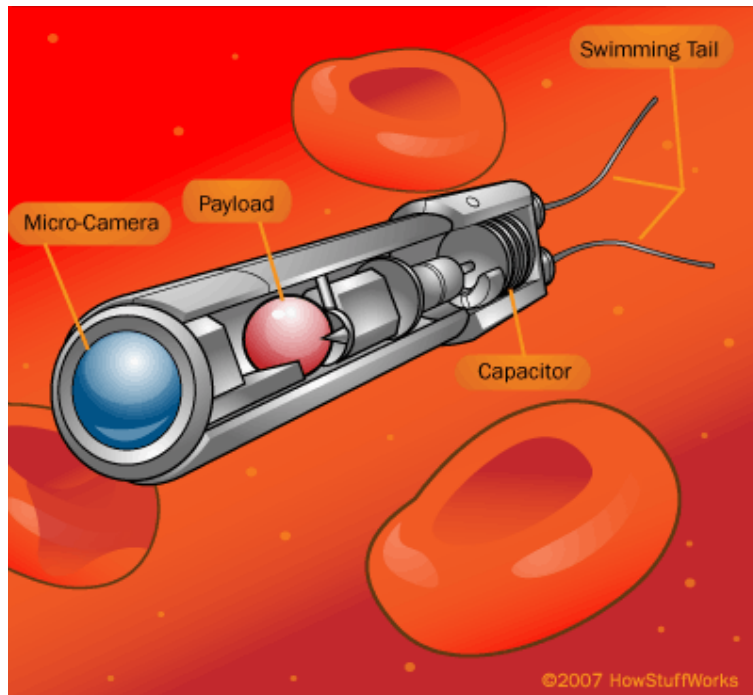
Motivation

- Control over forces, geometry and motion at small scale
 - Analogous to chemical manipulation systems
 - Minimally invasive
 - Compatible with quantitative time-lapse microscopy
 - Supported with computational modelling
 - Challenges: Cost, ease of use, versatility, compatibility, repeatability



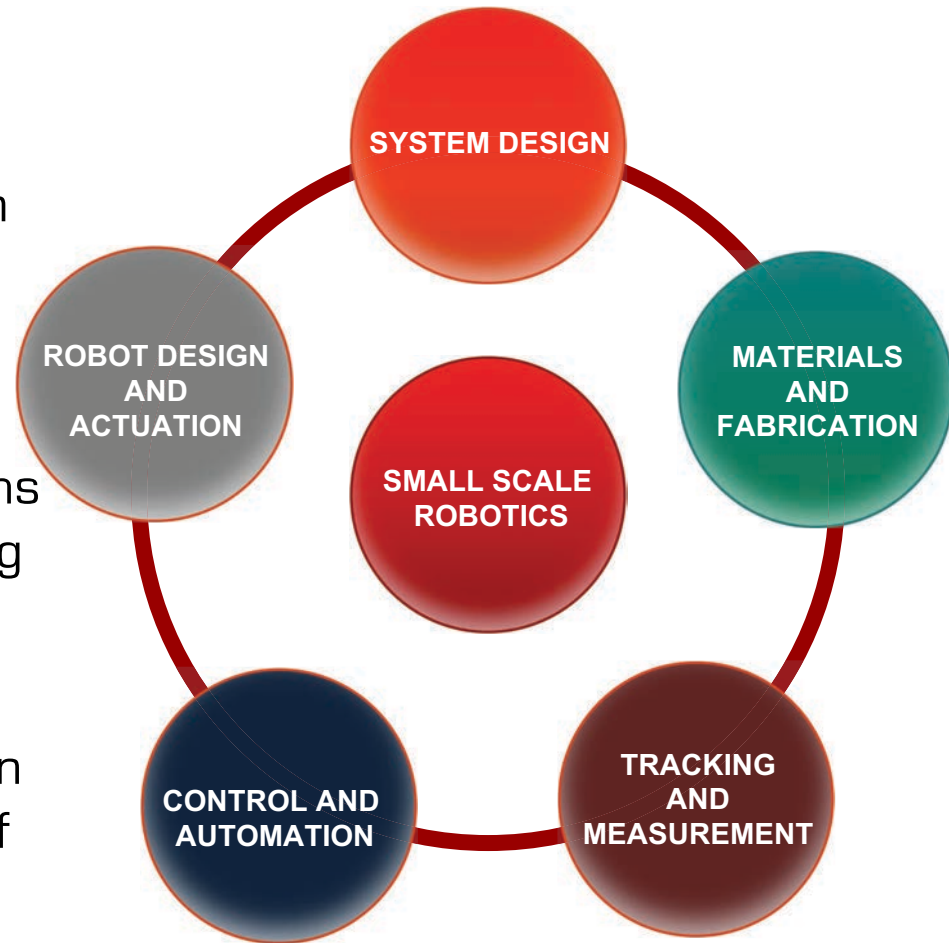
Microrobotic Platforms in Biomedical Research

- Microrobotic Platforms can introduce mobility, dexterity, precision, automation and new functionality
 - Mobile Micromachines (minimally invasive, targeted and triggered therapy in vitro and in vivo)
 - Advanced Microchips (cutting-edge microtools for characterization, diagnosis and treatment of engineered tissues and model animals)

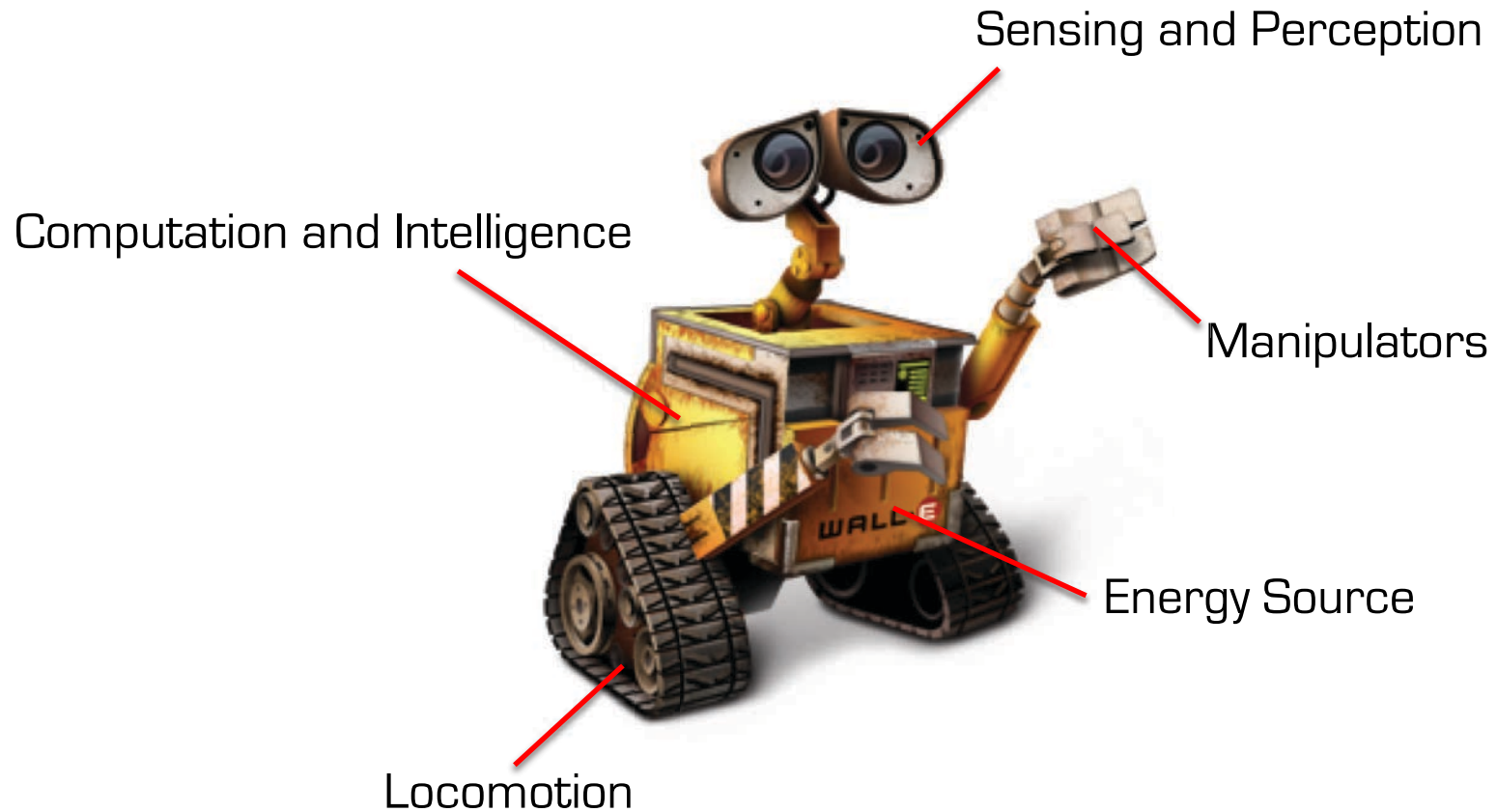


Methodology

- The fabrication and operation of complex micromachines operating in 3D microenvironments
- The development of modular and compact micromanipulation platforms equipped with state-of-the-art imaging capabilities
- The development and implementation of advanced algorithms for control of individual robots as well as swarms



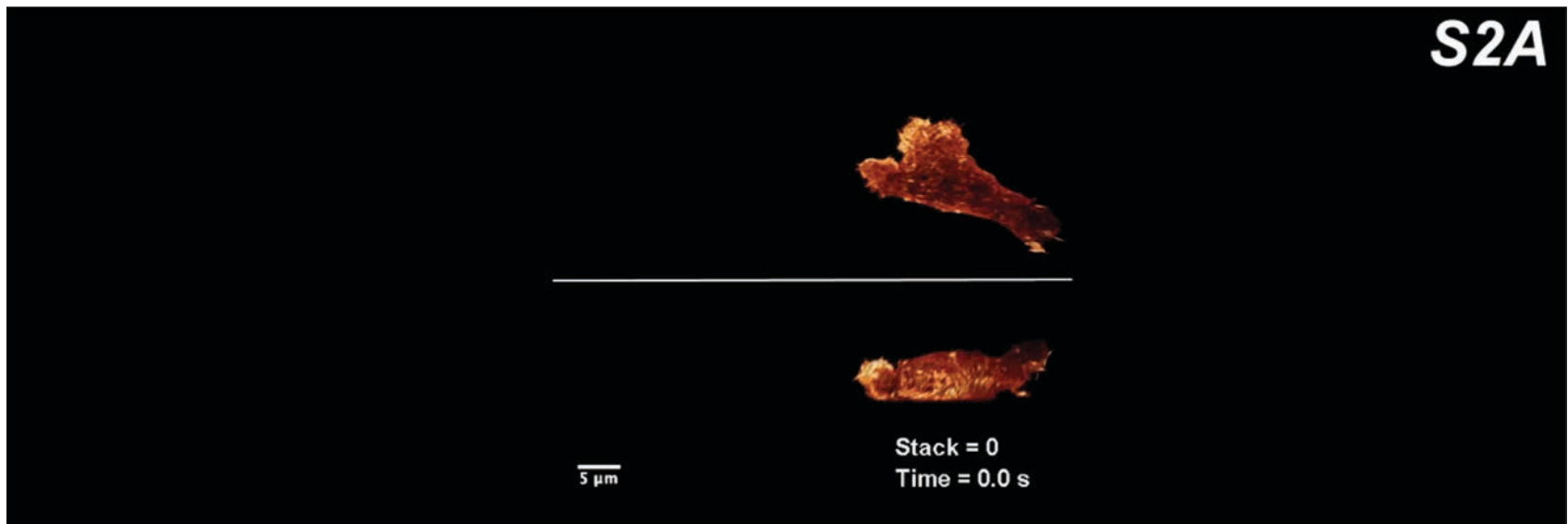
Autonomous Mobile Robots



Grand Challenge

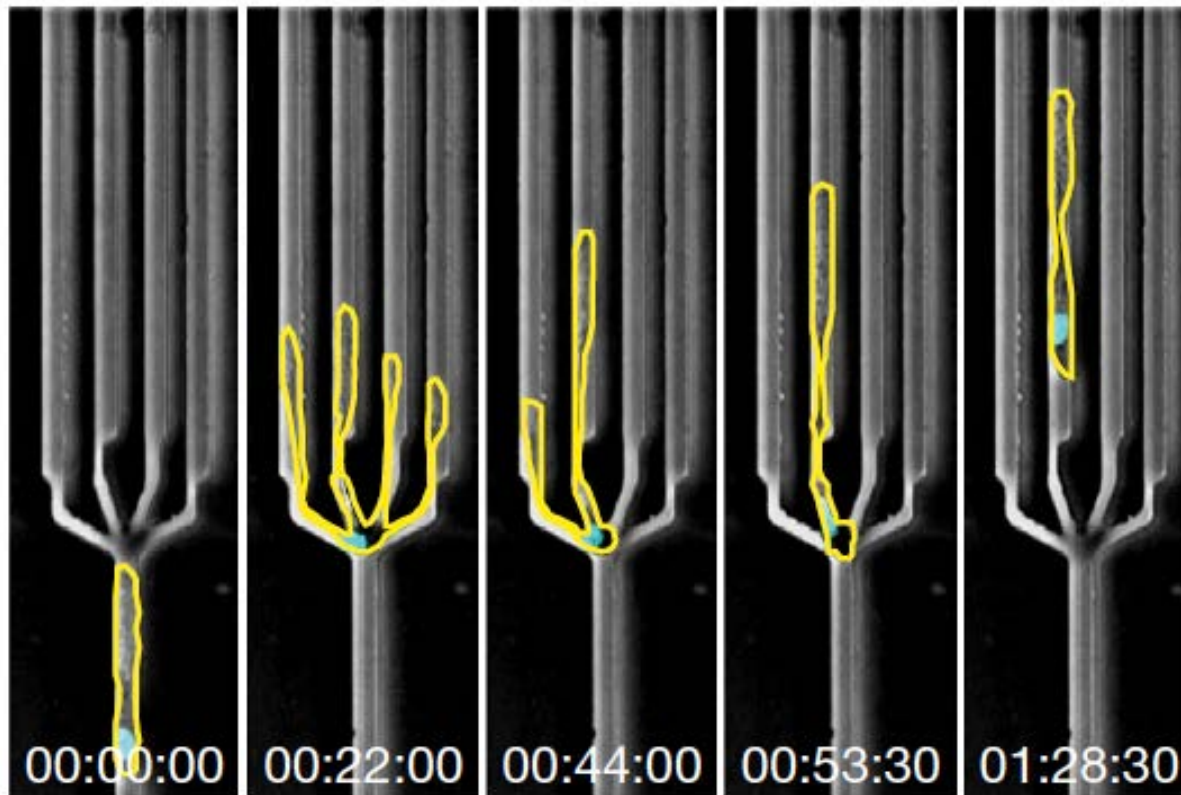
- Cells are distributed intelligent systems
- No central controller (i.e. brain) or sensing network (distributed receptors)
- Diffusion and active transport of signals (proteins)
- We are not even close to engineering an autonomous untethered microrobot

Immune cell (cytotoxic T cell) killing a cancer cell



Nuclear positioning and path finding

- Robots without brain and nervous system



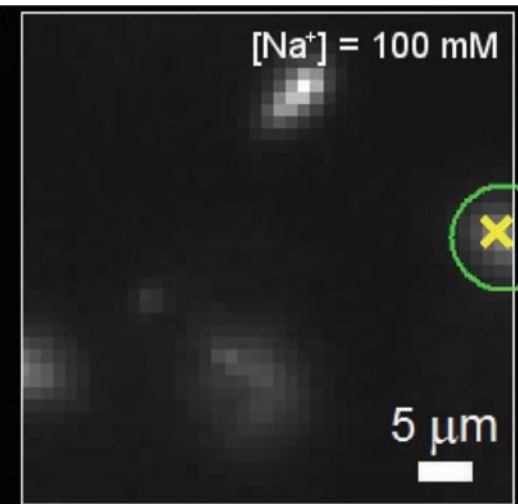
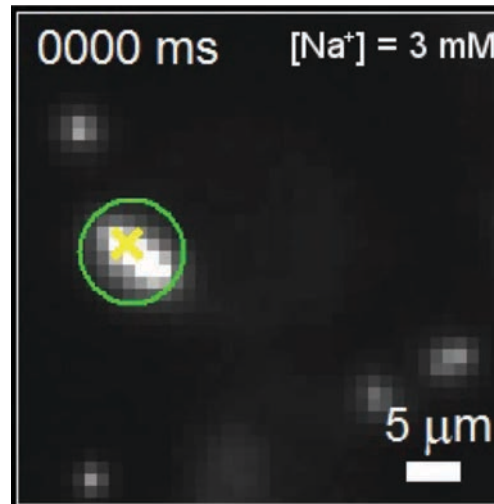
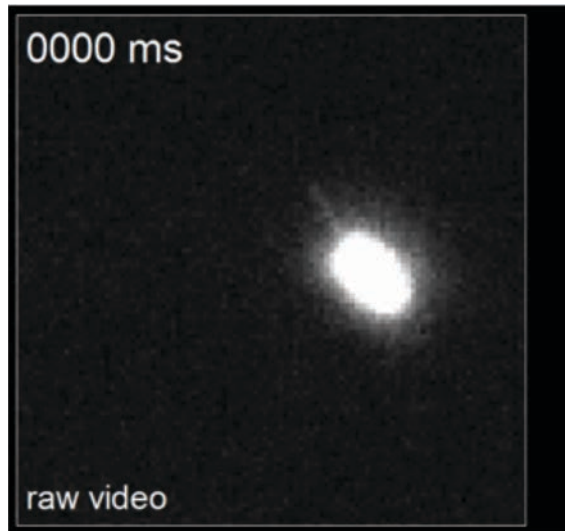
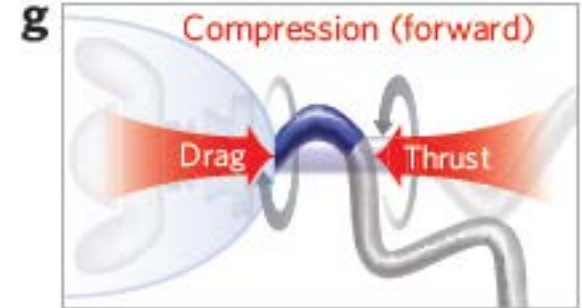
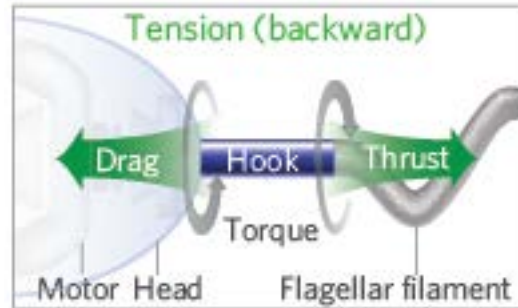
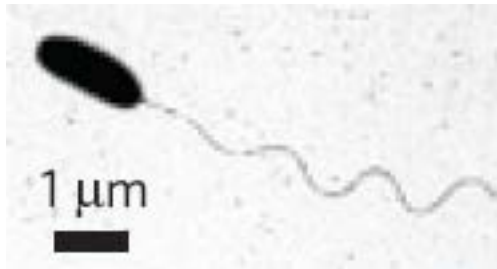
Nucleus-first vs MTOC-first
Configuration

Dendritic Cells

Single Pore Decision

Elastic Instabilities and Chemotaxis

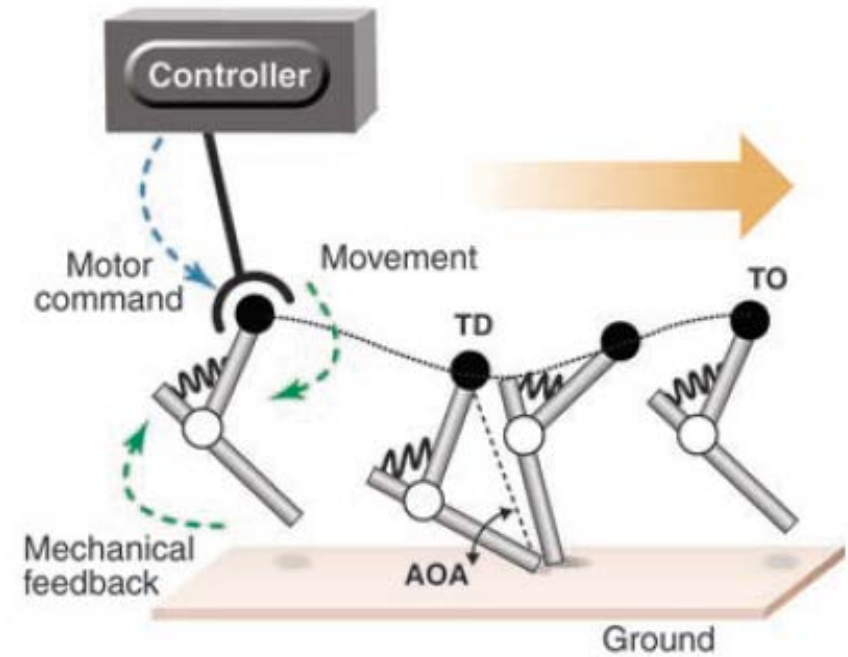
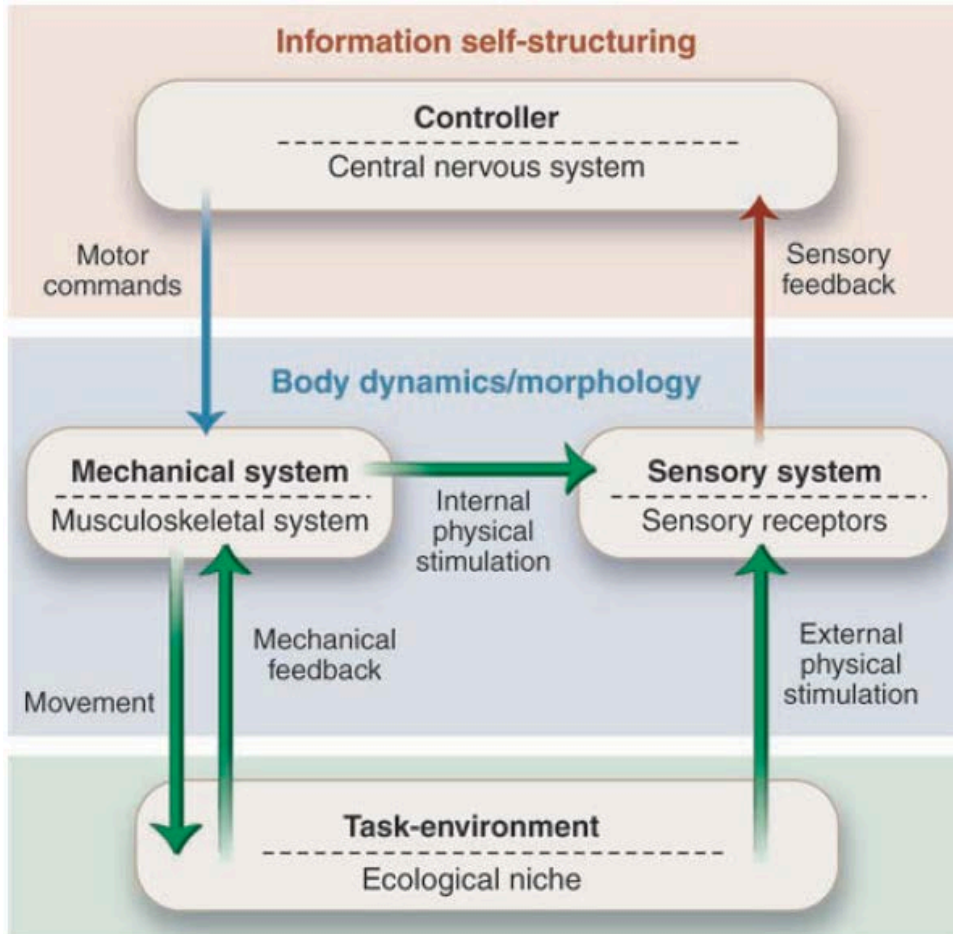
Vibrio alginolyticus



Son et al, Nature Physics, 2013

Embodied Intelligence

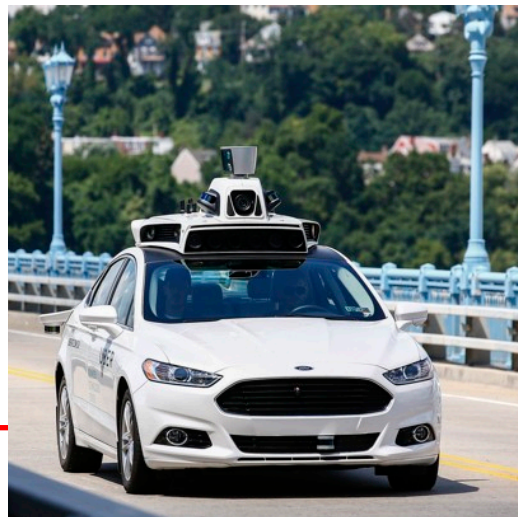
- Robots without brain and nervous system



Self (passive) stabilization

Macroscale Autonomous Robots

- Tethered vs untethered (vehicles and legged robots)
- Plant vs animal analogy
- Electric motors, heat engines, turbomachinery, hydraulics
- Battery



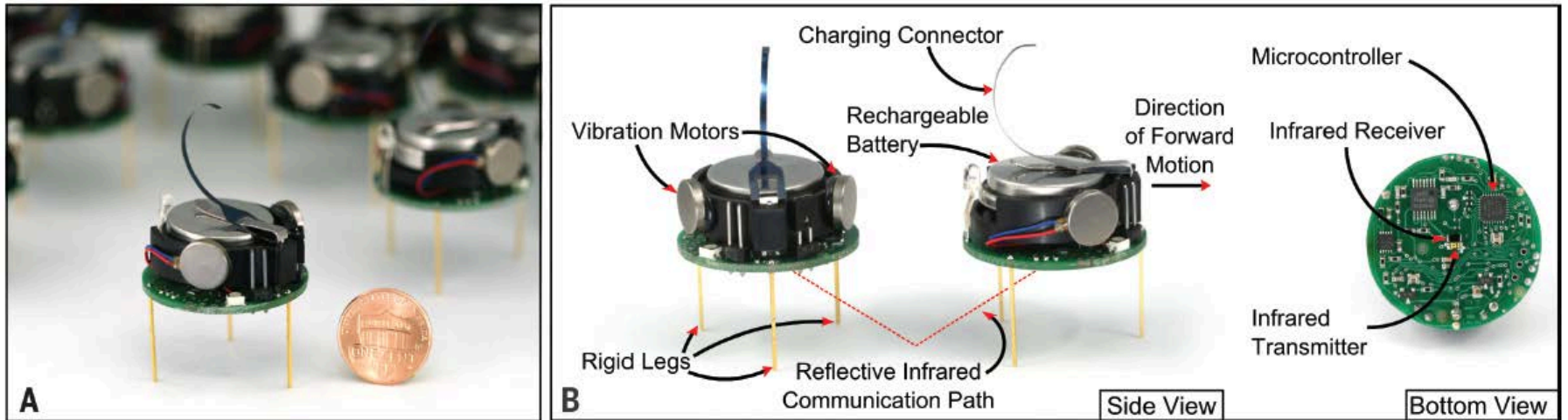
Mesoscale Autonomous Robots

- A few mm to tens of centimeters
- Energy storage: Battery, Spring mechanisms (clockwork)
- Pneumatic systems (soft robotics)
- Exotic actuators (shape memory alloys, magnetostrictive materials, dielectric elastomers, piezoelectric actuators)
- RF energy transfer

- Inertial effects are less effective but still dominant
- Can we simply scale down these robots?
- Is there a way to use them for micromanipulation?

Electric Motors: Kilobots

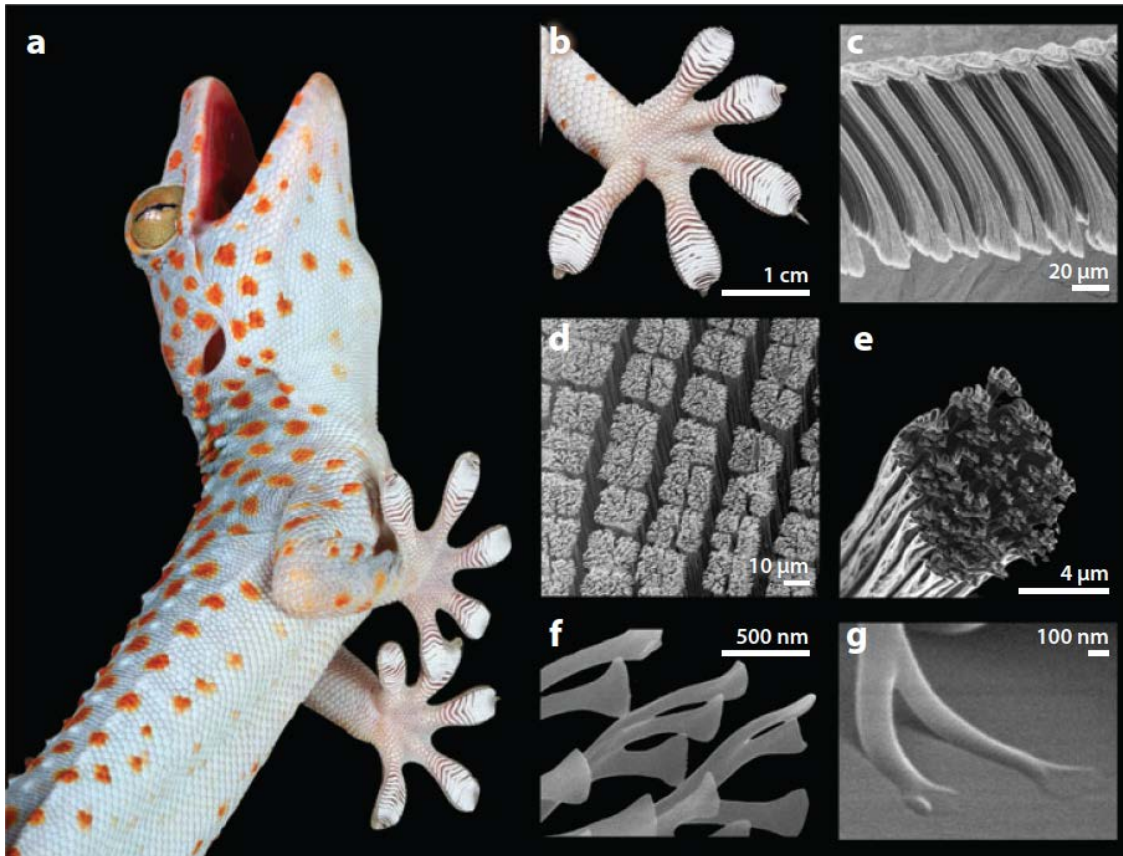
- Two vibration motors and a rechargeable battery
- IR transmitter and sensors
- Smallest commercially available battery: few millimeters



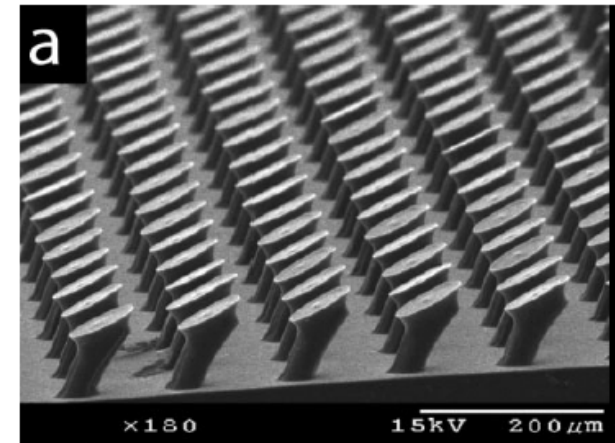
Scaling of Actuators: Electric motors

- Magnetic and inertial forces scale down poorly into the micro domain
- Miniaturization of many complicated components such as coils, magnets, and bearings
- Severe torque dissipation due to the scaling (adhesion, damping)
- Dominant role of electrostatics, surface tension, viscous forces, chemical reactions, heat transfer, vibrations
- State of the art motors: centimeter-sized
- You can find a review article on Moodle

Van der Waals Forces



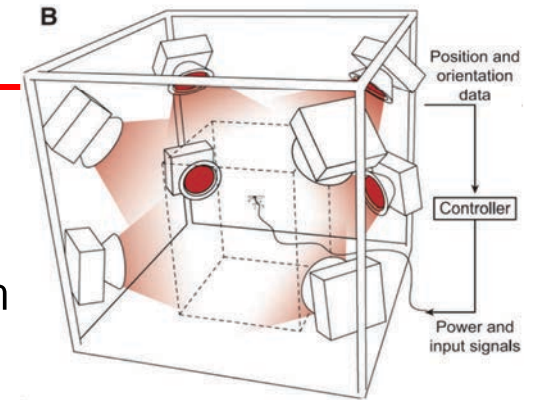
Autumn et al, *Annu Rev Eco*, 2014



Murphy et al, *Small*, 2009

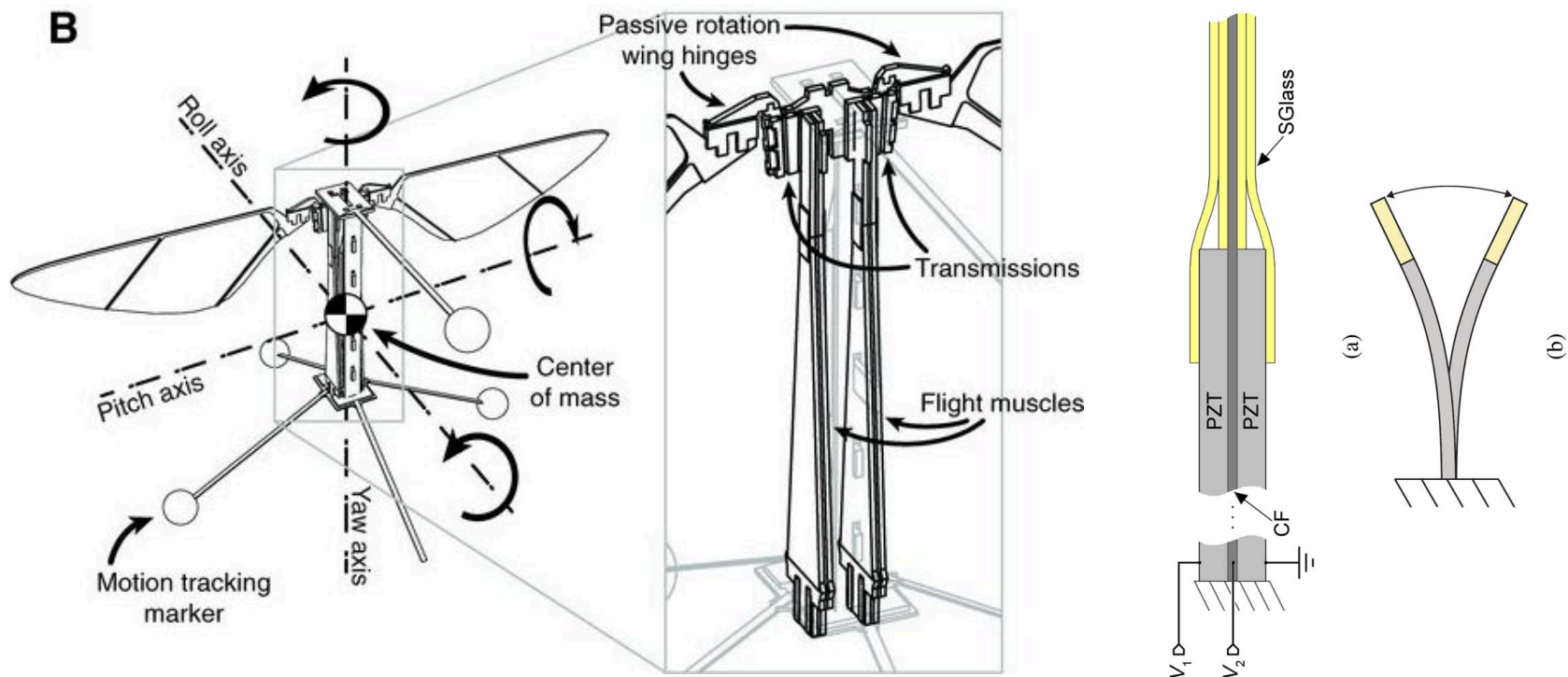
Piezoelectric Actuators: RoboBee

- Size: 3cm, Mass: 80 mg (pico-quadrotor is 10cm)
- Power consumption: 19 mW
- Controlled flight inside Vicon motion capture system
- Motion resolution : 1 mm



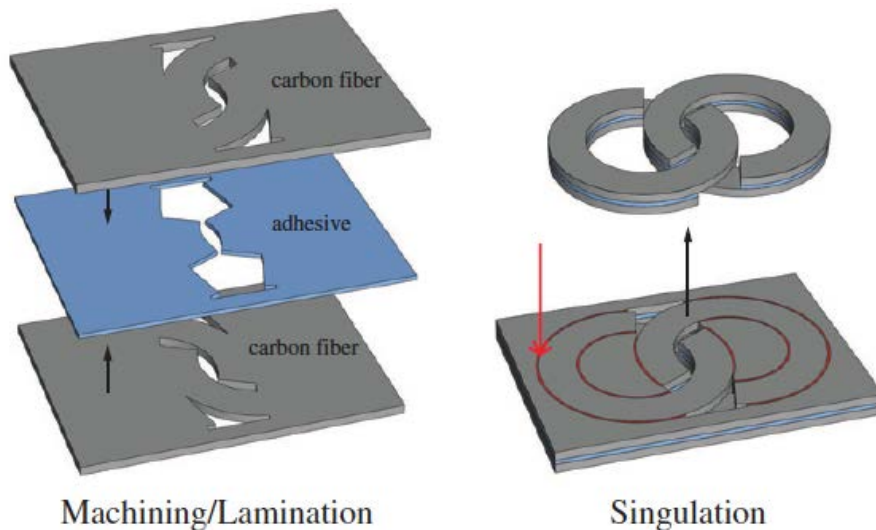
Piezoelectric Actuators: RoboBee

- Carbon fiber reinforced plastic structure (500 um thick)
- Titanium alloy wings (50 um thick)
- Polyimide joints (15 um thick)
- PZT actuators (120 um thick)



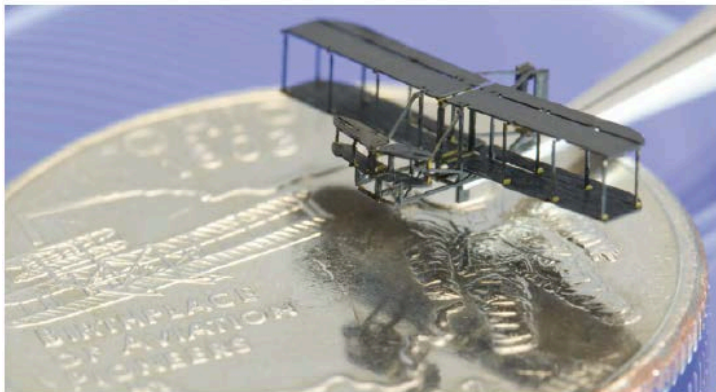
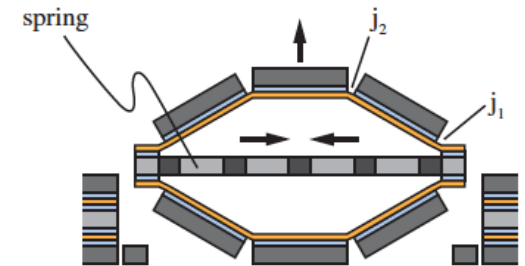
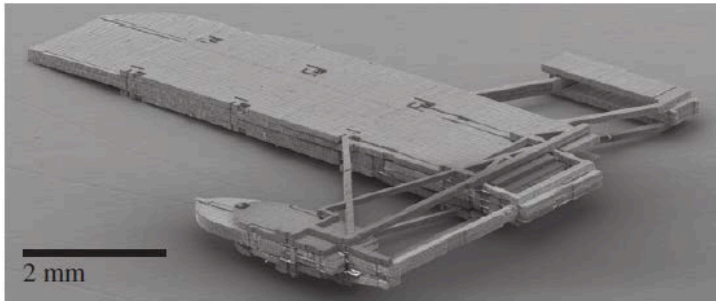
Monolithic Fabrication of Compliant Mechanisms

- Printed circuit board techniques
- Multilayer laminates, alignment pins,
- Leaving small tabs or bridges connecting parts to the bulk material
- Laser micromachining (355 nm): 1-150 μm thickness, 8 μm beam
- Electropolishing, ultrasonic cleaning, plasma treatment
- Acrylic sheet adhesive for lamination



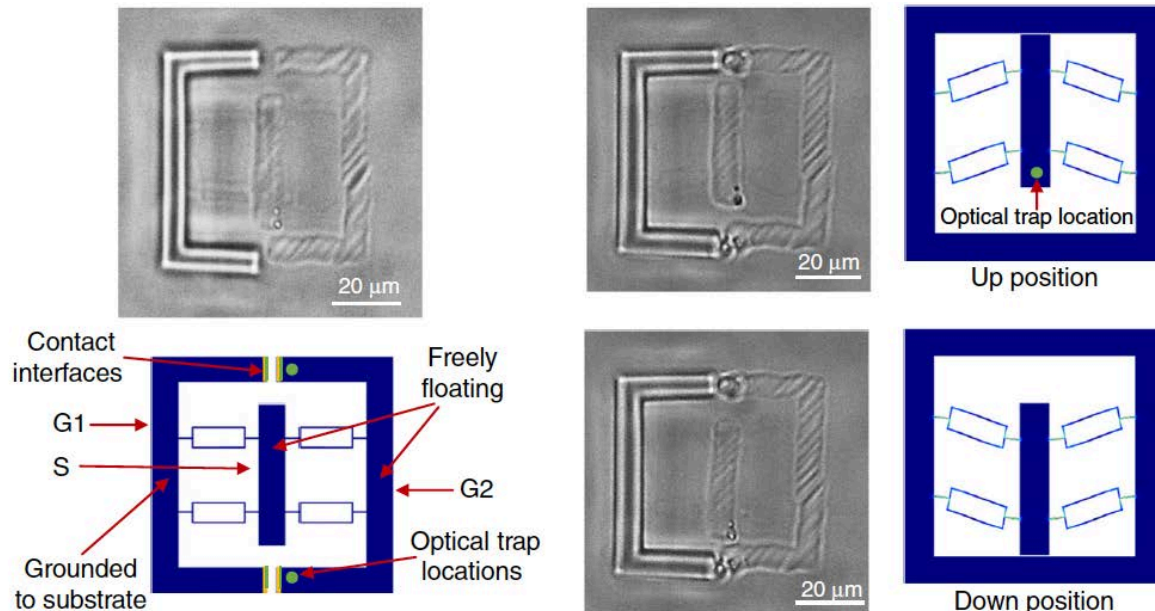
Monolithic Fabrication of Mechanisms

- Pop-up book folding: multiple rigid-flex folding layers are stacked and bonded together.
- Model is released by trimming each bridge and opening the mechanisms like a book.
- Springs to perform self-folding of pre-strained layer



Compliant mechanisms at microscale

- Photolithography, etching, 3D direct laser writing, DNA origami
- Down to nanometer size
- Few or no conventional hinges (revolute or sliding joints)
 - Reduced wear, simplified manufacturing, no or minimal assembly
- **Design:** trial and error process
- **Performance:** fatigue, creep, limited rotation



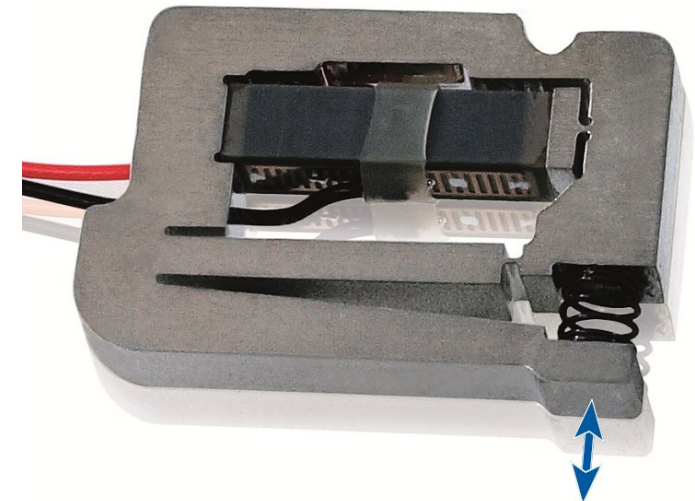
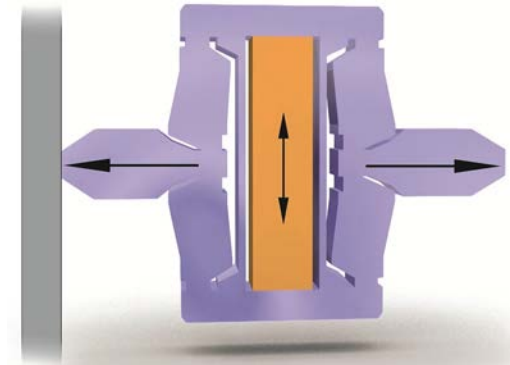
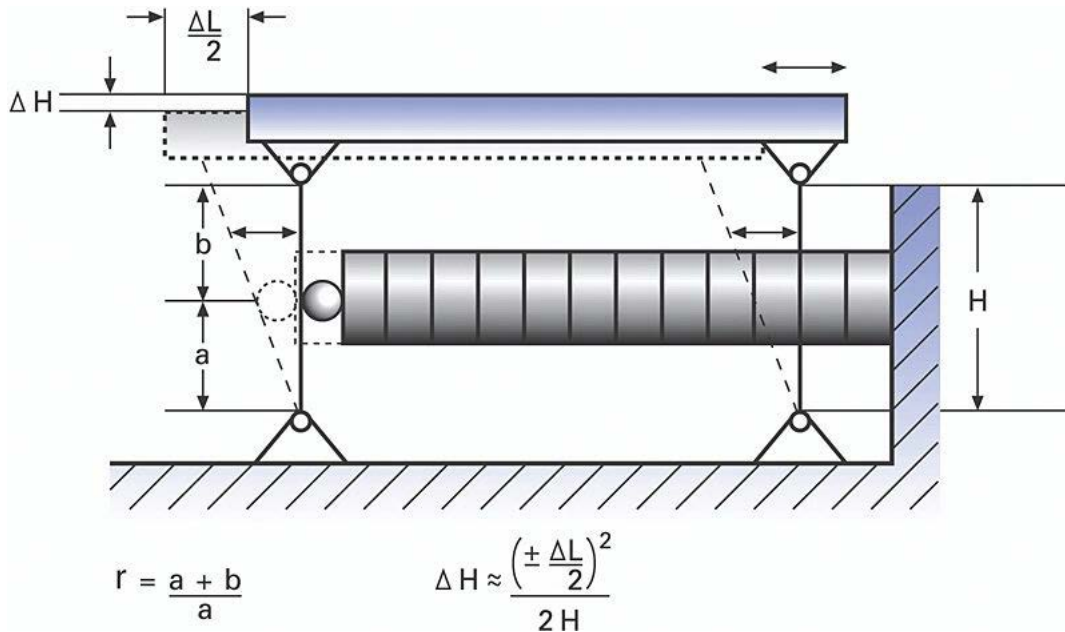
Why Use Piezo?

- Position precision
 - Almost linear dimensional change free of stiction effects
 - Down to sub-nanometer range
- Speed
 - Solid-state actuation: speed of sound (kHz)
 - Can respond to an input in milliseconds (valve control)
- High Force
- Reliability, generate little heat, nonmagnetic, vacuum compatible, few mechanical components (wear)

- **Cons:** Small actuation strain
 - Typically 0.1 percent of the length at max voltage
 - Frictionless lever amplifiers
- **Cons:** Brittle ceramics and large excitation field (MV/m range)

Amplification Mechanisms

- Flexure-guided (flexure linkages, flextensional mechanism)
- With increasing amplification ratio, both stiffness and responsiveness are reduced (preloading?)
- Bending actuators



Dielectric Materials

- All dielectric materials when subjected to an external electric field undergo change in dimensions.
 - Why? Displacement of positive and negative charges.
 - Dielectric crystal lattice: cations and anions connected by springs (interionic chemical bonds)
 - Cations get displaced in the direction of the electric field and anions in the opposite direction
 - Amount of deformation depends on the crystal structure

Important Dielectric Parameters

- Electric dipole moment p
- Electric polarization (polarization density) P [coulomb/m²]
- Electric displacement field (flux density) D [coulomb/m²]
- Dielectric constant ϵ_r
- Electric susceptibility χ
- Vacuum permittivity (permittivity of free space) ϵ_0

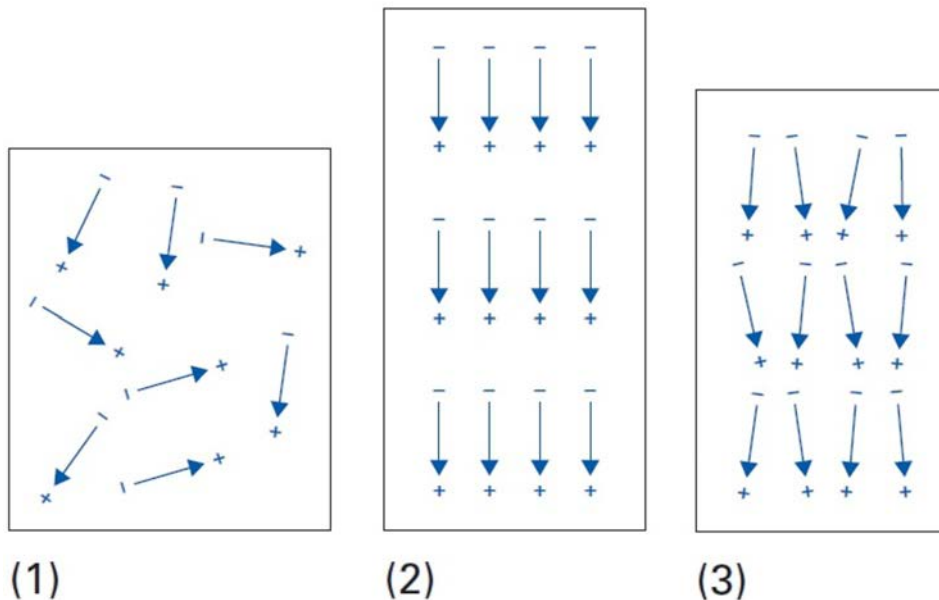
- Gauss's Law and Maxwell's equations

Inversion Symmetry in Crystal Structure and Electrostrictive Effect

- Centrosymmetric dielectric materials
 - When subjected to external electric field, the movement of cations and anions are such that extension and contraction get canceled out between neighboring springs and the net deformation is zero.
 - There are second order effects (chemical bonds are not perfectly harmonic) which lead to a small net deformation
 - Deformation is proportional to the square of the electric field (electrostrictive effect)
- Non-centrosymmetric dielectric materials
 - When subjected to external electric field, there will be asymmetric movement of the neighboring ions, resulting in significant deformation of the crystal
 - Deformation is proportional to the applied electric field (piezoelectric effect)
 - Second order effects are also present but negligible

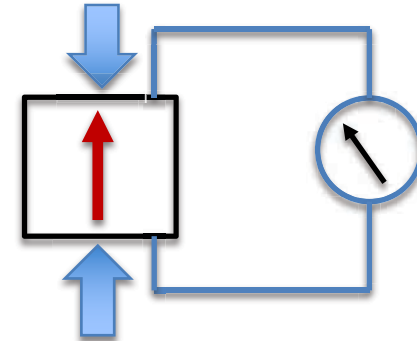
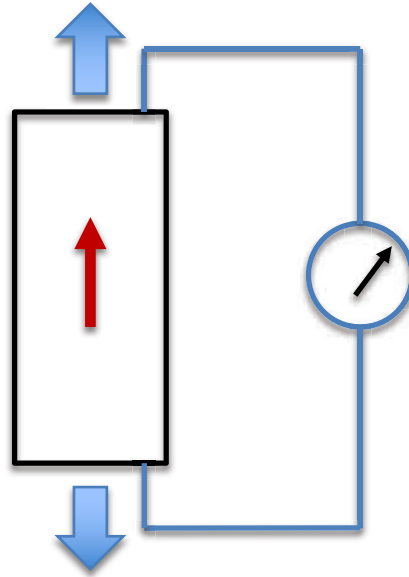
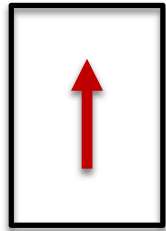
Poling

- The process of generating net remnant polarization by applying sufficiently high electric field (to attain saturation polarization) at a temperature slightly less than the transition temperature
- 2-3h of electric field application
- Most of the domains remain frozen in the oriented state even after cooling to room temperature

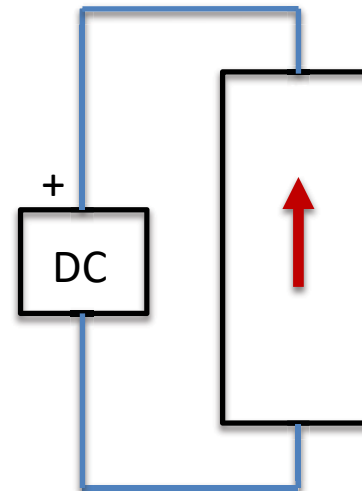
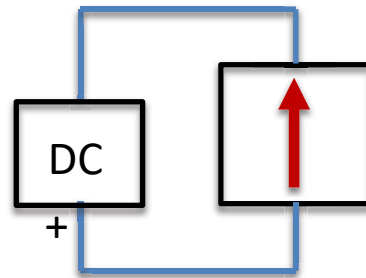
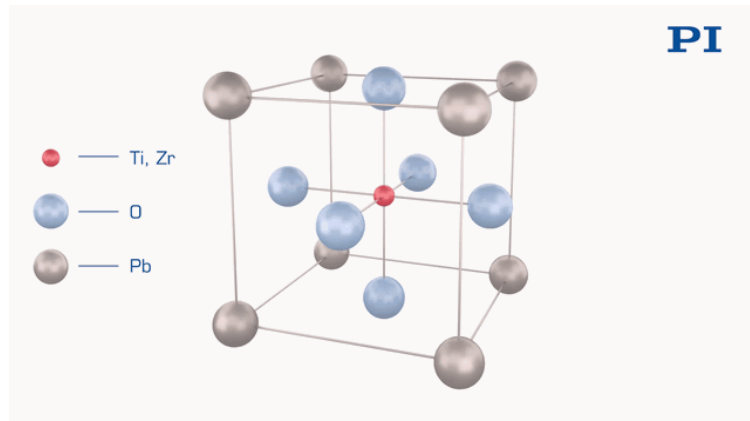


Piezoelectric Effect

Poled piezoelectric material



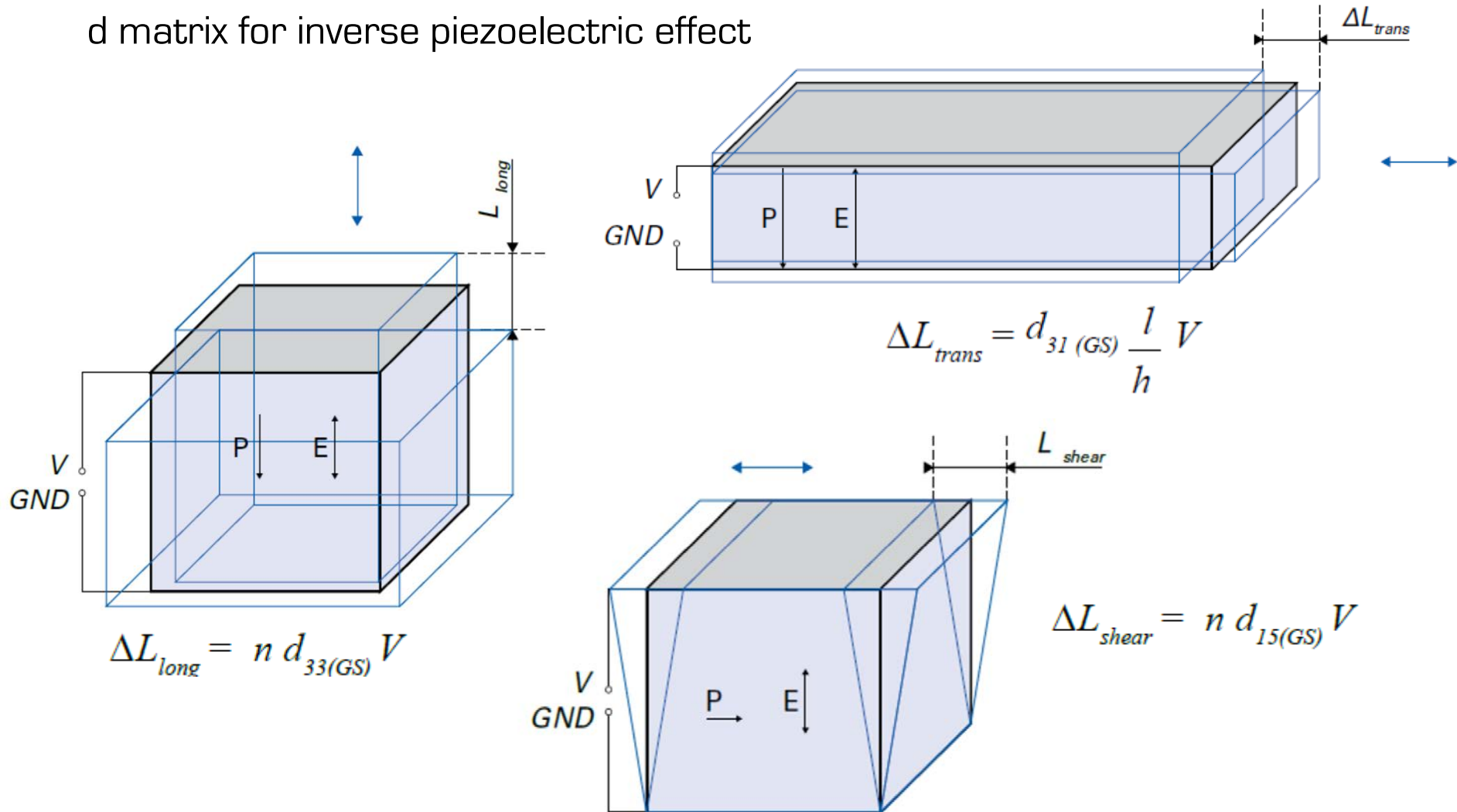
direct



inverse

Piezoelectric Characteristics

d matrix for inverse piezoelectric effect



Piezoelectric Materials

- Quartz (crystalline form of silicon dioxide, natural)
 - Crystal cut, chemical etching, watches, computer clocks
- Lead zirconate titanate ($\text{PbZr}(\text{Ti})\text{O}_3$, PZT).
- **Electromechanical coupling coefficient**

$$k^2 = \frac{(\text{piezoelectric energy density stored})^2}{\text{electrical energy density} \times \text{mechanical energy density}}$$

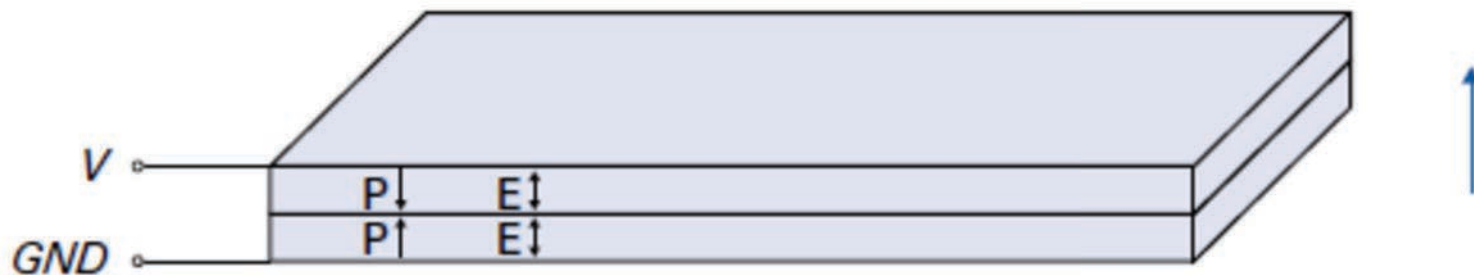
Property	PZT	PMN-PT	PZN-PT
Strain [%]	0.2	0.6	1.7
Stress [MPa]	110	>100	130
Efficiency [%]	90	90	90
Electromechanical coupling (k_{33})	0.7	0.92	0.95
Piezoelectric coefficient (d_{33}) [pC N^{-1}]	750	2500	2500

Bimorph configuration

- Bonding two strips with opposing piezoelectric expansion axes
- For a cantilever mounted bimorph, the unloaded deflection δ of the beam resulting from the applied voltage V

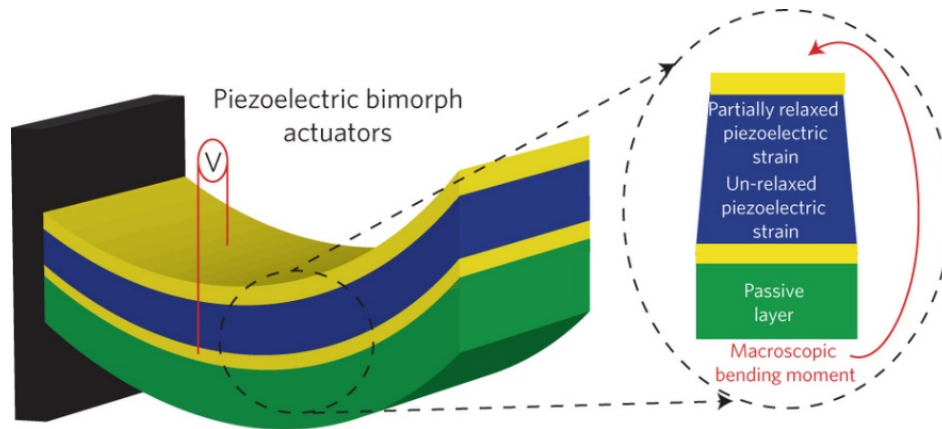
$$\delta = \frac{3}{5} d_{31} V \left(\frac{L}{a} \right)^2$$

Where a is the width of each strip, L is the length, $d_{31} = 2 \times 10^{-11}$ m/V for PVDF. As an example, $a = 0.5$ mm, $L = 30$ mm, $V = 300$ V then $\delta = 13$ μ m.



Bimorph configuration

- Coupling with a passive layer

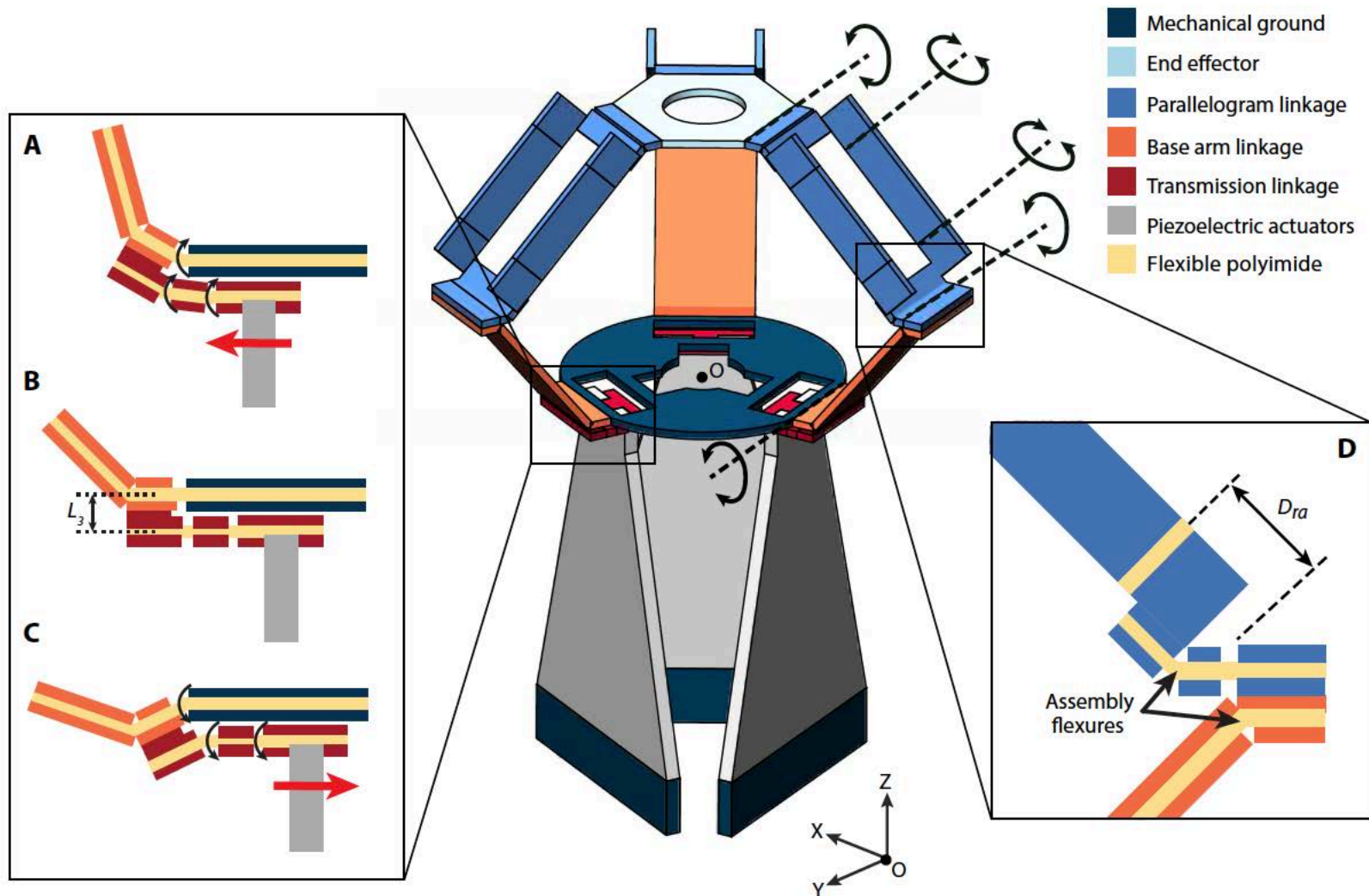


L = Bending displacement [m]
 d_{31} = Transverse deformation coefficient
 n = Number of stacked layers
 V = Operating voltage
 l_f = Bender length
 h_p = Height of piezo
 R_h = Ratio of substrate height and ceramic height
 R_E = Ratio of elastic moduli of substrate and ceramic

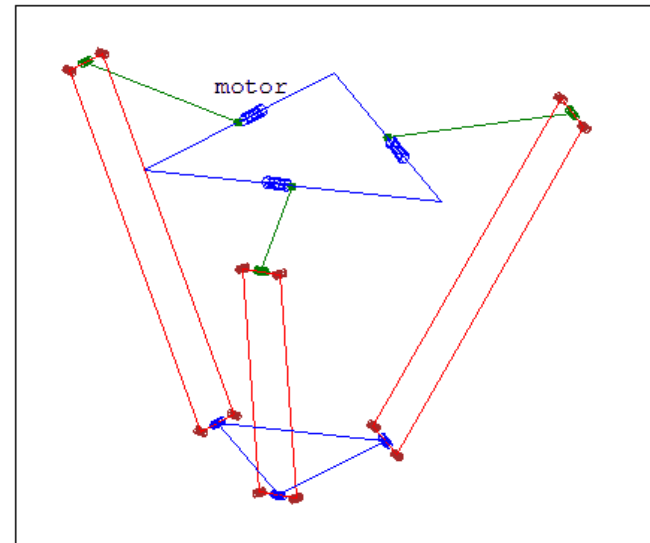
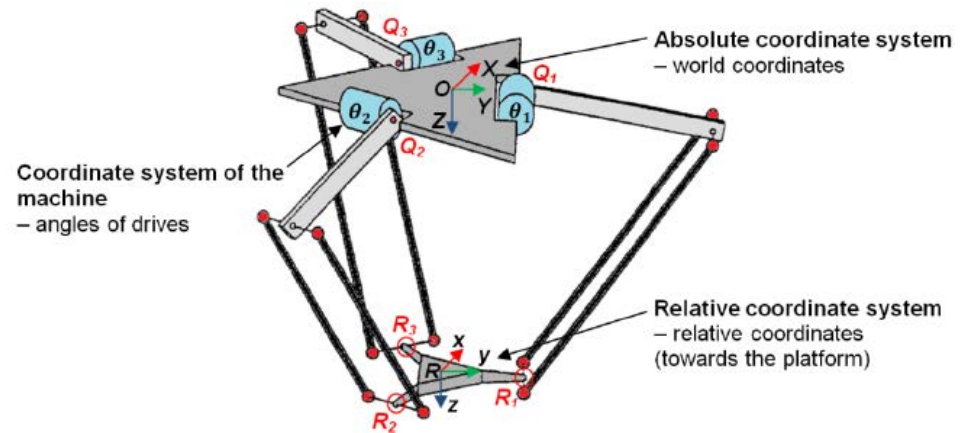
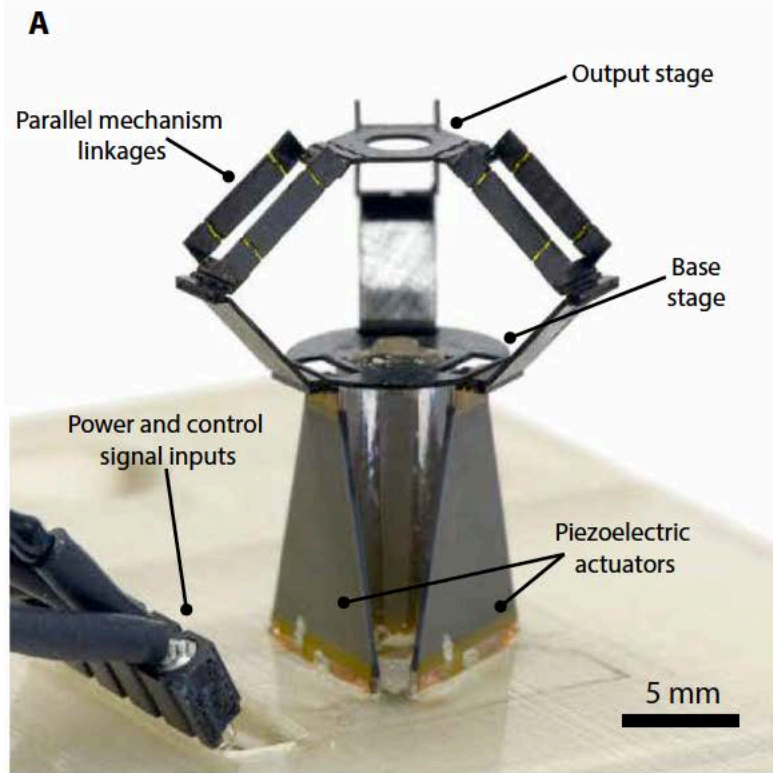
$$\Delta L_{bend} = \frac{3}{8} n d_{31(GS)} \frac{l_f^2}{h_p^2} \frac{2R_h R_E (1+R_h)}{R_h R_E (1+R_h)^2 + 0.25(1-R_h^2 R_E)^2} V$$

Timoshenko Beam Theory

Robotic Micromanipulation: milliDelta Robot



Robotic Micromanipulation: milliDelta Robot



The milliDelta: A High-Bandwidth, High-Precision, Millimeter-Scale Delta Robot

Hayley McClintock*, F. Zeynep Temel*,
Neel Doshi, Je-Sung Koh, Robert J. Wood



HARVARD
John A. Paulson
School of Engineering
and Applied Sciences

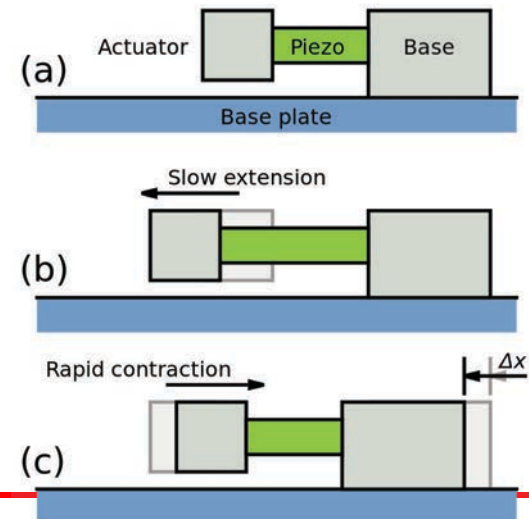
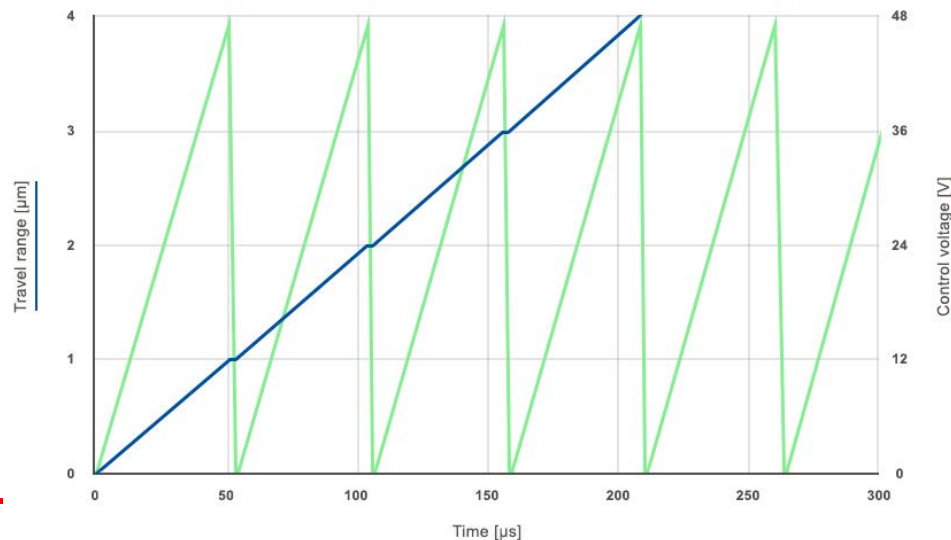
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for Biologically Inspired Engineering

*Both authors contributed equally

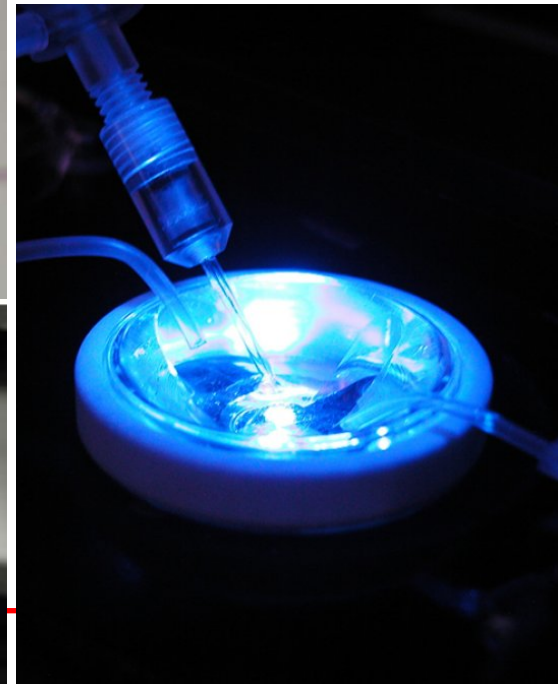
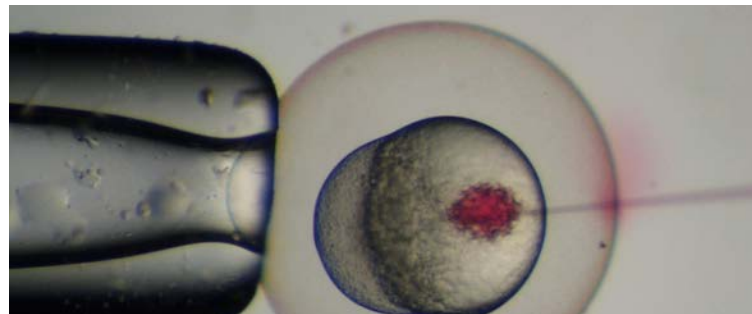
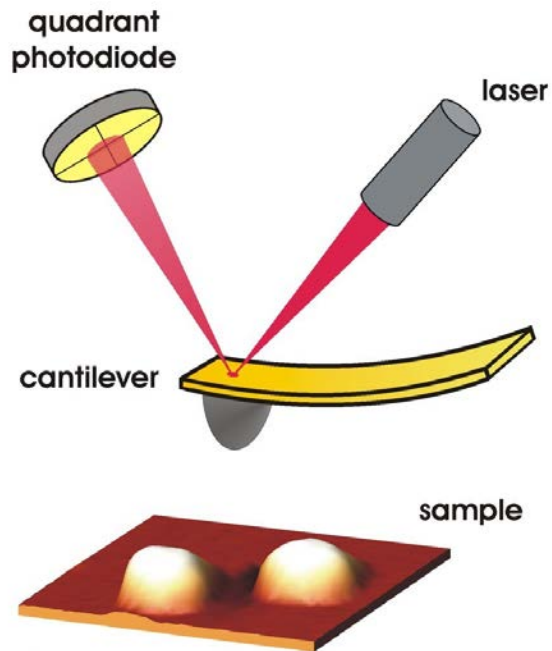
Piezo Motors

Video

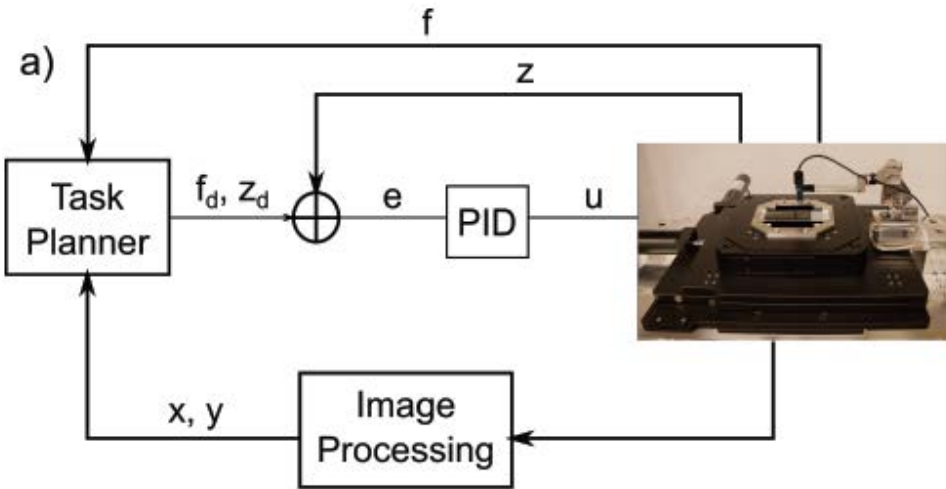
- Stick-slip mechanism (impact drive)
- A platform makes frictional contact with the ground, and on the platform is a piezo element and attached mass
- Reaction forces resulting from rapid acceleration of the mass by the piezo cause the platform to make a step (slip)
- The mass is then slowly retracted so that friction prevents return motion of the platform (stick)
- Saw-tooth shape signal (slow expansion, fast contraction)



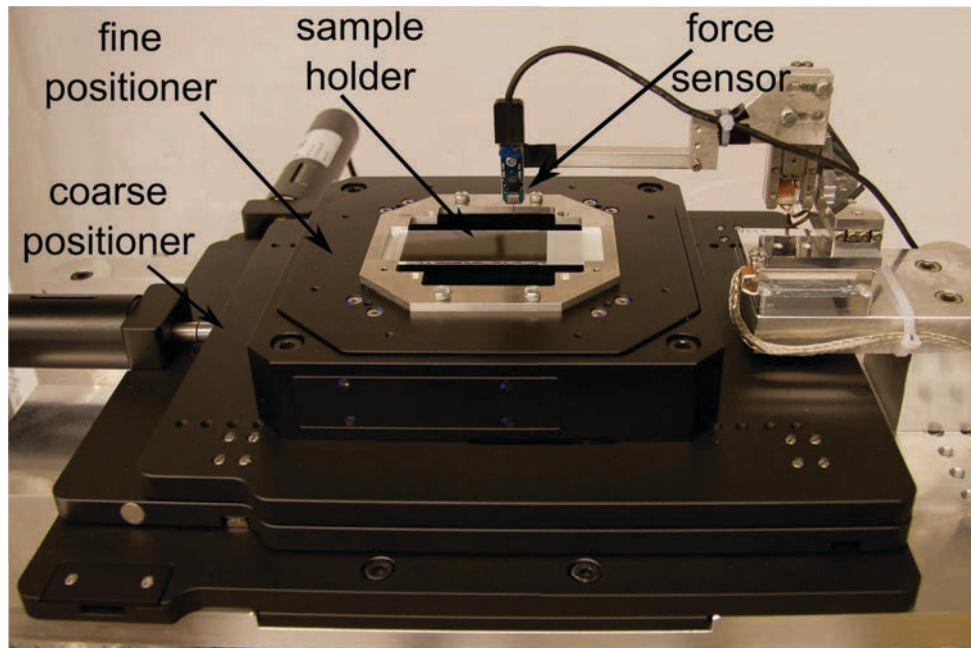
Robotic Biomanipulation using Tethered Microtools



Real-time Cellular Force Microscopy



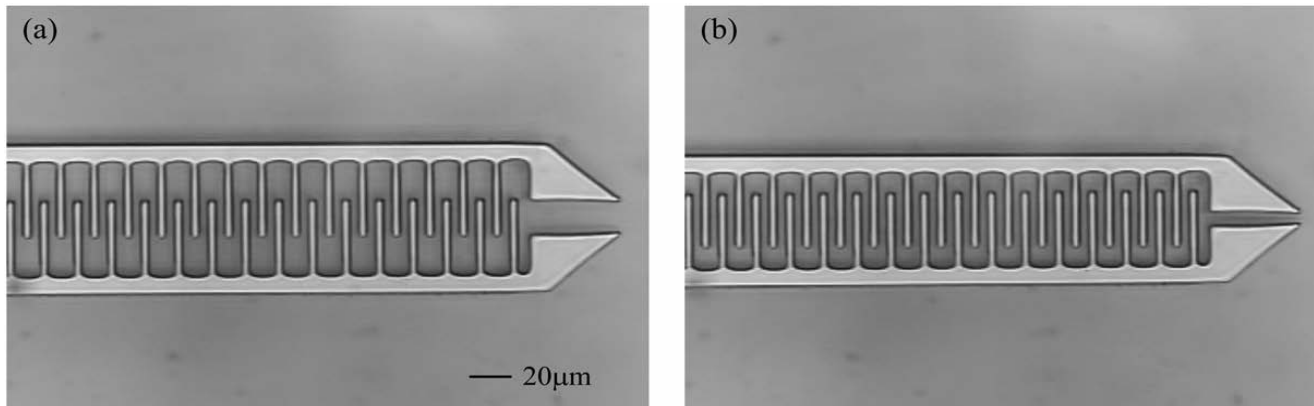
- Capacitive Force Sensors
- Automation for the stage (sample), micromanipulator and imaging system
- Different imaging modalities (phase-contrast, fluorescence, FRET)
- Algorithms for imaging, planning, control and manipulation



D. Felekis and **M.S.Sakar et.al.**, *IJRR*, 2015

Electrostatics

- Relatively long range interactions at microscale
- Induced by ionization or polarization
- Major function of and source of failure for MEMS devices



Electrostatic Actuation

- Electrostatic force between charged plates
- Electrostatic fields can exert great forces across very short distances
- High efficiency but low power density

Method	Efficiency	Speed	Power density
Electrostatic	Very high	Fast	Low
Electromagnetic	High	Fast	High
Piezoelectric	Very high	Fast	High
Thermomechanical	Very high	Medium	Medium
Phase change	Very high	Medium	High
Shape memory	Low	Medium	Very high
Magnetostrictive	Medium	Fast	Very high
Electrorheological	Medium	Medium	Medium
Electrohydrodynamic	Medium	Medium	Low
Diamagnetism	High	Fast	High

Electrostatic Force

- Energy stored in an electric field

$$W = \frac{1}{2} CV^2 = \frac{1}{2} \frac{\epsilon_r \epsilon_0 abV^2}{d} = \frac{\epsilon AV^2}{2d}$$

Where a is the length, b is the height of the finger and d is the gap between plates.

- Micron-sized air gap: $E \leq 10^8 \text{ V/m} \rightarrow W = 44 \text{ kJ/m}^3$
- Electrostatic Attractive Force (perpendicular to the plates)

$$F = \frac{\partial W}{\partial d} = \frac{\epsilon AV^2}{2d^2}$$

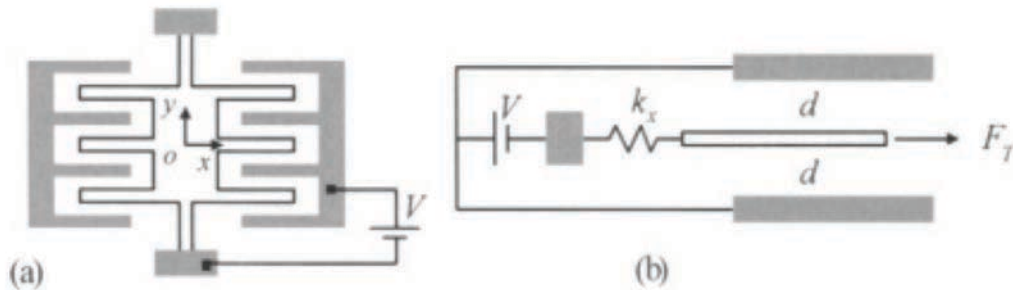
Scaling Analysis: Electrostatic Actuators

- Assuming that all dimensions scale linearly proportional to L
- Volume scales with L^3
 - Inertia, weight, heat capacity, and body forces
- Surface area scales with L^2
 - Friction, heat transfer, surface forces

- Assuming that the voltage and d is constant, F scales as $\sim L^2$
- If we scale the gap as well then F remains the same

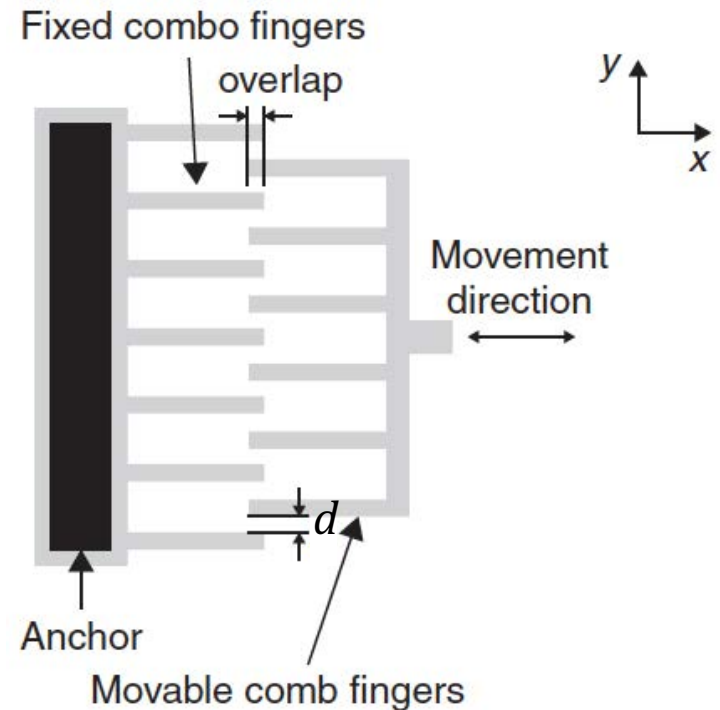
Comb Drive

- Make use of tangential forces for driving
- The stationary electrodes are arranged symmetrically on both sides of each moving finger so that normal forces cancel out



$$F_N = \frac{\epsilon AV^2}{2d^2} \quad F_T = \frac{\epsilon bV^2}{2d}$$

where b is the height of the finger.



Comb Drive

- For a set of n capacitors the total driving force is given by

$$F_T = n\varepsilon \frac{bV^2}{d}$$

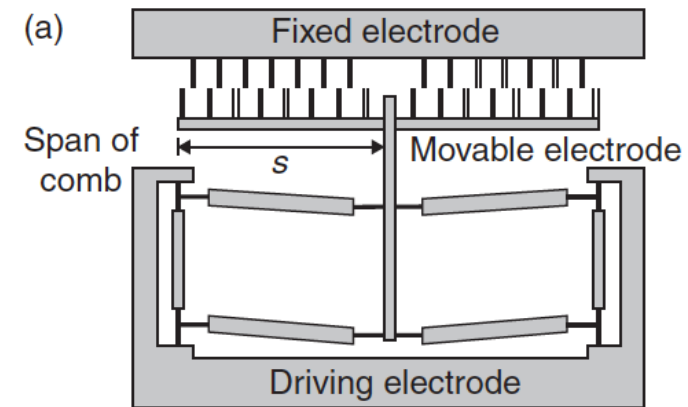
- The restoring force is

$$F_R = kx = 4 \frac{Eb w^3}{l^3} x$$

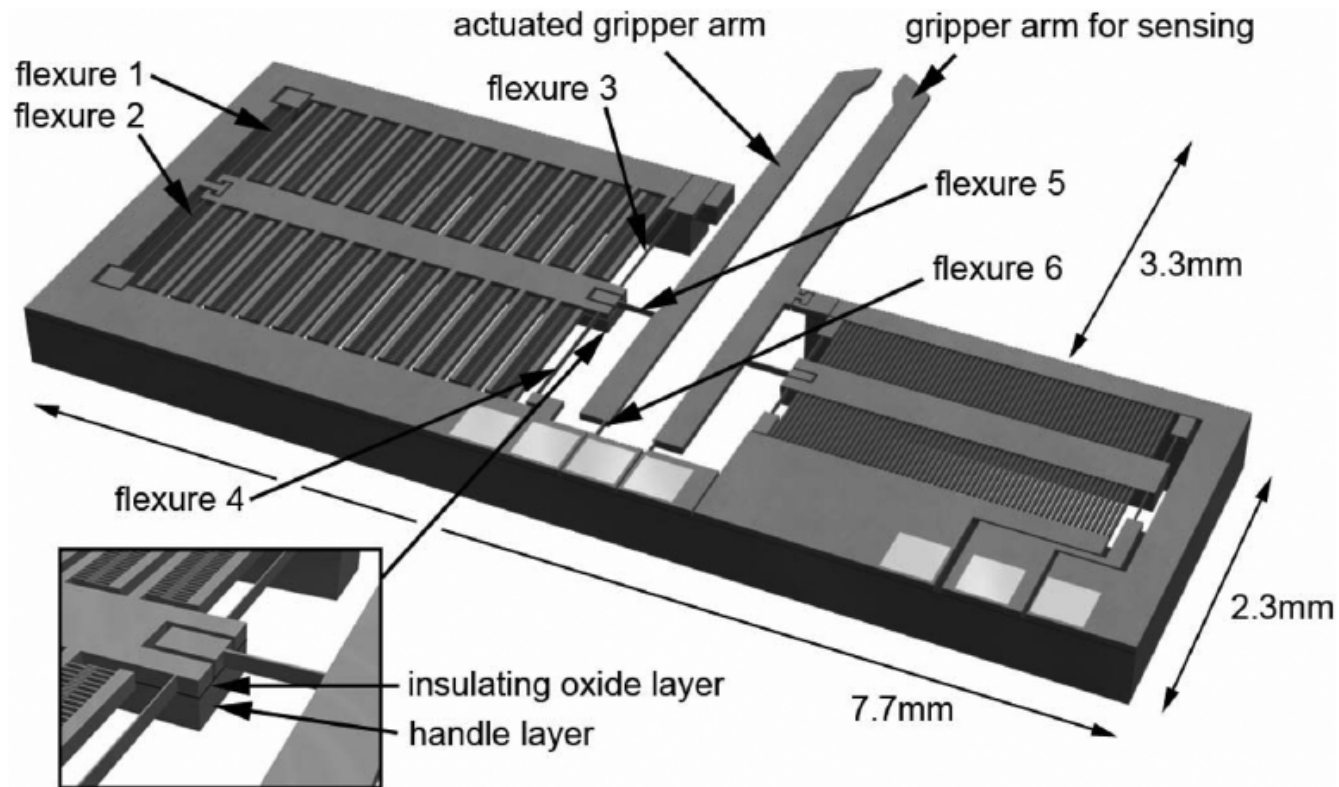
where w is the width and l is the length of the flexure

- The equation of motion

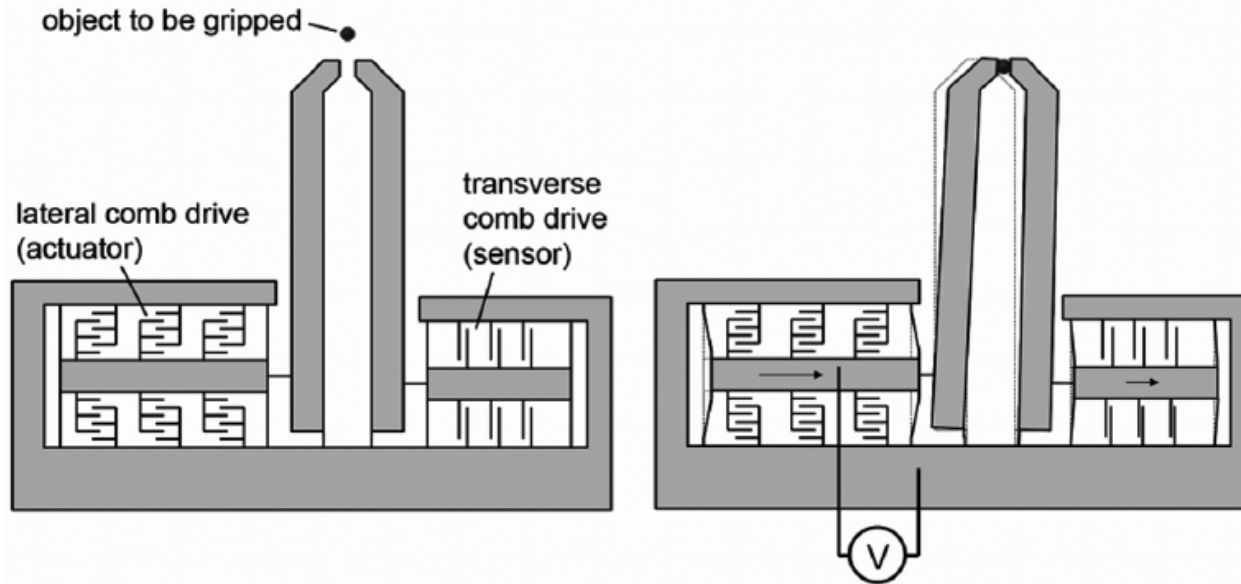
$$F_T - F_R = n\varepsilon \frac{bV^2}{d} - 4 \frac{Eb w^3}{l^3} x = 0$$



Capacitive Force Sensors and Grippers ([video](#))



Capacitive Force Sensors and Grippers



	50 μm opening	100 μm opening	200 μm opening
actuation voltage	0-110V	0-150V	0-150V
gripper opening range	0-50 μm	0-100 μm	100 μm -200 μm
flexure dimensions	900 μm x 10 μm x 50 μm		
electrode dimensions	100 μm x 5 μm x 50 μm		
gap spacing between electrodes	5 μm		

Capacitive Force Sensors and Grippers



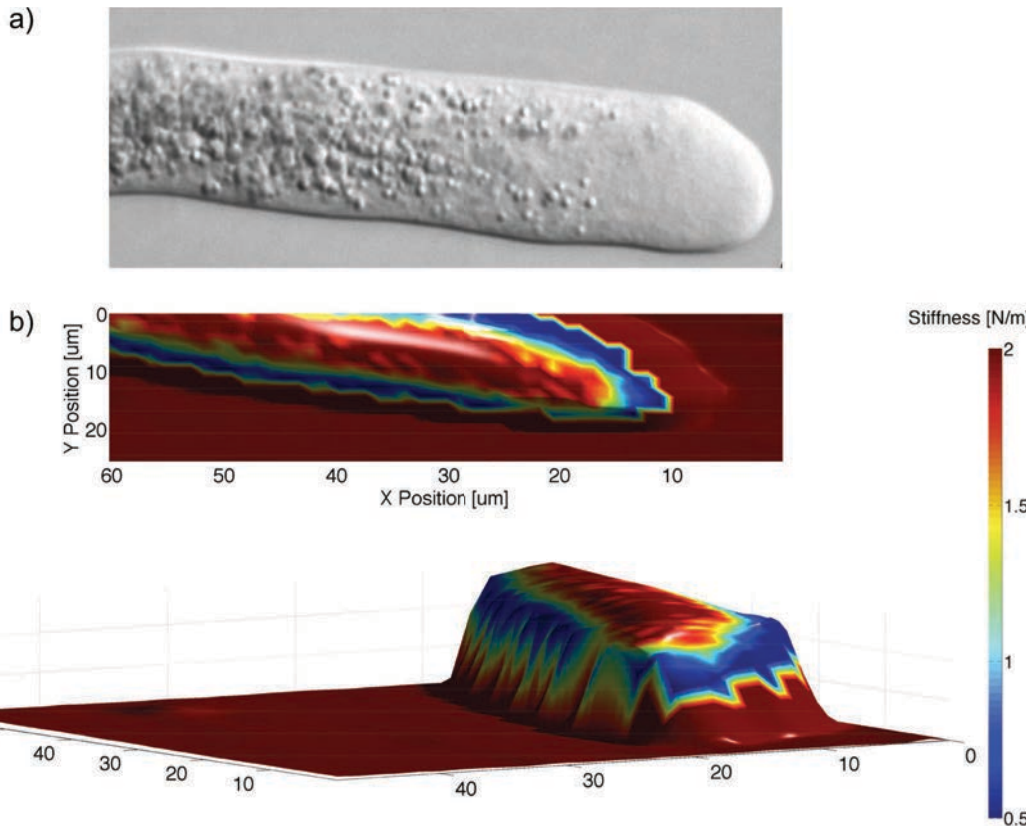
	150 μ m flexure	300 μ m flexure
linear range	$\pm 2800\mu\text{N}$	$\pm 360\mu\text{N}$
sensitivity*	0.55mV/ μ N	4.41mV/ μ N
resolution	520nN	70nN

gripper opening range	0-50 μ m	0-100 μ m	100 μ m-200 μ m
flexure dimensions	900 μ m x 10 μ m x 50 μ m		
electrode dimensions	100 μ m x 5 μ m x 50 μ m		
gap spacing between electrodes	5 μ m		

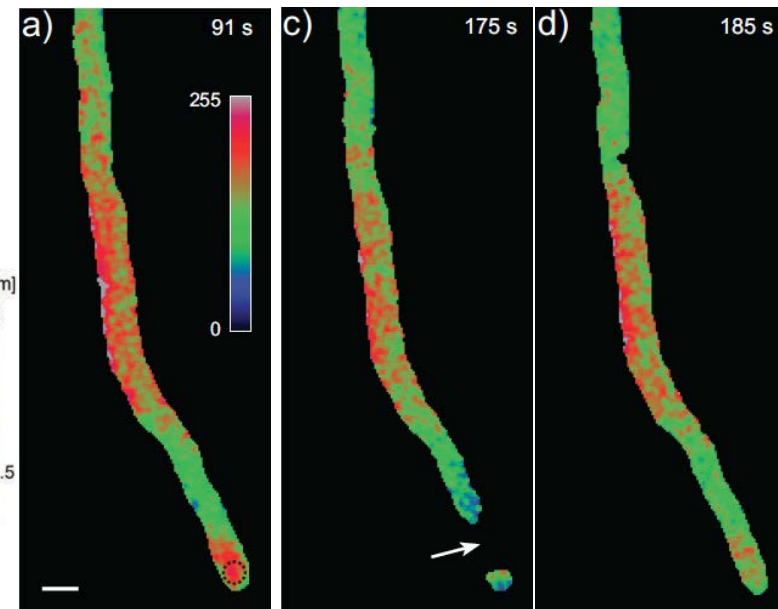
Real-time Cellular Force Microscope

- Pollen tubes: Fastest growing cells
- Turgor pressure, shape, cell wall stiffness, mechanosensing

Topography Maps and Stiffness Measurements



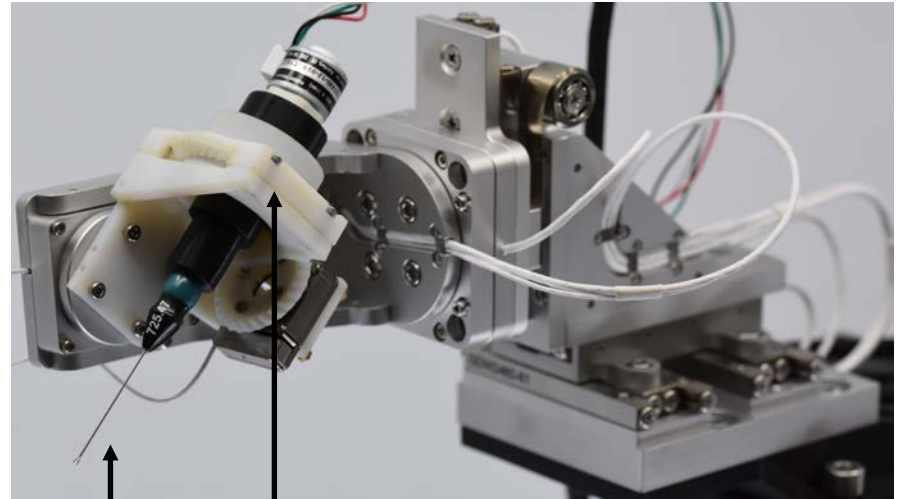
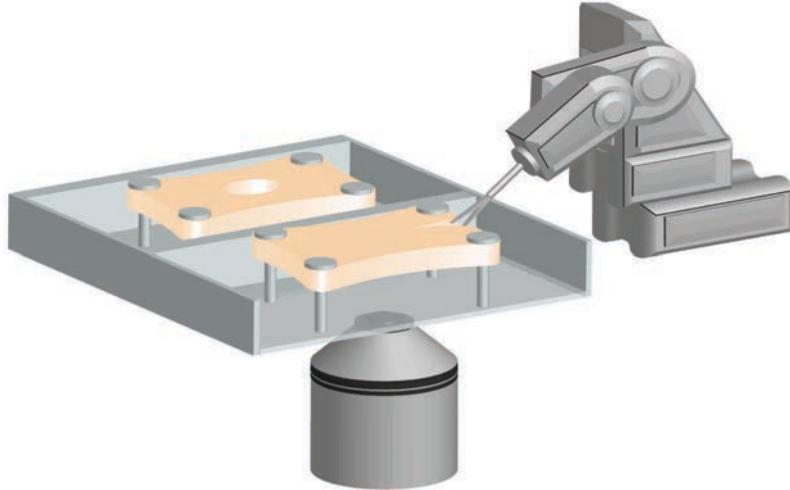
Compression and Calcium Imaging



D. Felekis and **M.S.Sakar** *et.al.*, *IJRR*, 2015

Robotic Microsurgery

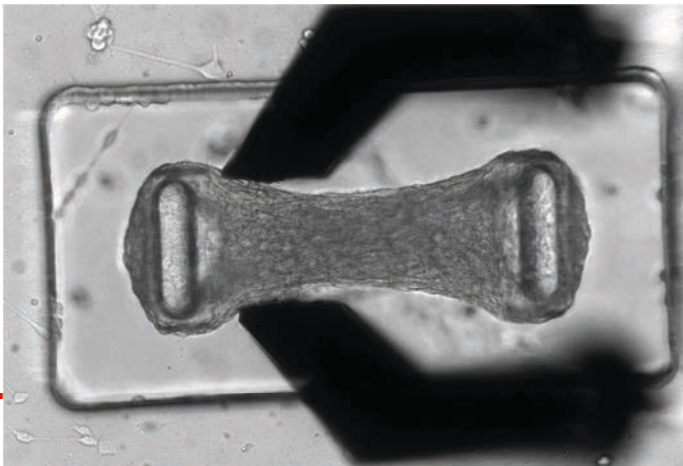
- Actuated tools: Scissors, forceps
- Implantation of microfabricated structures
- Visual servoing and automation



Six degree-of-freedom
with submicron precision

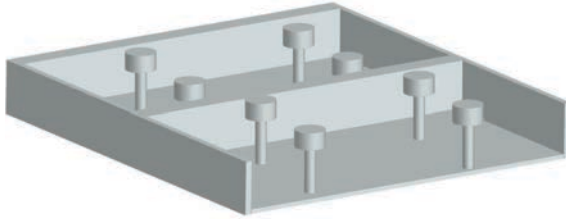
Motorized actuation

Quick change of
microsurgical tools

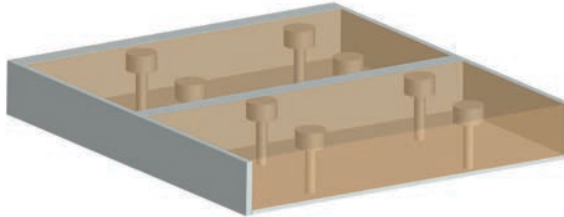


Microfabricated tissue gauges

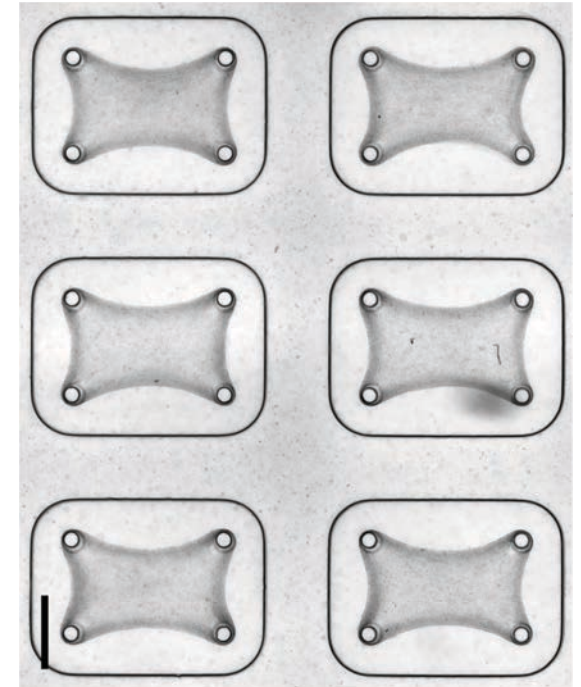
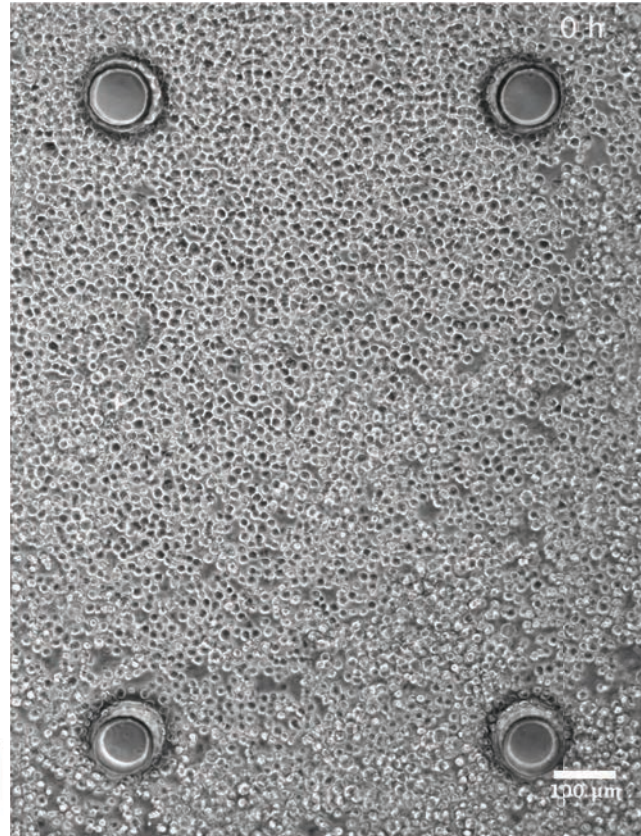
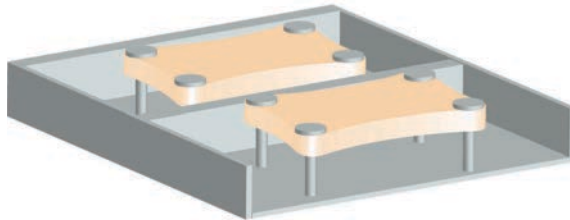
PDMS device



Seeding cell/collagen suspension

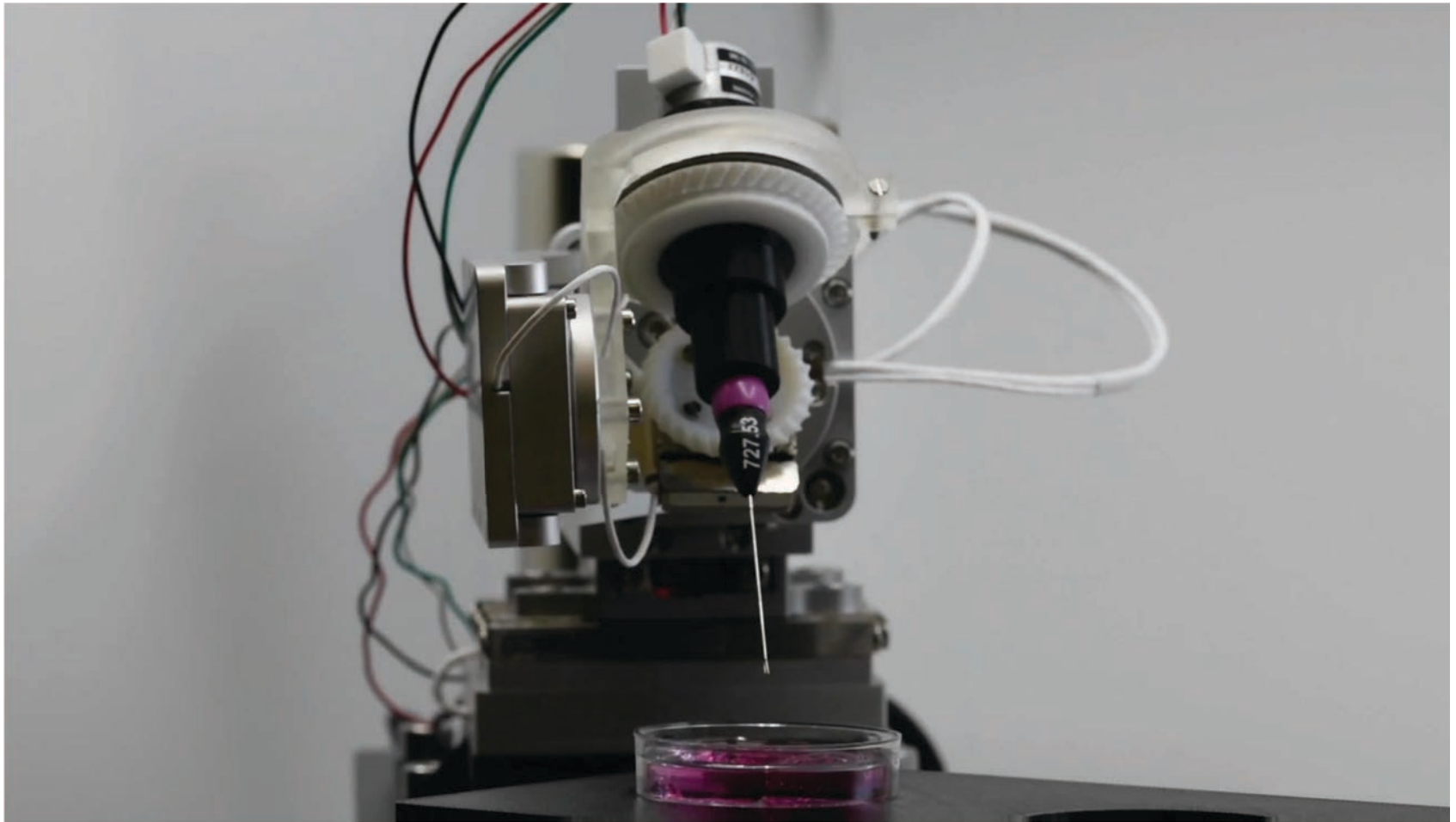


Microtissue formation

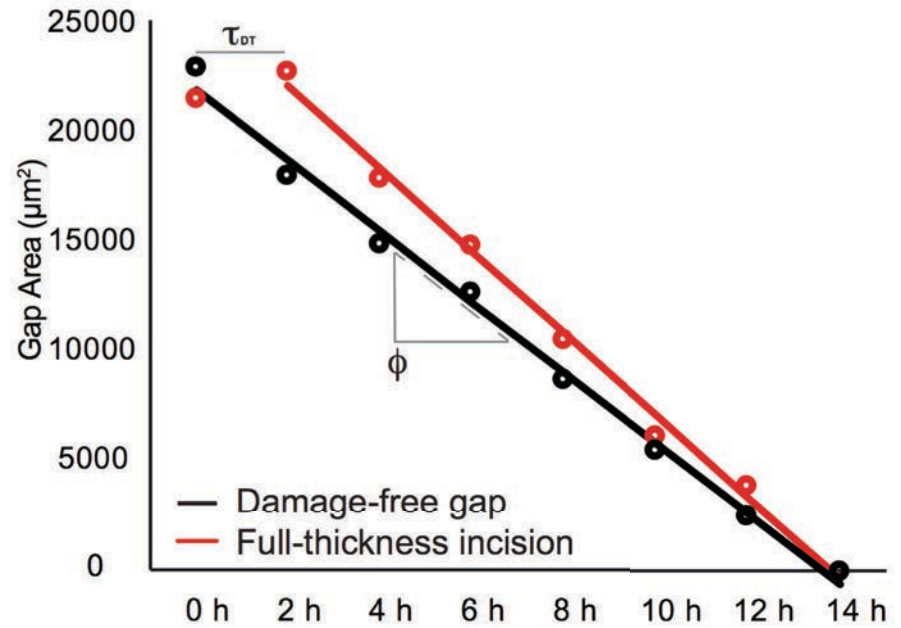
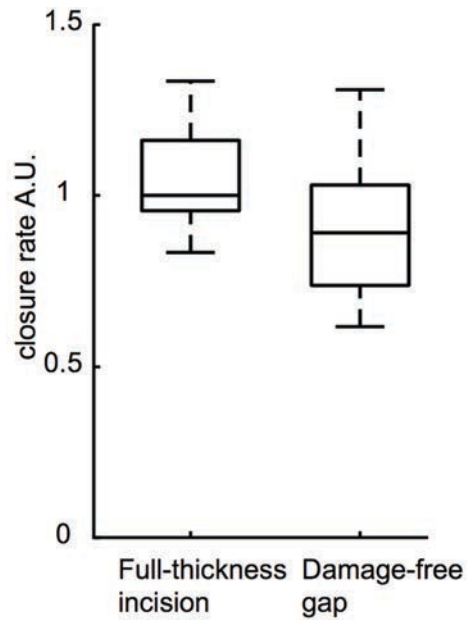
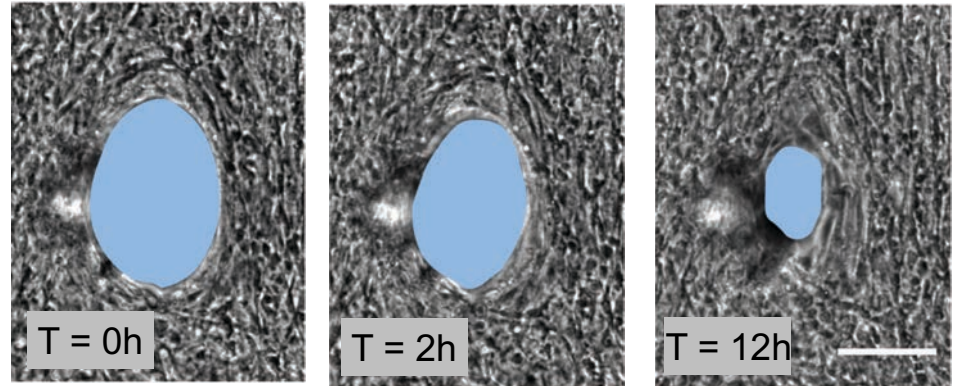
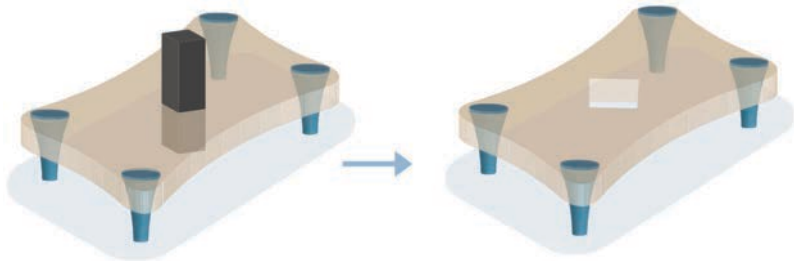


3T3 + reconstituted collagen I

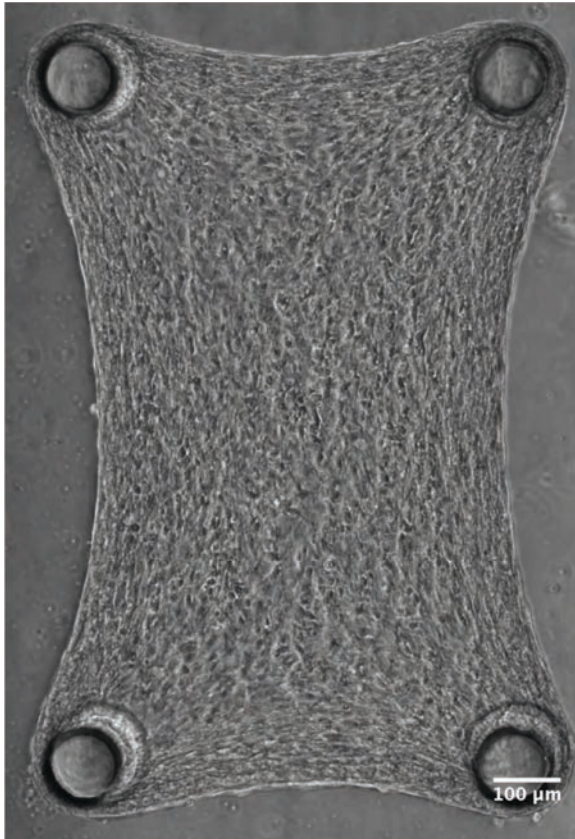
Robotic Microsurgery



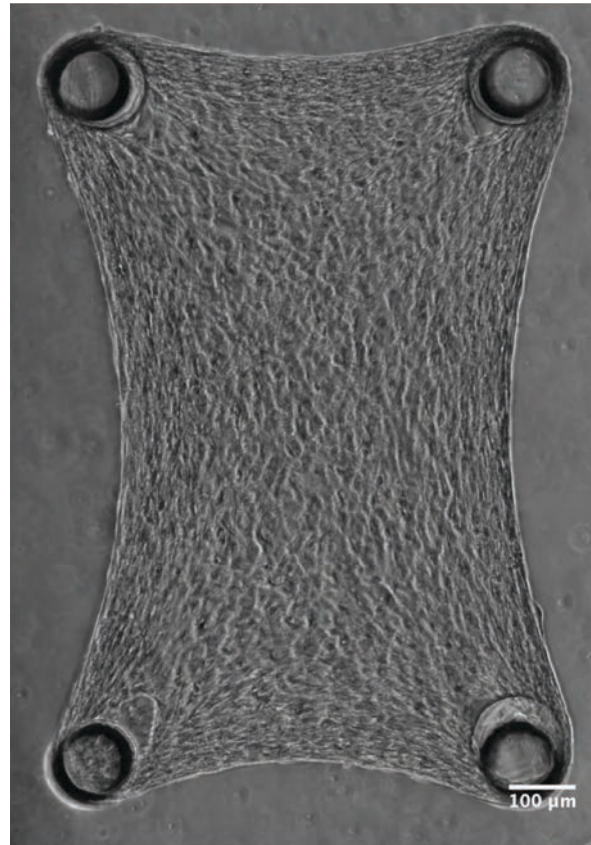
Microscale implants: Damage-free gaps



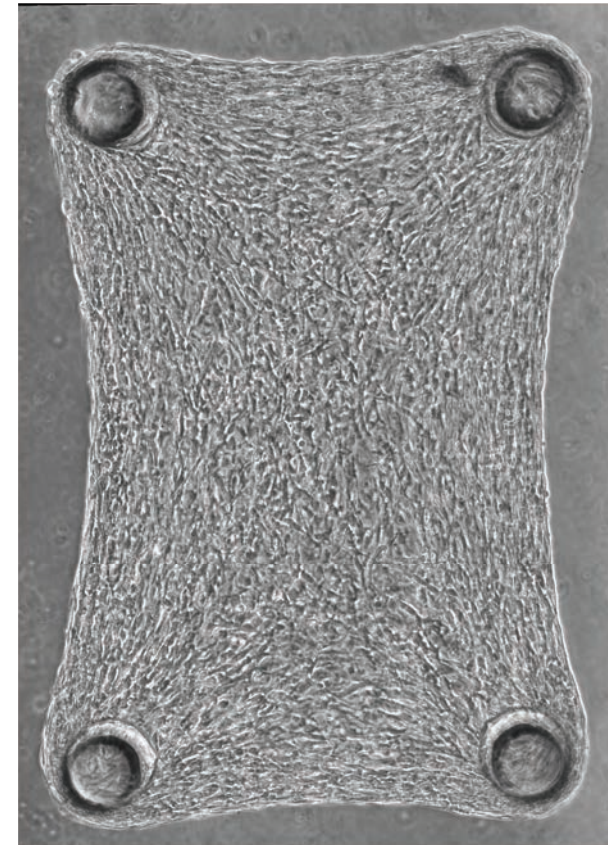
Plastic Deformation



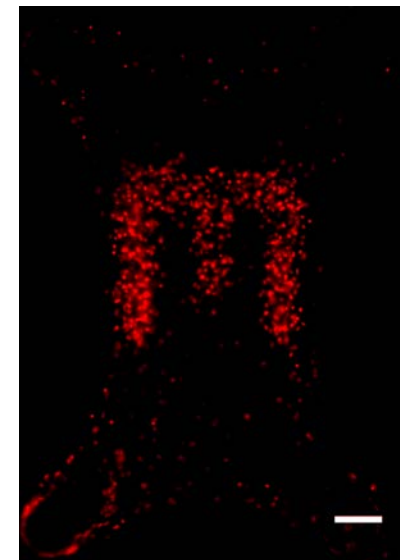
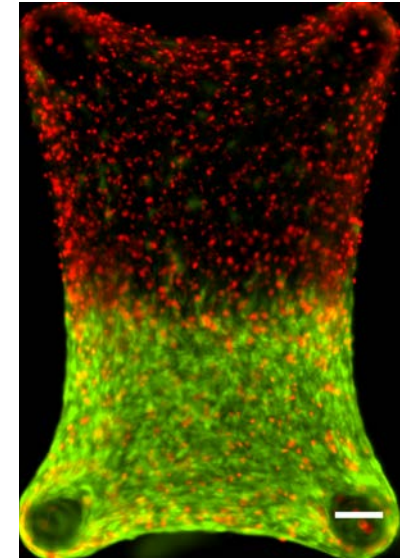
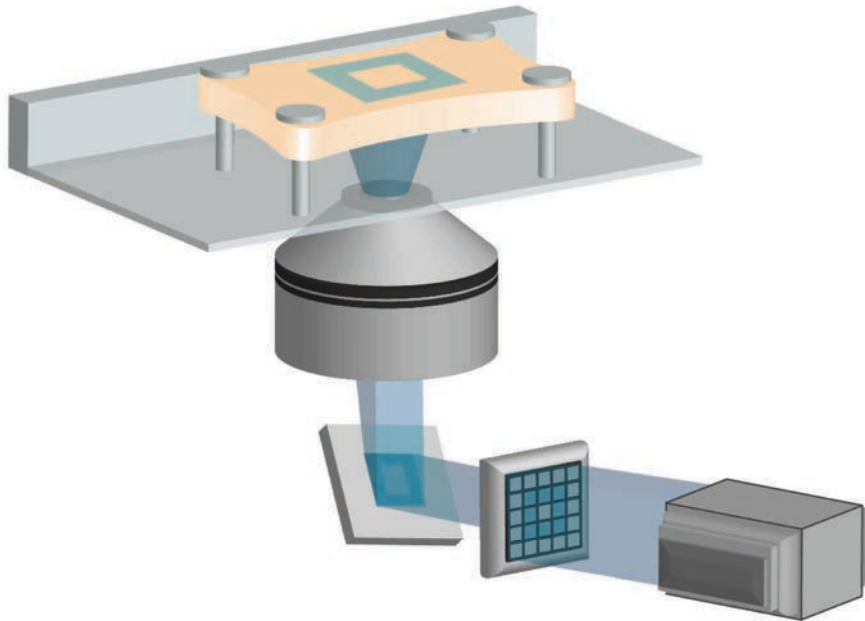
Reconstructive Surgery



Stitching



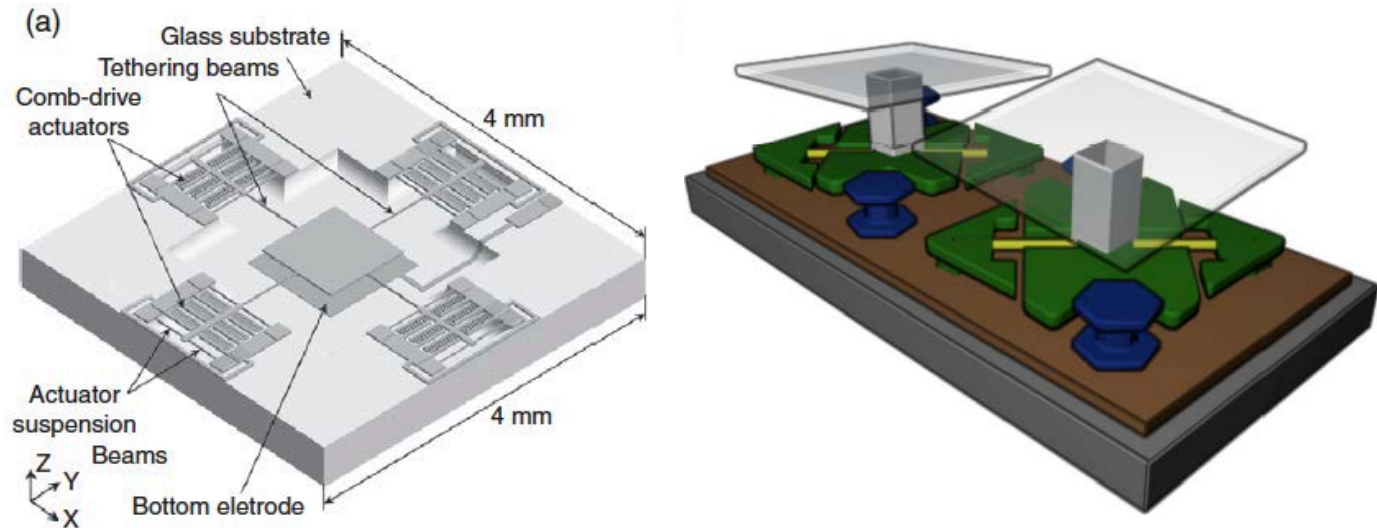
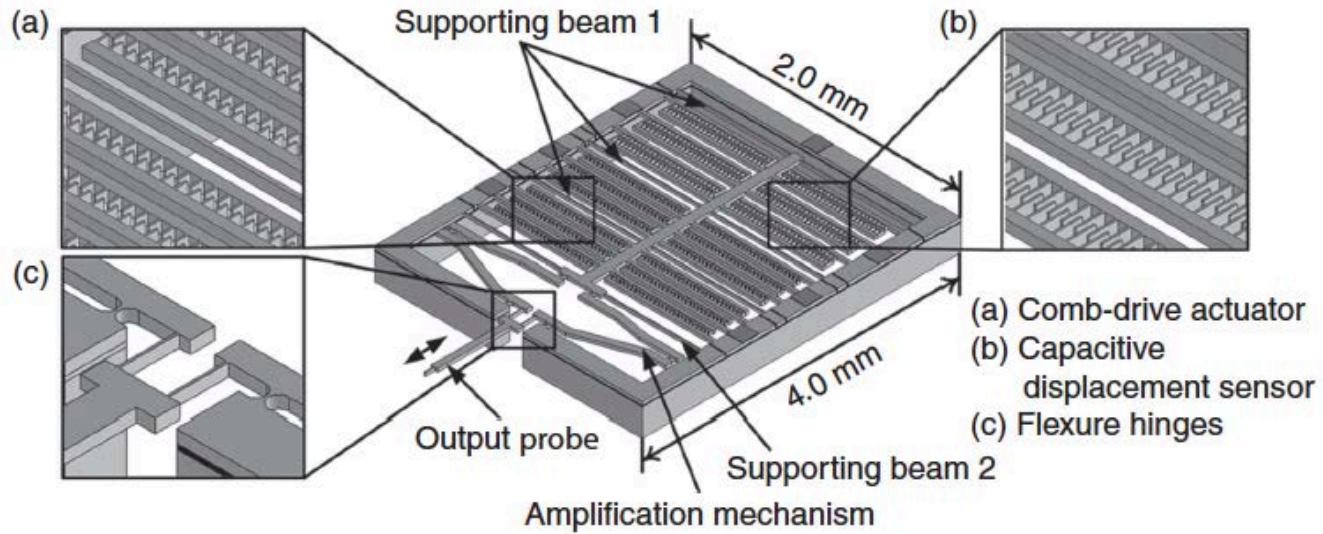
Decellularized scaffold



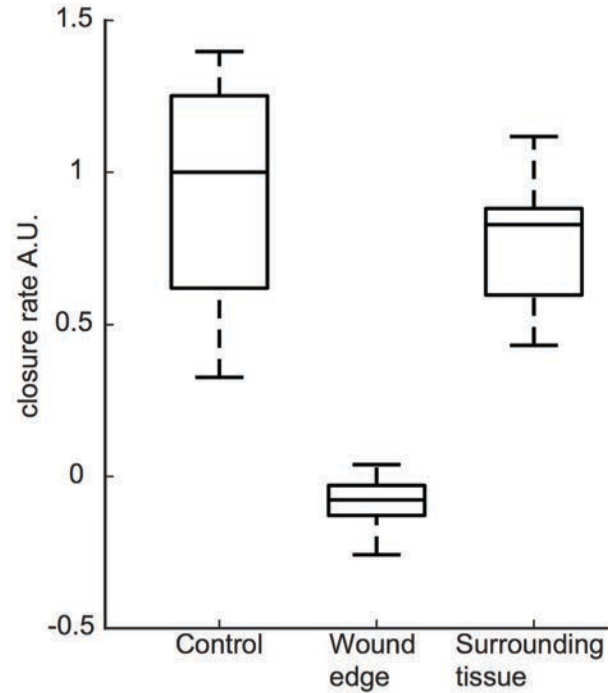
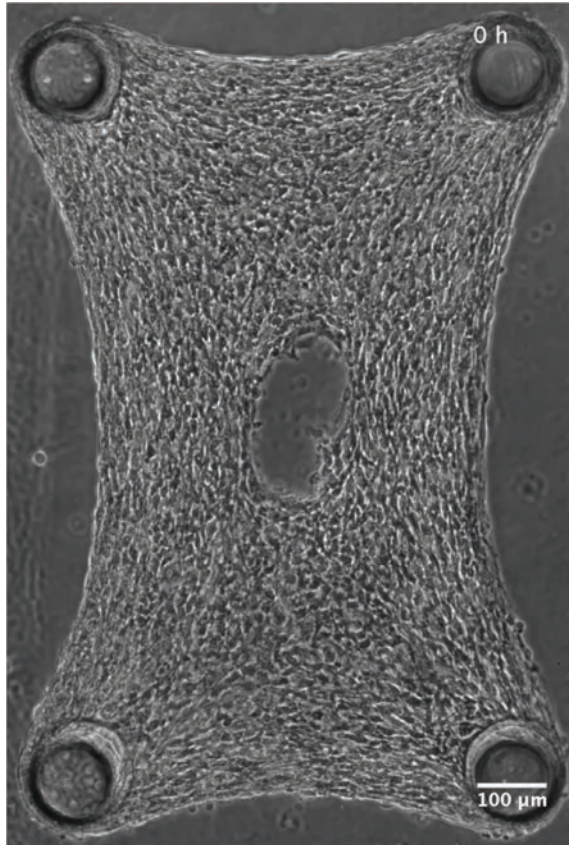
Programmable digital mirror device
freezes cells within pre-defined regions

- Extension to optogenetics (RhoA)

Digital Mirror Device

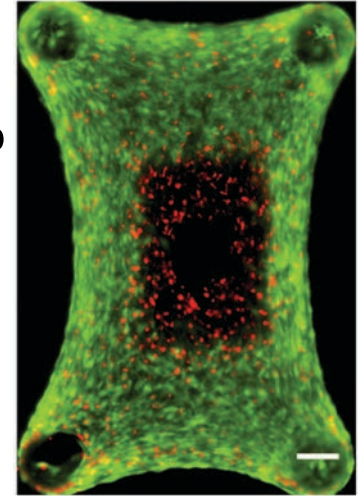


Closure is organized by the front cells

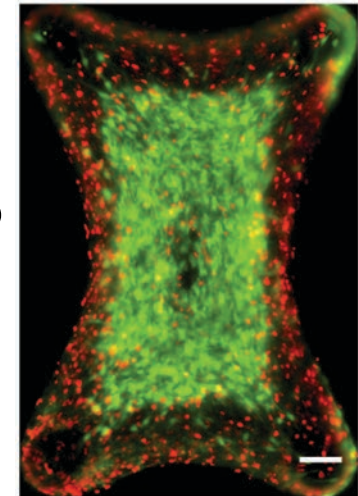


EthDIII / Calcein AM

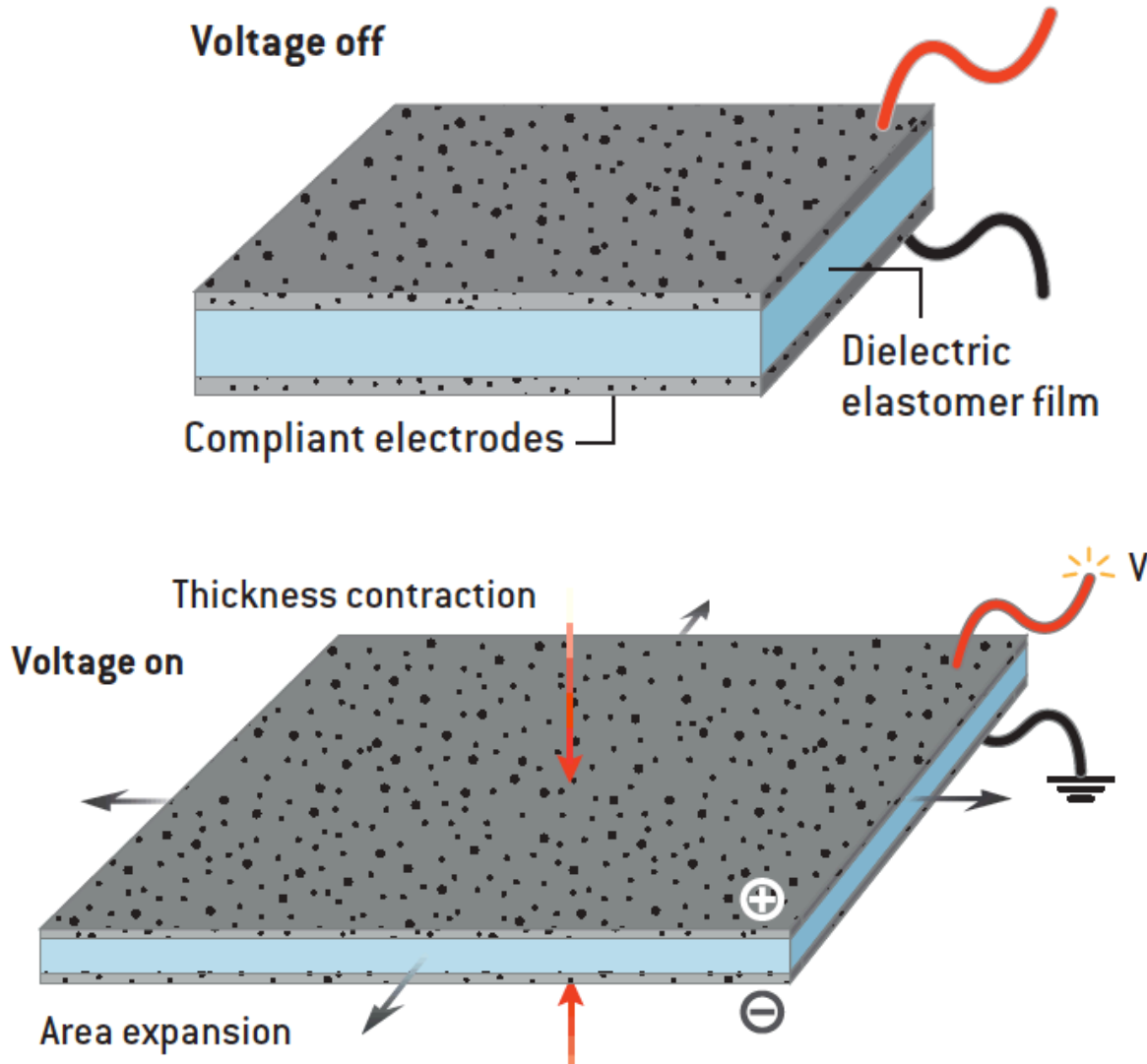
wound edge



surrounding tissue



Dielectric Elastomers



Electric-field-actuated Polymers

$$p = \epsilon_r \epsilon_0 E^2 = \epsilon_r \epsilon_0 (V/t)^2$$

where p is the effective compressive stress, ϵ_r is the relative dielectric constant of the material, ϵ_0 is the permittivity of the free space, E is the electric field (V/m), V is the applied voltage, t is the film thickness.

- Effective compressive stress is twice the stress normally calculated for two rigid, charged capacitor plates.
 - In an elastomer, the planar stretching is coupled to the thickness of compression (constant volume)
 - Compressive stress has compressive and tensile components
- For low strains (<20%) the thickness strain can be approximated as

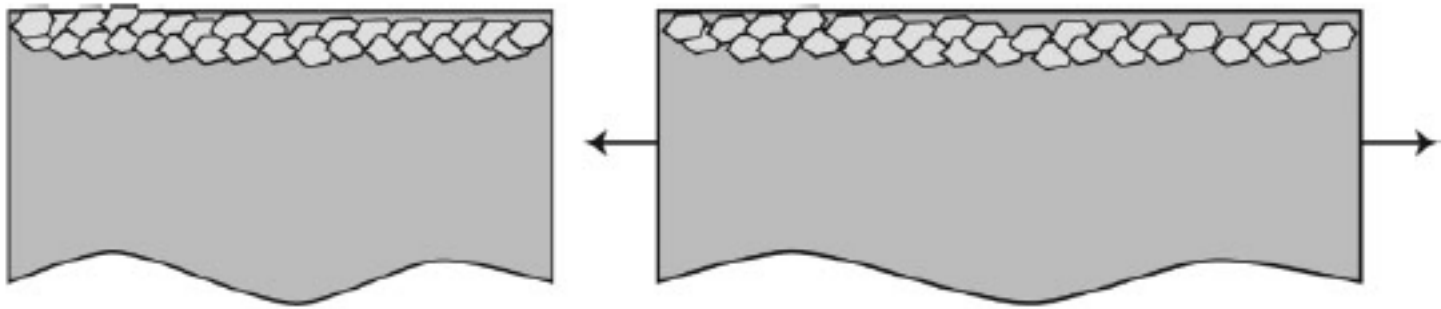
$$s_z = -\frac{p}{Y} = -\epsilon \epsilon_0 E^2 / Y \rightarrow \text{Elastic modulus}$$

High-speed, giant strain actuators

- Stanford Research International (SRI) published a paper in 2000.
- Artificial muscles (light weight, quiet operation, high strain and efficiency)
- Low elastic modulus (1 MPa) and high dielectric strength (>100 MV/m)
- Up to kHz range bandwidth
- Low viscoelastic losses and low electrical leakage
- Electromechanical coupling is 60-80% for acrylic, 90% for elastomer
- Up to 380% strain (typical 10-100%), up to 7.2 MPa stress, elastic energy density up to 3.4 J cm^{-3}
- On the order of 1 kV for electrode separation of 10 to 100 μm
- **Key innovation:** pre-strain

Compliant Electrodes

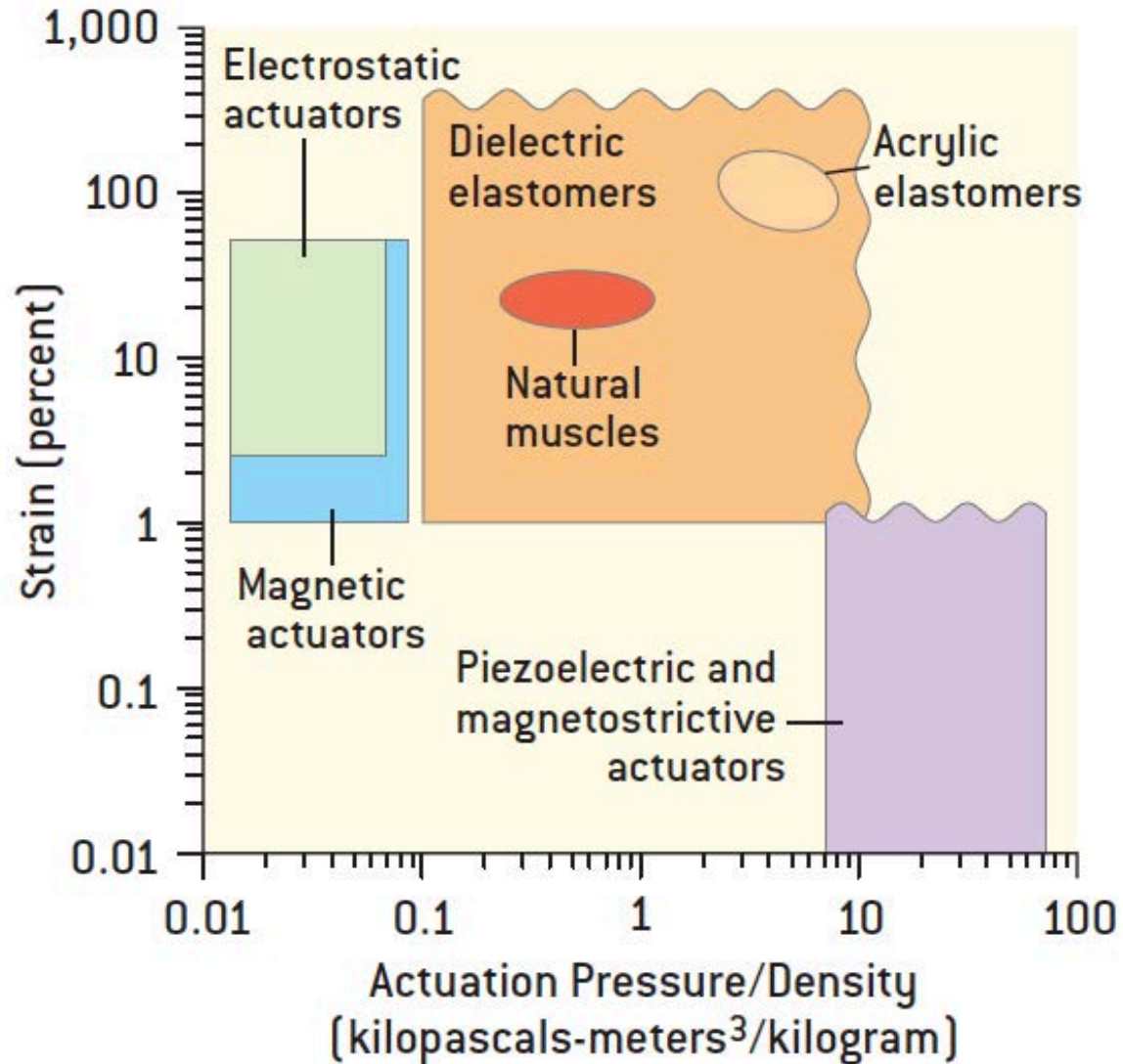
- Conductive paste (carbon-impregnated grease or silver paste)
- Spin-coated conductive rubber
- Sprayed graphite particles
- Carbon sheets
- Compliance with high conductivity



Performance

Property	Dielectric elastomers ^[154–157]
Stimulus	Voltage/electric field
Amplitude of stimulus	100–150 MV m ⁻¹ (breakdown <420 MV m ⁻¹)
Areal strain [%]	<380
Thickness strain [%]	<79
Stress [MPa]	<7.2
Work density [MJ m ⁻³]	<3.5
Tensile strength [MPa]	<7.2
Electromechanical coupling efficiency [%]	<90
Dielectric constant	2–10
Bandwidth	<1 kHz
Efficiency [%]	<90
Cycle life	>10 ⁶

Performance comparison



Shape Memory Alloys

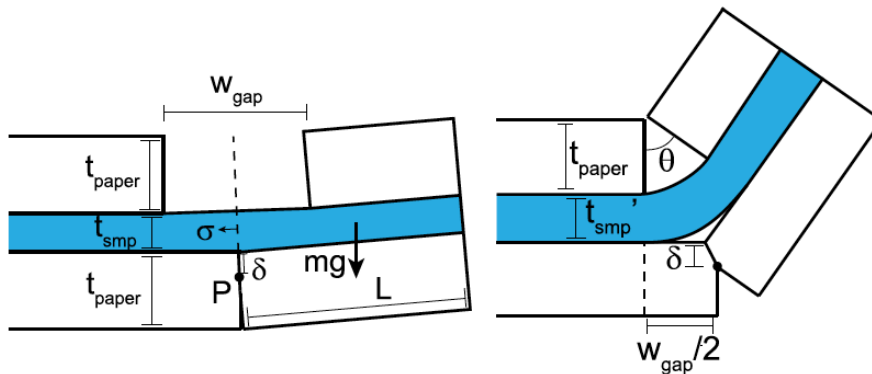
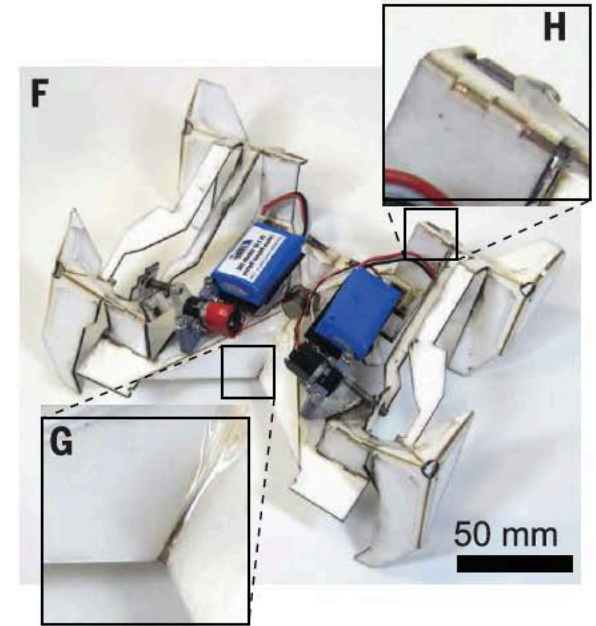
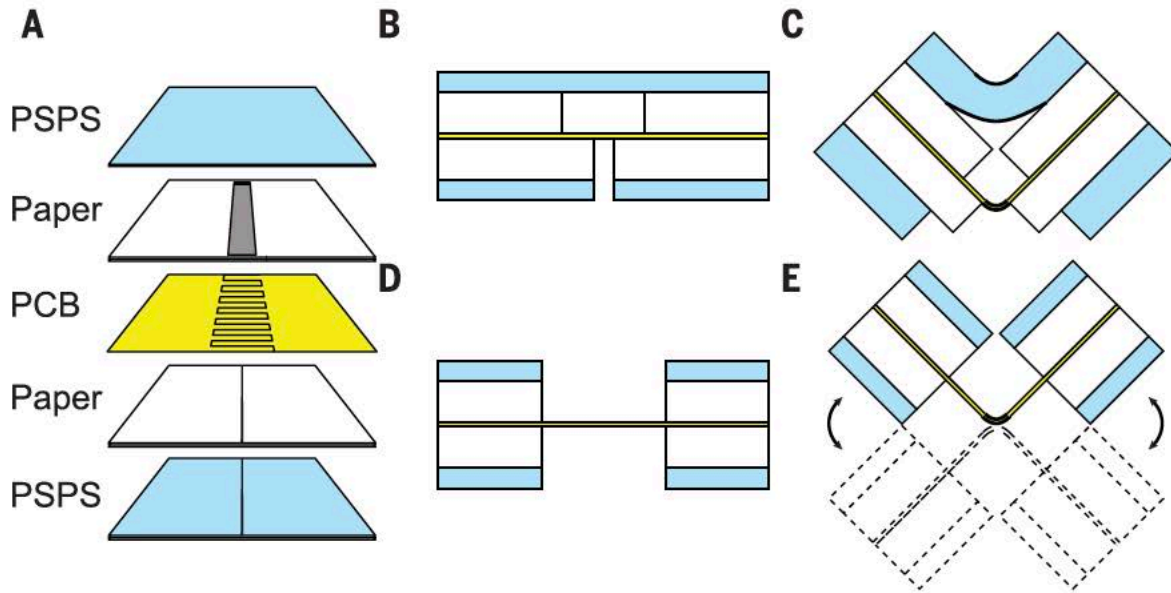
- Discovery in 1932 by Arne Olander.
- Alloys of nickel-titanium (e.g., NiTi or Nitinol) outperforms most other materials such as iron or copper-based alloys
- The shape memory property of NiTi alloy was discovered in 1960s in the Naval Ordnance Laboratory, hence the name Nitinol.
- Reversible transition between two phases, martensite (low-temp) and austenite (high-temp)
- Martensitic phase is yield-able (shapeable, plastic deformation)
- Deformations of the martensitic phase, occurring above a critical stress, are recovered completely during the transformation at austenite phase
- Fabrication conditions determine the shape-memory effect and phase transition temperatures

Actuation performance

Limitations: thermal hysteresis in the strain, low cycle life, high fabrication cost, relatively low efficiency

Property	Thermally activated SMAs
Stimulus	Heat (Joule heating)
Amplitude of stimulus	$\approx 4 \text{ V}$ ($>> 4 \text{ V}$ in short pulse excitation)
Strain [%]	< 8.5
Stress [MPa]	< 700
Strain rate [% s ⁻¹]	< 300
Work density [MJ m ⁻³]	< 10
Power density [MW m ⁻³]	< 30
Tensile strength [MPa]	< 1900
Bandwidth [Hz]	< 3 (< 35 in a bending actuator) ^[80]
Efficiency [%]	$< 16\%^a$
Cycle life	300 (@ $\approx 5\%$) to 10^7 (@ $\approx 0.5\%$)

Self-folding Machine



Torque

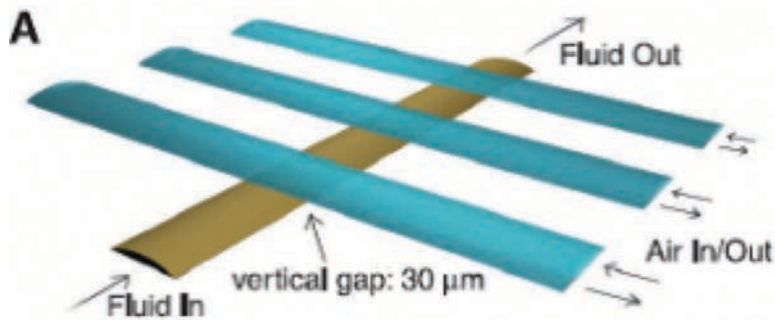
$$T = \frac{\sigma_a}{1 - \nu} W t_{smp} \left(\frac{t_{smp}}{2} + \delta \right)$$

Self-Folding Crawler

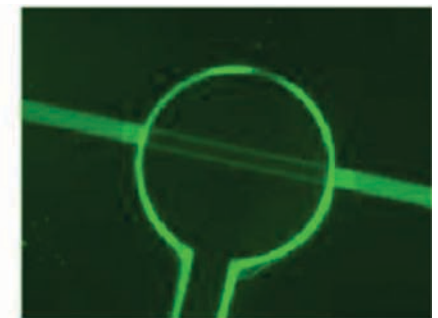
Harvard Microrobotics Lab

Pneumatic Actuators

- Pneumatics can be miniaturized (microfluidics)
- Like dielectric elastomer and SMAs, resolution and bandwidth are limited



Quake Valve **Off**



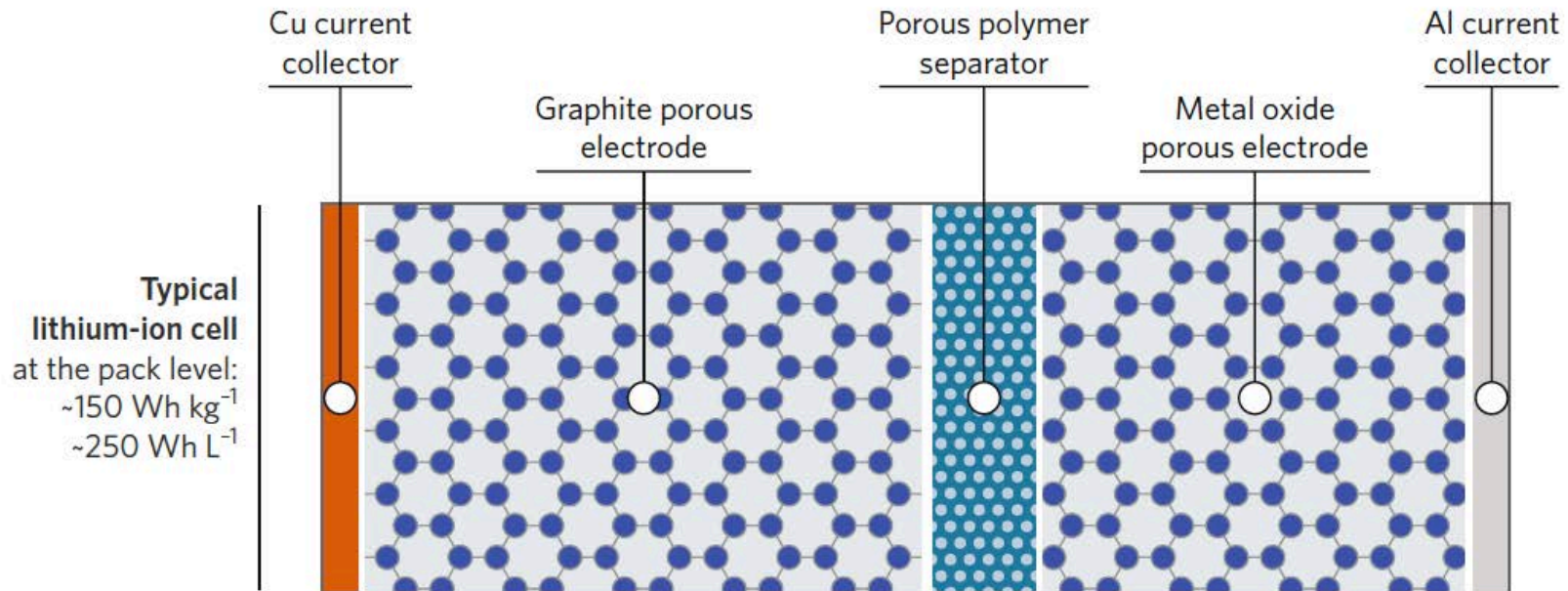
Quake Valve **On**

Challenges

- How do we get rid of cables or tubes?
 - From tethered to untethered
- Working in fluid or on rough substrates
- Working against load (brittle vs tough)
- Manufacturing at small scale
- Voltage and current
 - Electroactive materials: high voltage
 - Shape memory alloys: high current

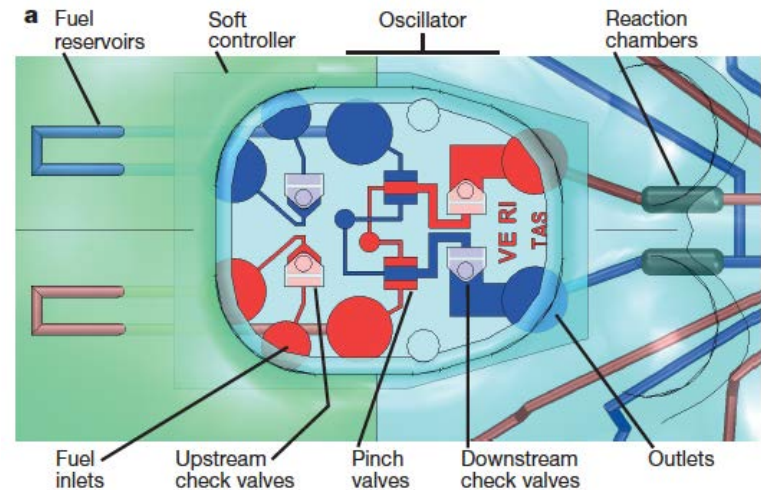
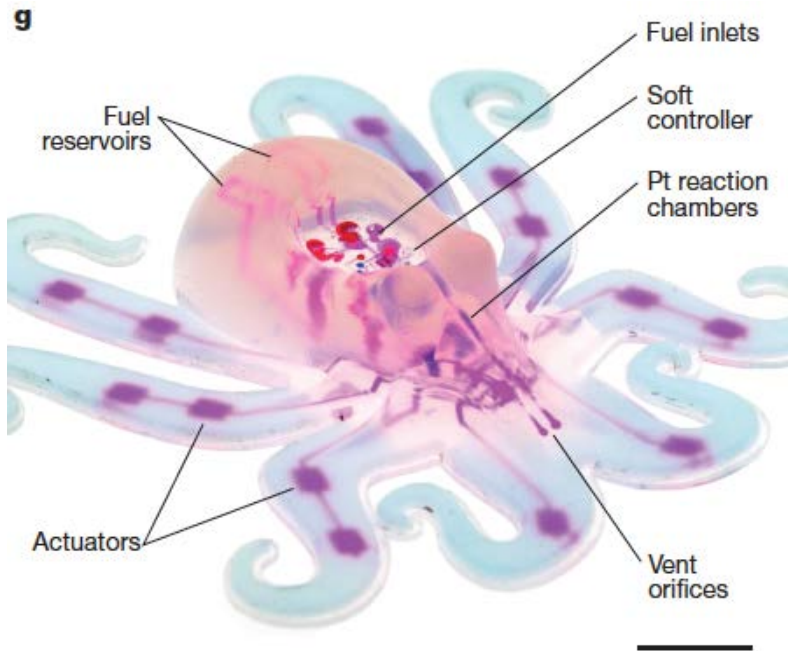
Scaling of Battery Technology

- Chemical energy into electrical energy (solid, liquid, composite electrolyte)
- Energy density (surface area of electrode, thickness of separator)
- Electrochemistry is dark magic (mass transport, thermodynamics, materials science)
- Research in 2D materials (graphene, MoS₂) and organic materials



Scaling of Actuators: Pneumatic Actuators

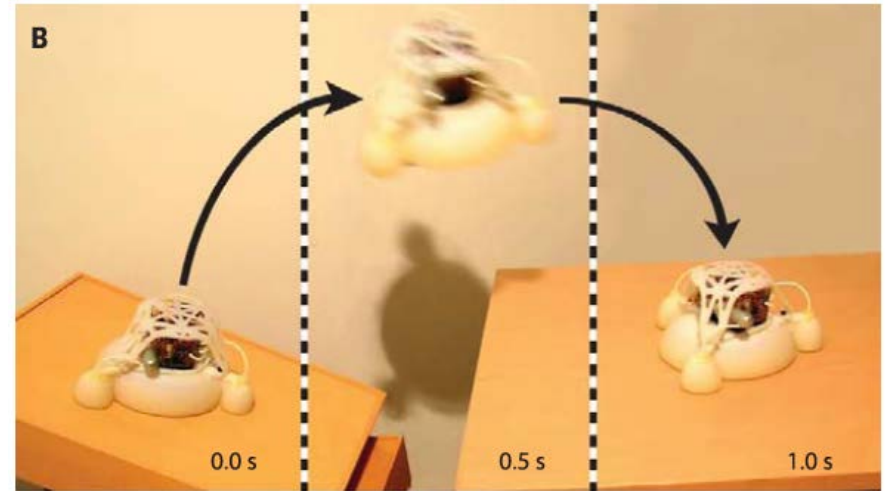
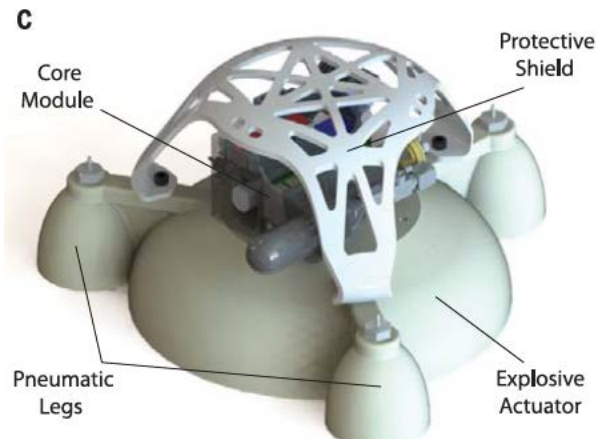
- On-board generation of gas pressure?



Wehner et.al., Nature, 2016

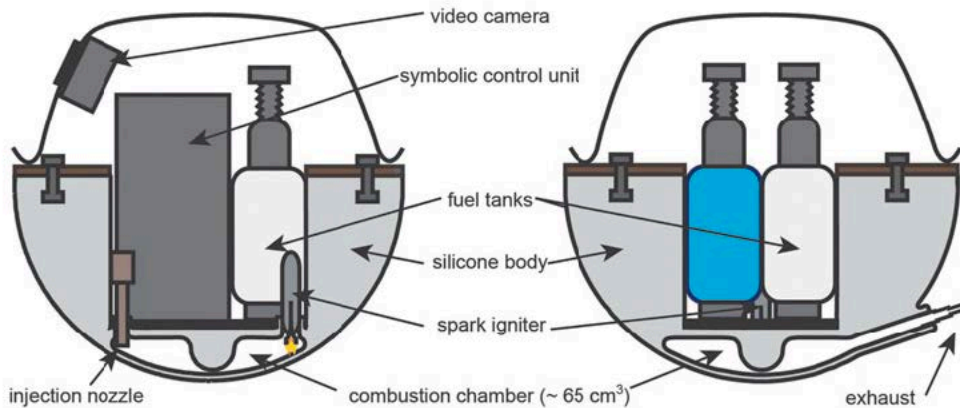
Scaling of Actuators: Heat Engines

- Combustion



a Cross section A

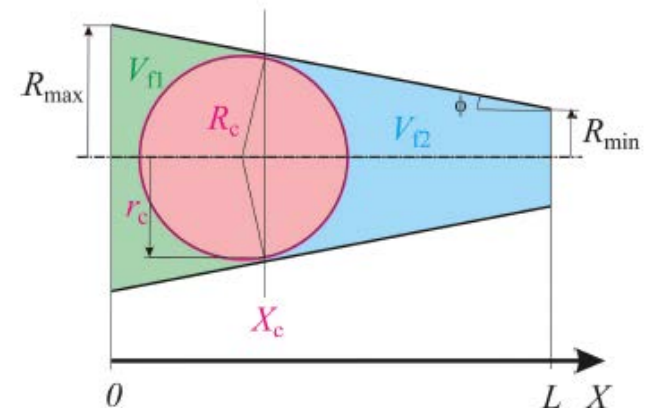
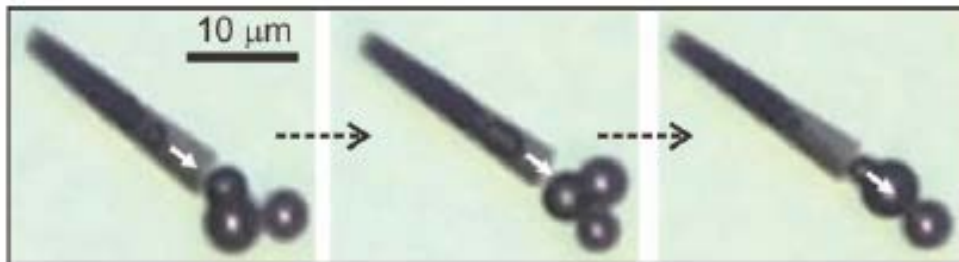
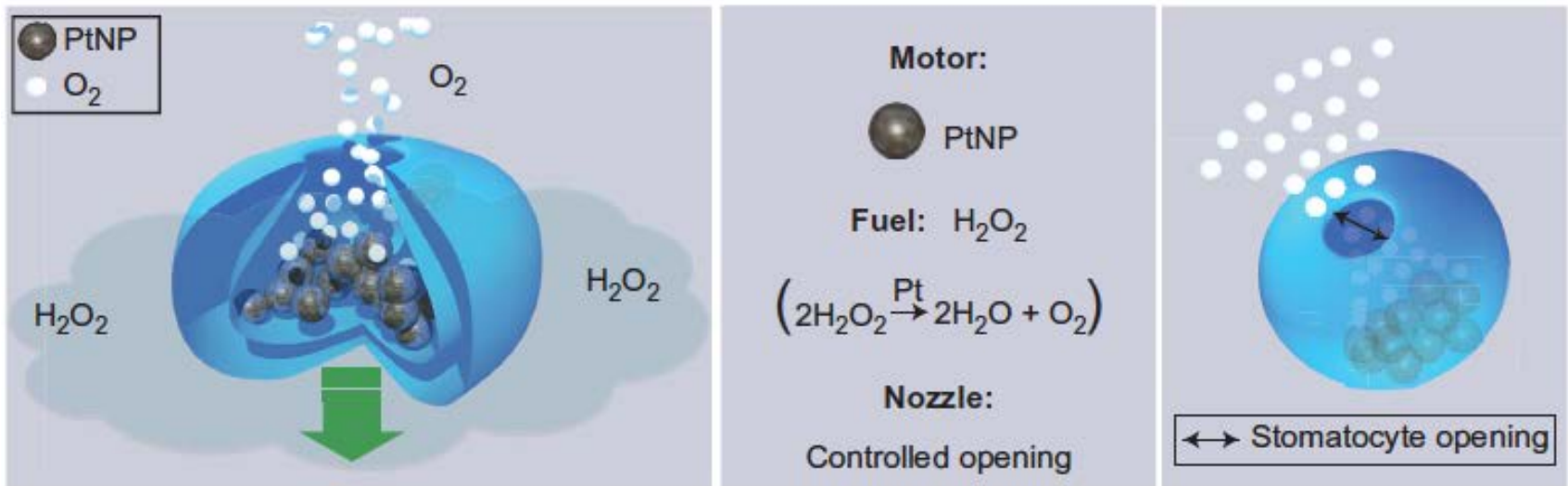
b Cross section B



Bartlett et.al., Science, 2015

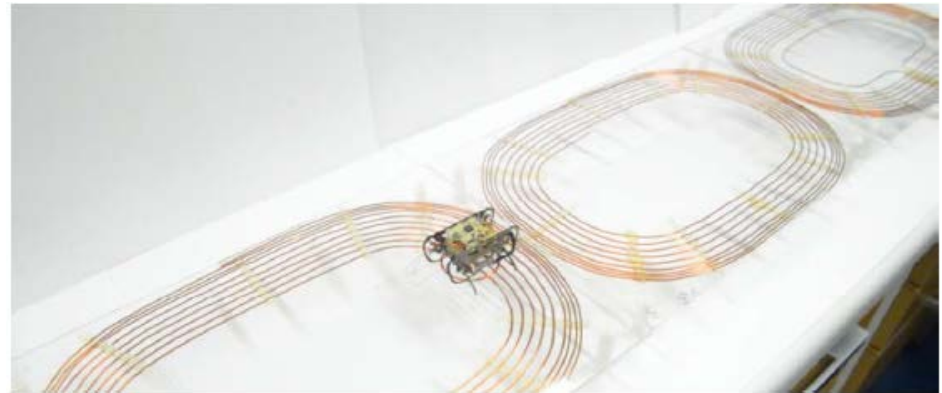
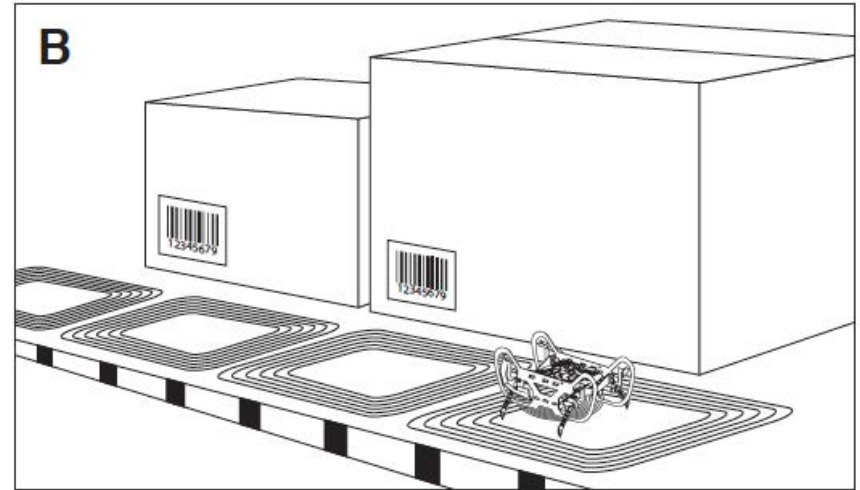
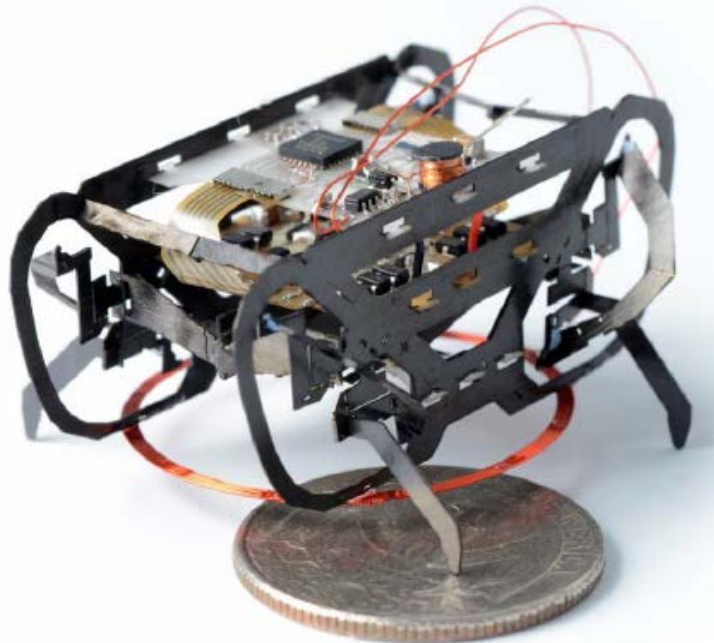
Chemical Propulsion at Small Scale

- Platinum and Hydrogen Peroxide



Wireless Energy Transfer

- Radio frequency power transfer
- Inductive coupling
- Power and control electronics
- 4cm, 2g robot

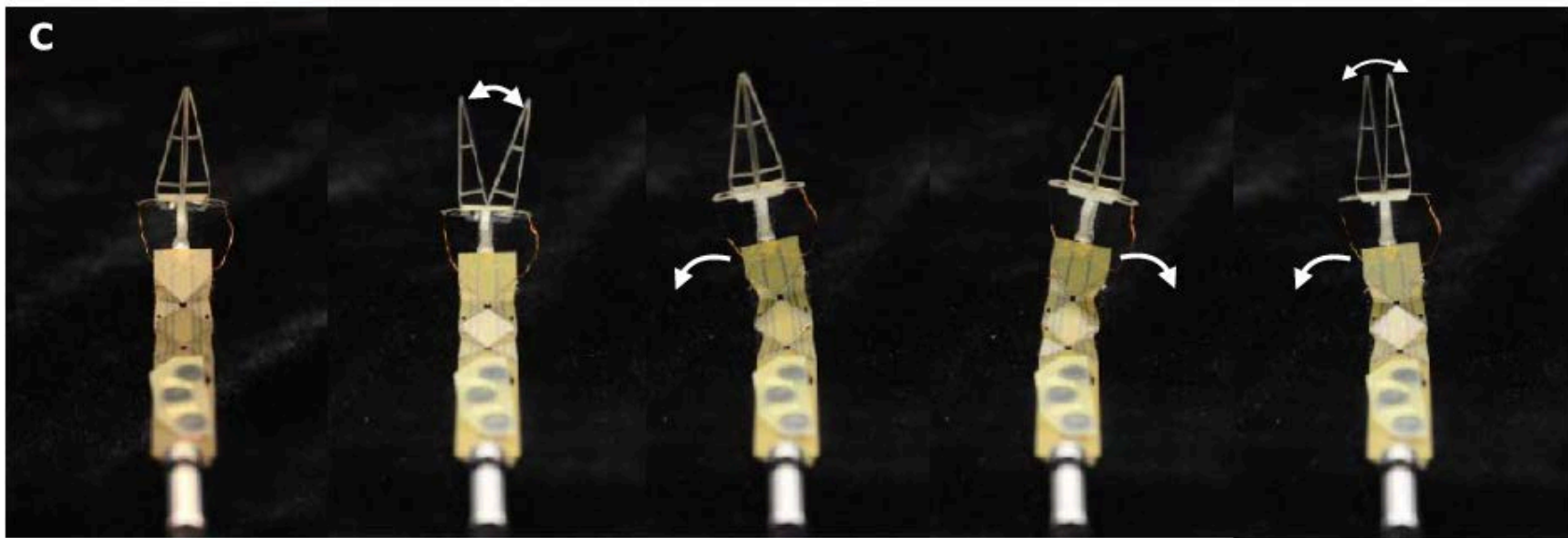
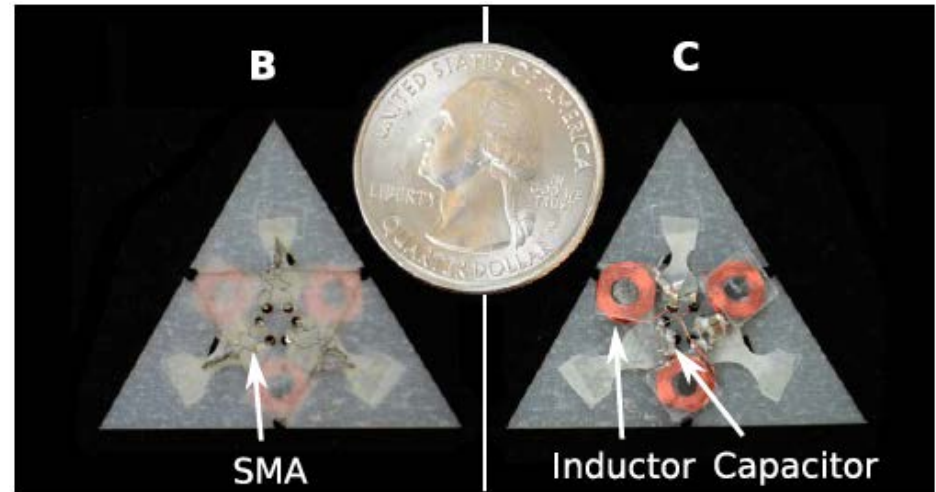


Karpelson et.al., ICRA, 2014

Wireless Energy Transfer

Boyvat et.al., Sci Rob, 2017

- RF power transfer
- Inductive coupling
- Heating SMA actuators

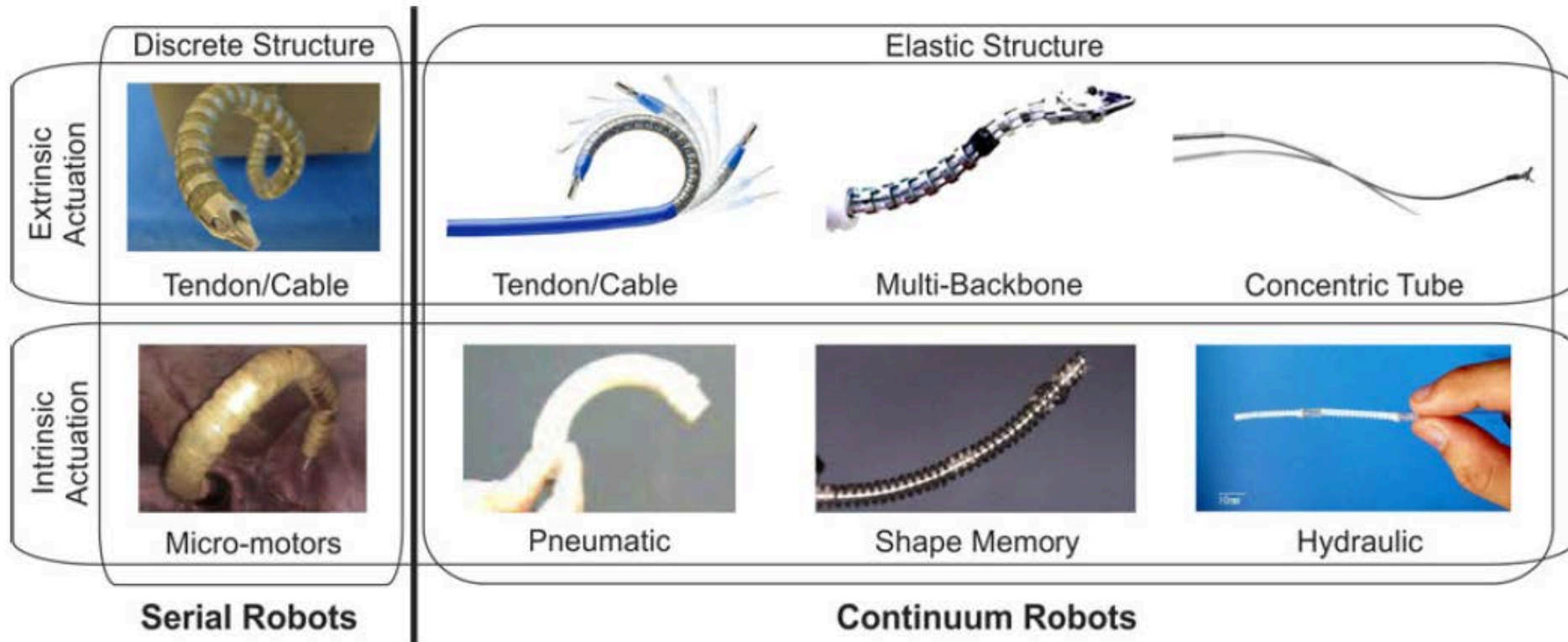


Challenges

- Antenna size: minimum millimeter range
- Inductive coupling does not scale well (resonant cavities)
- Distance: the coils must be kept close
- On-board power electronics (not enough voltage or current)

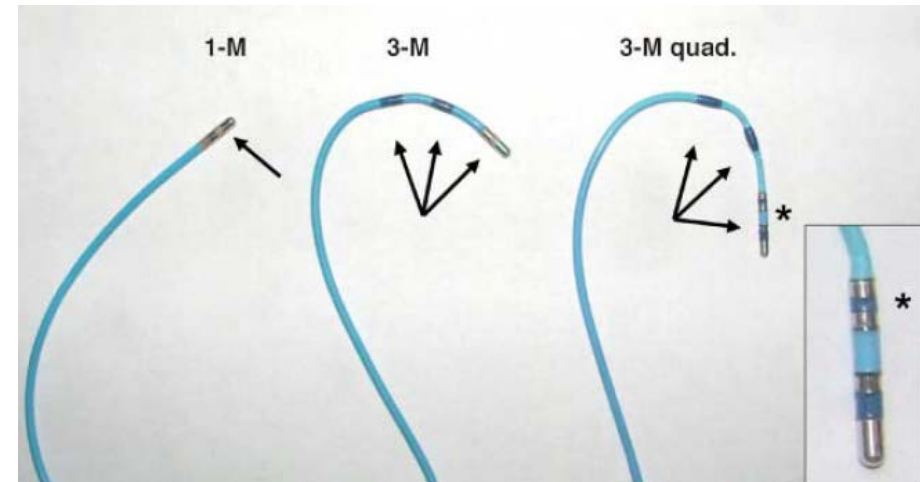
Case Study: Continuum Robots

Choset et al, TRO, 2015



Magnetically-Guided Microcatheters

- Development of novel end-effectors
- Dexterity and precision
- Ablation, microsurgery and imaging

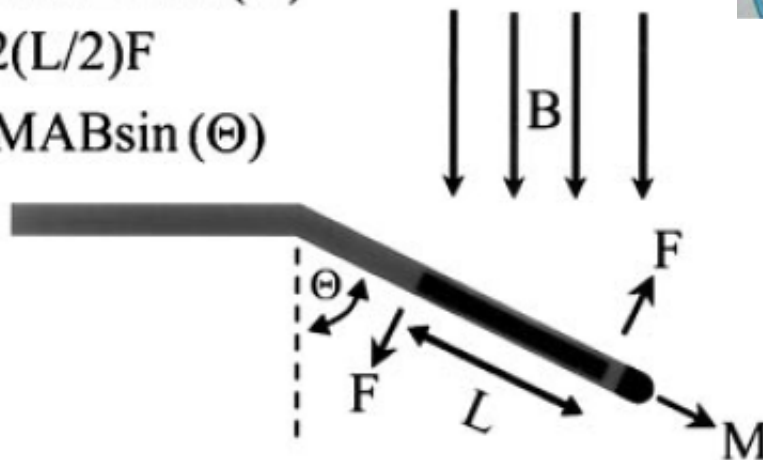


J. Chun *et al.*, *Eu Heart J*, 2007

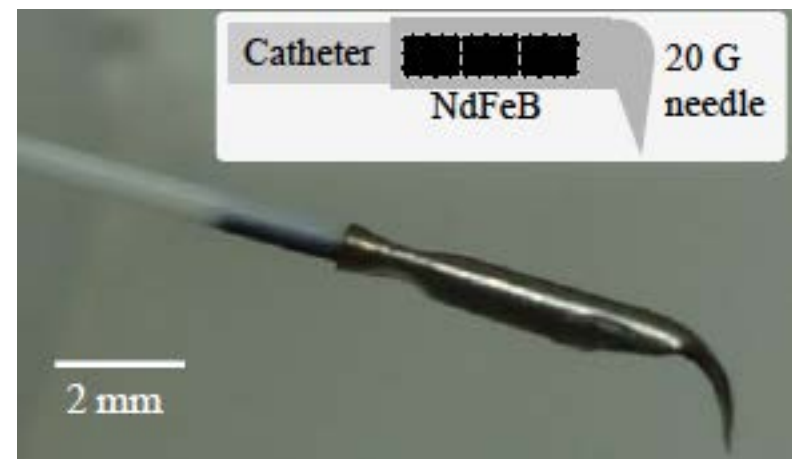
$$\tau = MALB\sin(\Theta)$$

$$\tau = 2(L/2)F$$

$$F = MAB\sin(\Theta)$$



M. Farris *et al.*, *Circulation*, 2002

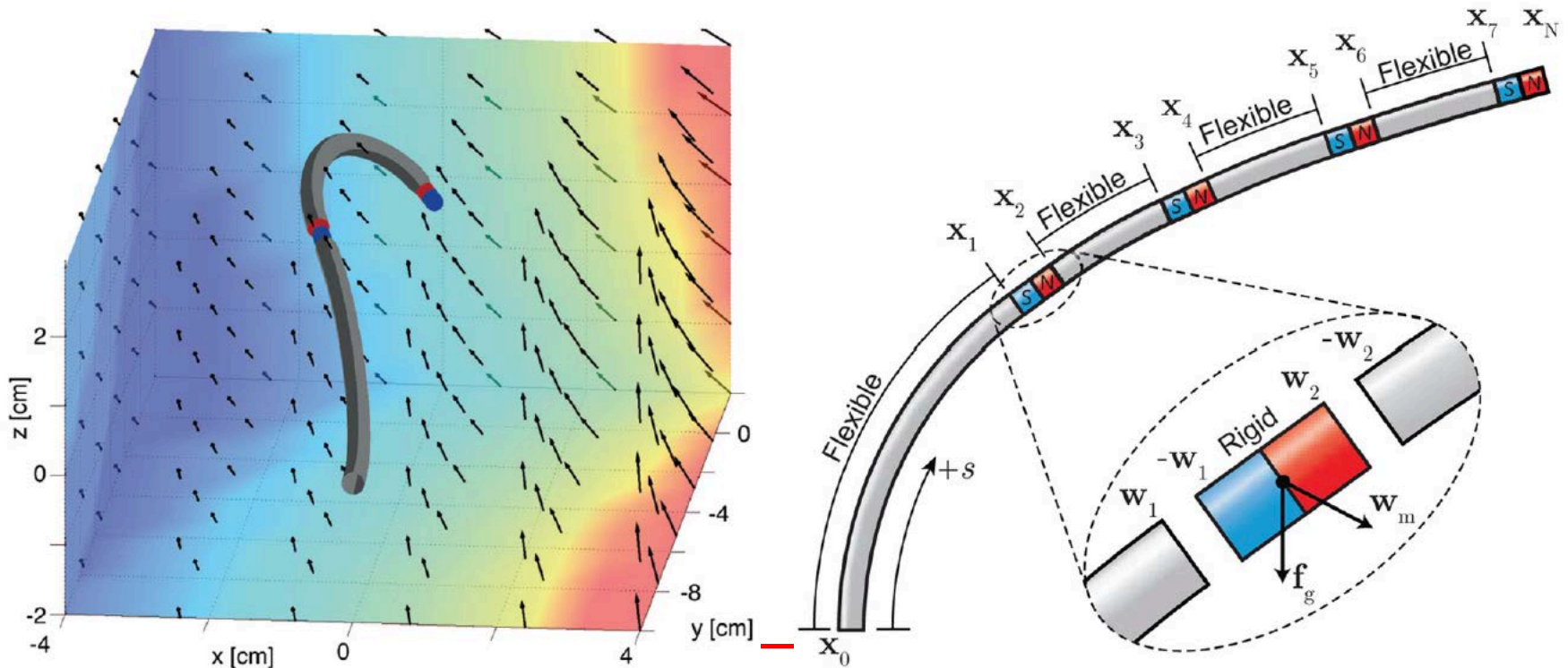


F. Ullrich *et al.*, *ICRA*, 2014

Magnetic control of continuum devices

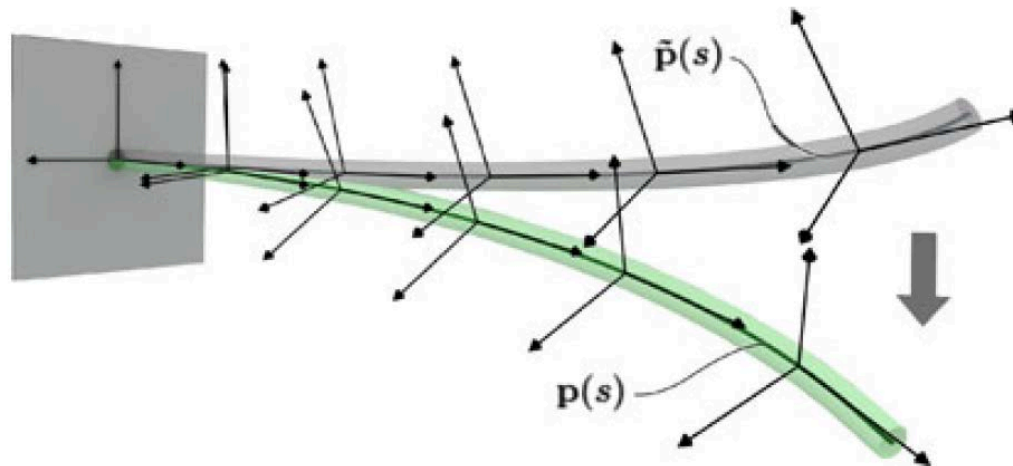
video

- Guiding the translation and/or deformation of elastic rods
 - Surgical tasks with catheters
 - Do not require pull wires or other bulky mechanisms
 - Forces and torques generated by the interactions between embedded hard magnets and magnetic vector field



Magnetic control of continuum devices

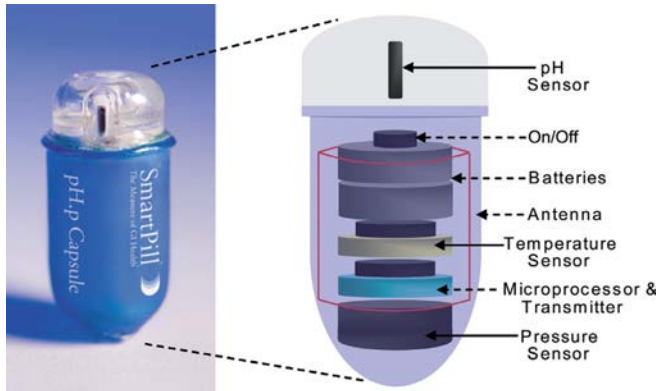
- Rigid segments: standard rigid-body kinematics and force-torque equilibrium equations
- Flexible segments
 - Kirchhoff's theory: rod is not stretched, only bending strain
 - Cosserat-Timoshenko rod theory: with tensile and shear stiffness (flexibility of the rod in tension and shear)
 - Small strains and Hooke's law
 - Solving the inverse problem (Jacobian Matrix)



PillCam

video

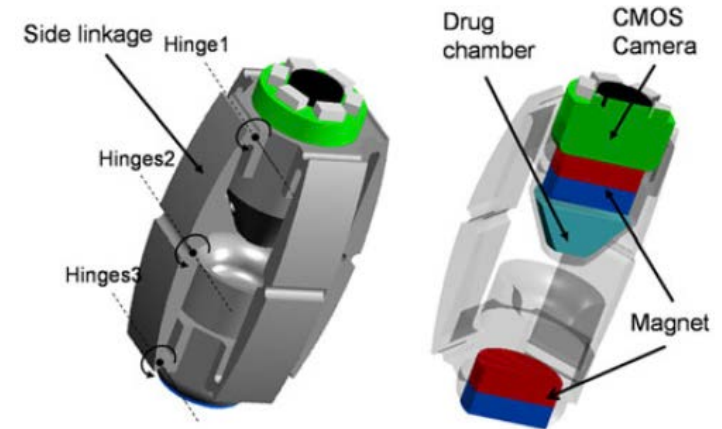
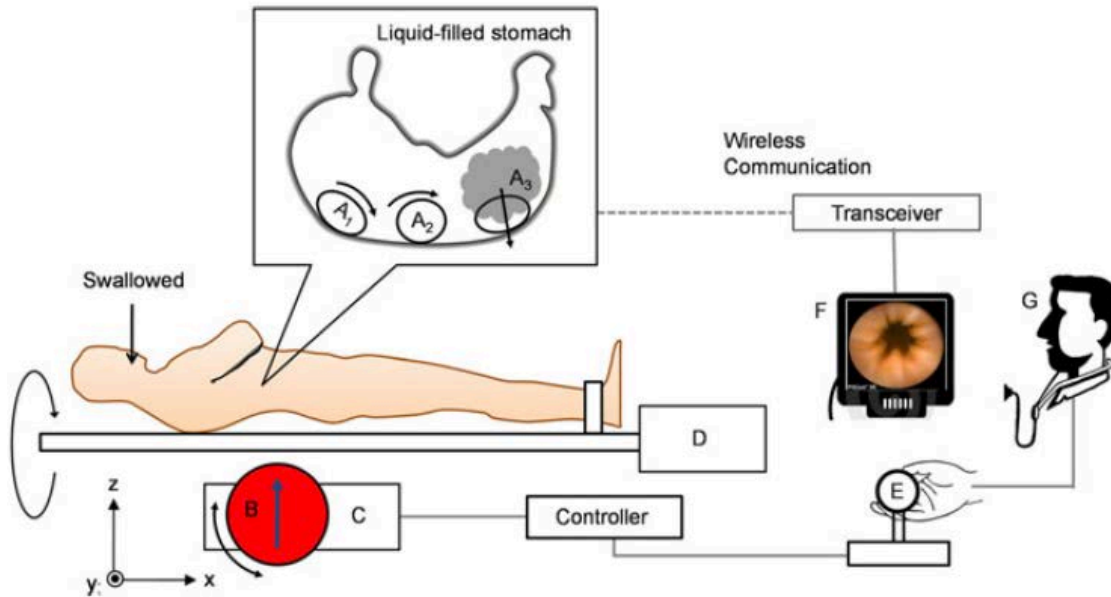
- Built-in light source and camera
- 4-6 frames per second for 8 hours
- Around 50,000 images will be taken per investigation
- Upper gastrointestinal endoscopy or colonoscopy



More than 1.5 million patients

Wireless Capsule Endoscope

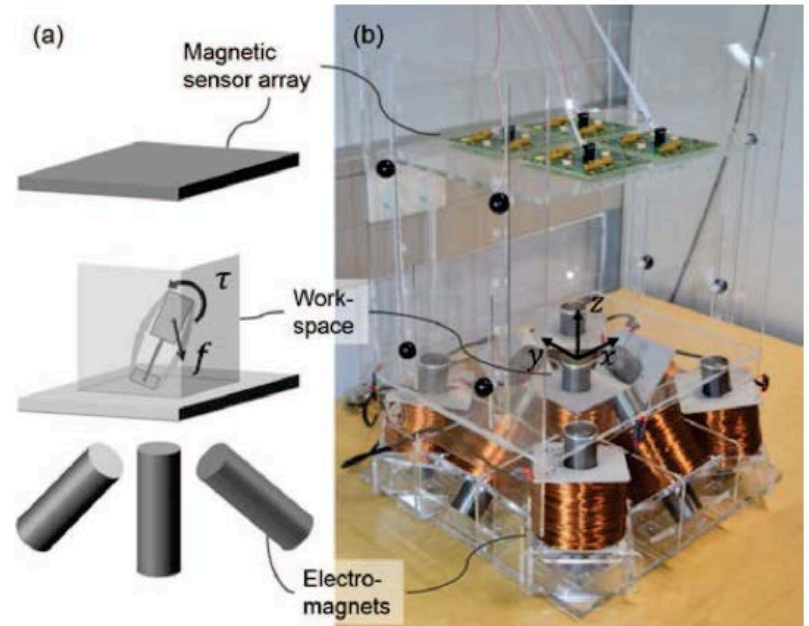
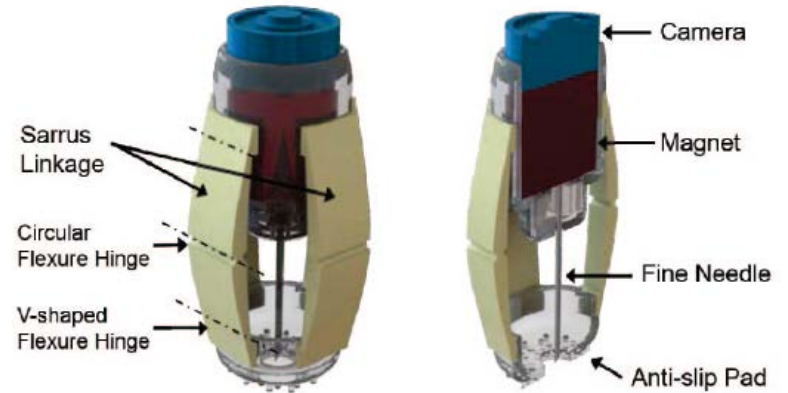
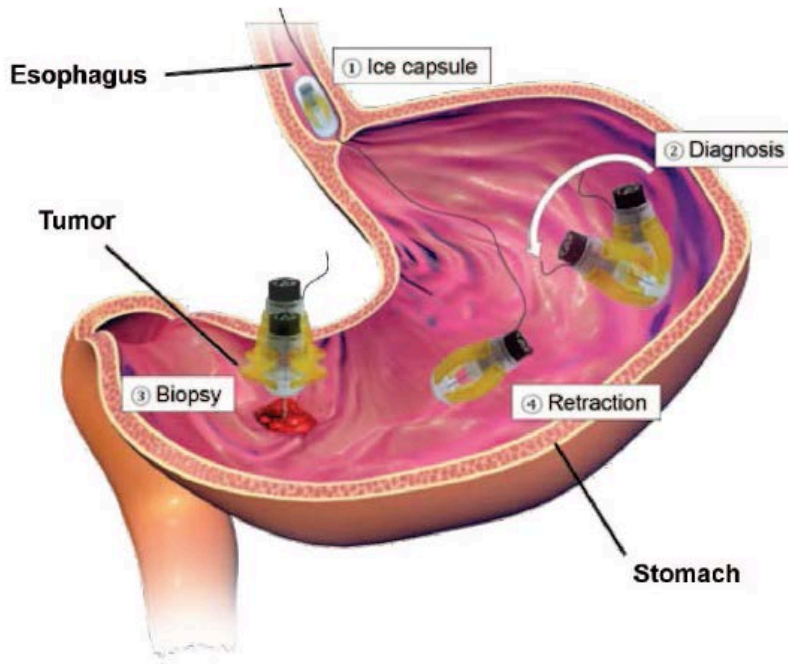
- Actuated tools for biopsy or drug release
- Magnetic control of position and actuation
- Localization (Ultrasound, Fluoroscope, MRI)



Kim et.al., TRO, 2012

Wireless Capsule Endoscope

- Overall dimensions $\varnothing 12\text{mm} \times 30\text{mm}$
- Fine needle 24G
- Penetration depth 10mm
- Localization: Hall sensor array

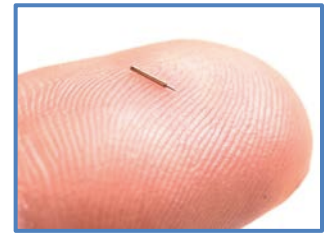


Intraocular Microrobots



In vivo mobility experiments in Female New Zealand White Rabbits

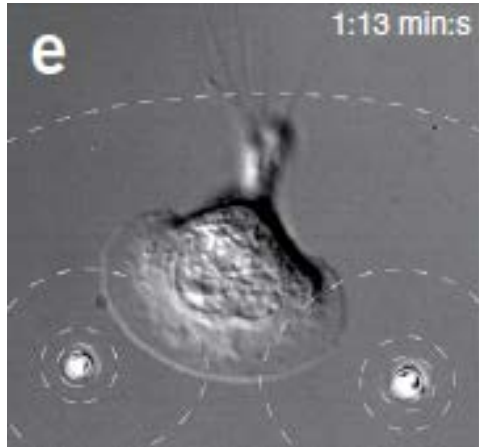
Ullrich et al, Invest Ophth, 2013



- OD: 300 μ m
- ID: 125 μ m
- Len: 2.5mm
- Coated with Au and Polypyrrole
- Fits in a 23G needle
- No need for sutures

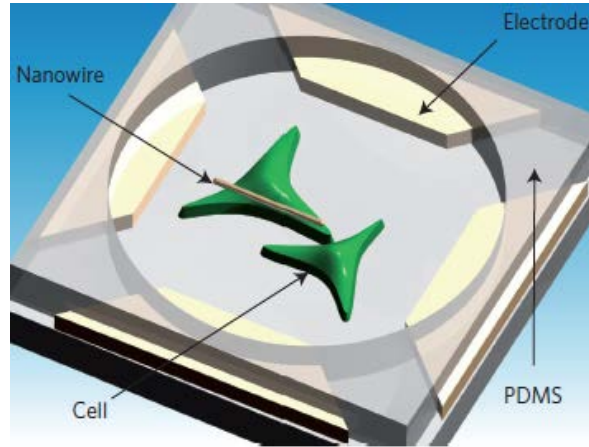
Microscale Untethered Robots

Optical Traps



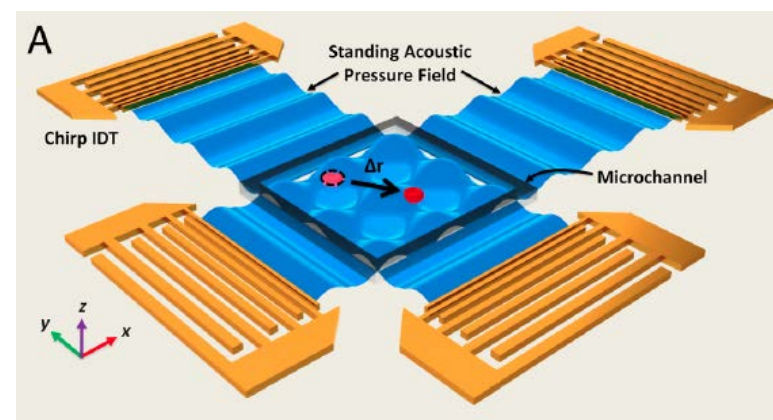
H. Kress *et.al.*, *Nature Meth*, 2009

Electric Field



D. Fan *et. al.*, *Nature Biotech*, 2012

Acoustic Waves



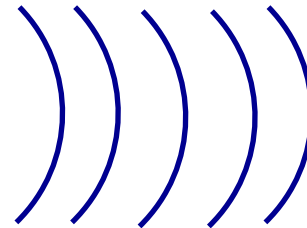
X. Ding *et.al.*, *PNAS*, 2012

From waves to mechanical work



SYSTEM

POWER AND CONTROL



MICROAGENT

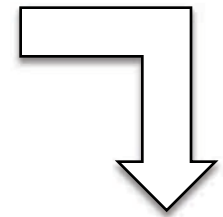
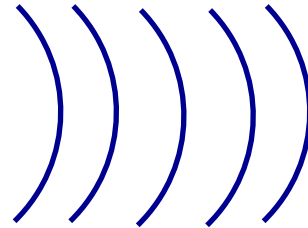
Wirelessly Powered and Controlled Microrobots

TOO SMALL FOR ON-BOARD BATTERY

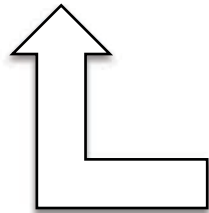
ELECTROMAGNETIC SYSTEM



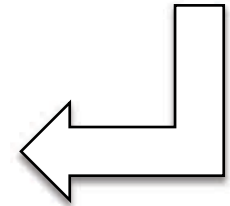
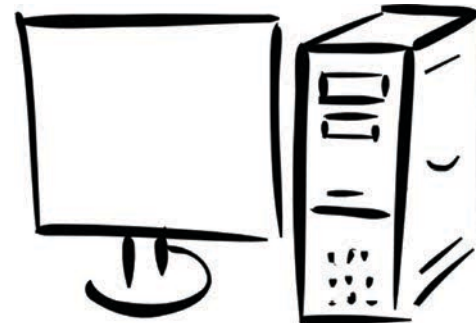
POWER
SIGNAL



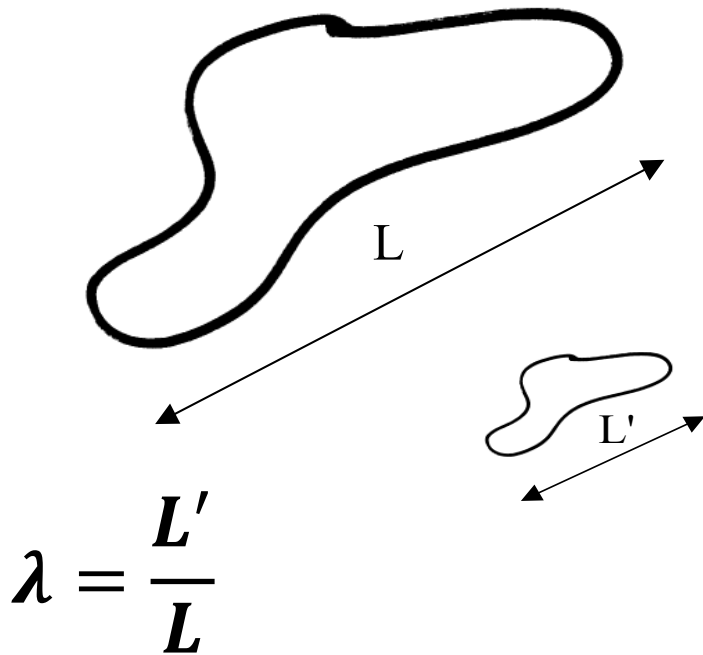
LOCALIZATION
&
SURVAILANCE



CONTROL
SIGNAL



Scaling Laws



Magnitude	Scaling factor
length (L)	λ
area (A)	λ^2
volume (V), mass (m)	λ^3
surface to volume ratio	λ^{-1}
stiffness (k)	λ
resonance frequency (f_0)	λ^{-1}
mass responsivity (\mathfrak{R})	λ^{-4}
thermal time constant (τ)	λ

Scaling Laws

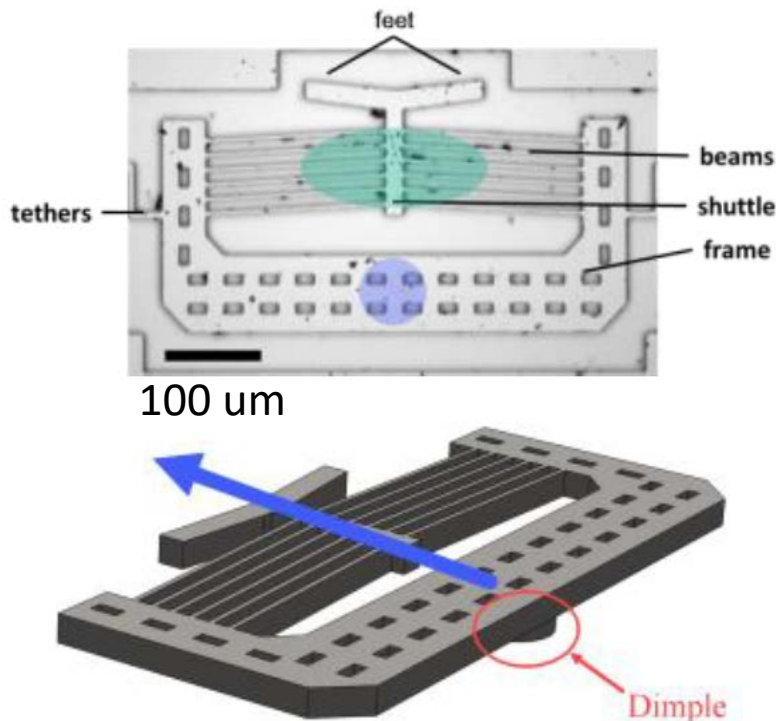
- Depending on the size-scale different physical effects become more or less important
- At small scale, inertial forces become less important as mass scales $\sim L^3$ (keeping density constant)
 - Resonant frequencies go very high
 - Thermal equilibrium is achieved faster
 - Electromagnetic forces dominate mechanics
 - Laminar flow dominates fluidics

Light-matter interactions

- Thermal forces (radiometric forces)
 - Temperature gradients in the medium surrounding the object
 - Thermal expansion of solids
 - Thermophoresis of microparticles
 - Phase transitions (vapor pressure, shape memory, liquid crystal)
 - Thermocapillary convective flows
 - Photoacoustic effect
- Radiation pressure
 - Optical tweezers
 - Momentum transfer

Thermal expansion (impact drive)

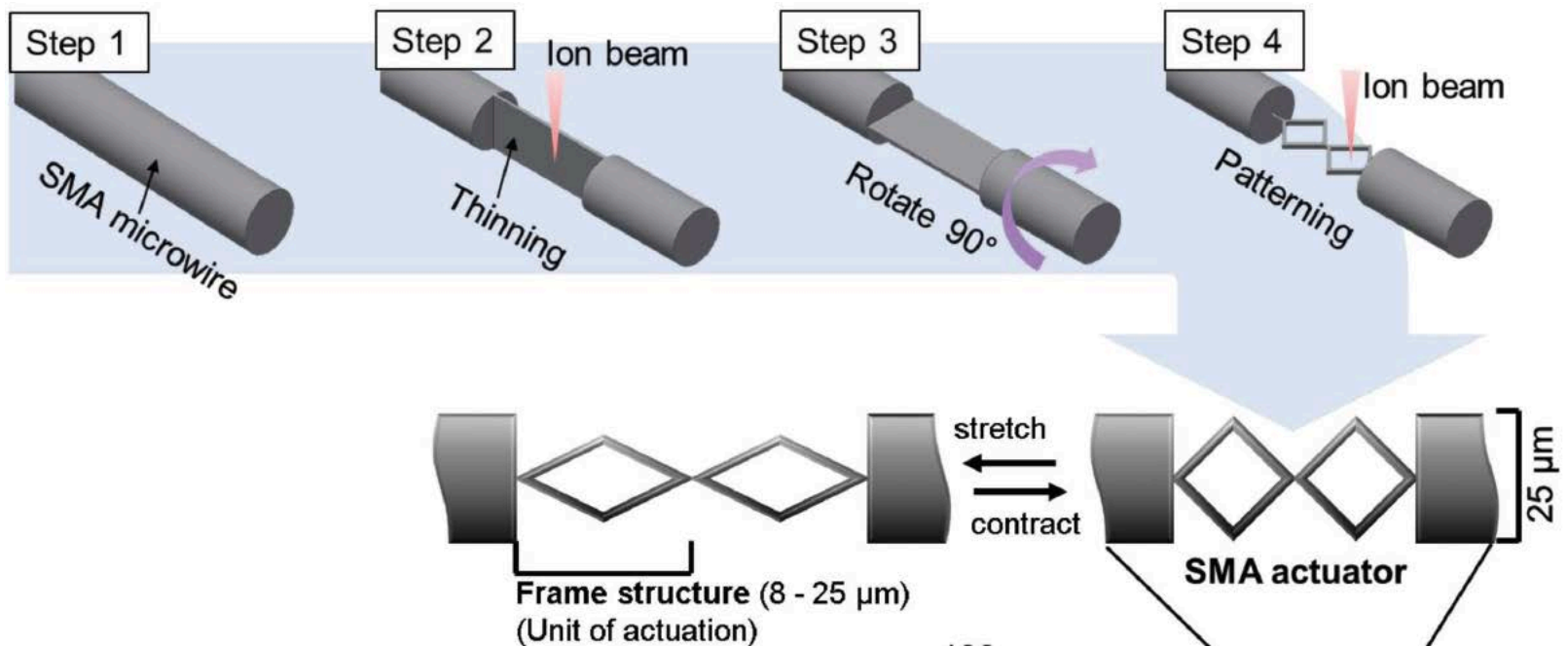
- Based on expansion of materials due to temperature changes
- Temperature control: Joule heating or light absorption
- Direct expansion vs bending moment (bimorph actuator)
- Example: Actuated at resonance frequency: stick and slip motion



Constant	Quantity/Name	Value
R	Reflectivity of Silicon	0.3
T_{env}	Environment Temperature	20 °C
ρ_{Si}	Silicon Density	2328 kg · m ⁻³
h_{air}	Air convection constant	10 W · (m ² · K) ⁻¹
k_{air}	Air thermal conductivity	0.025 W · (m · K) ⁻¹
c_{v-air}	Air specific heat	716 J · (Kg · K) ⁻¹
k_{Si}	Silicon thermal conductivity	124 W · (m · K) ⁻¹
$c_{v,Si}$	Silicon specific heat	702 J · (kg · K) ⁻¹
α_{Si}	Silicon coefficient of thermal expansion	2.6 × 10 ⁻⁶ (°C) ⁻¹
θ	Theta (beam angle)	0.04991642 rad

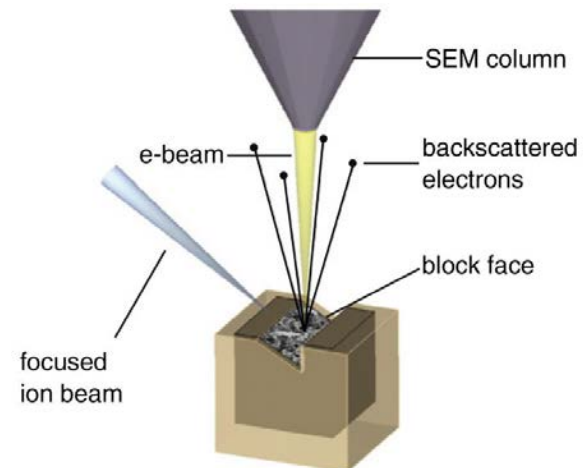
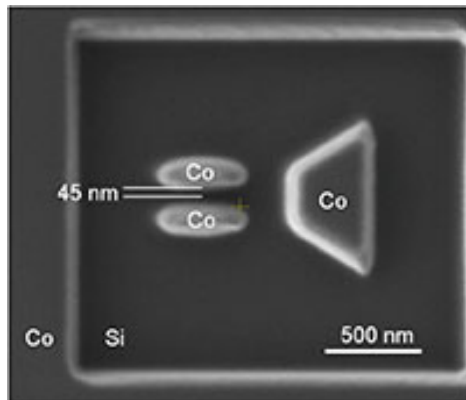
SMA Microactuators

- Focus Ion Beam milling of 25 μ m wire
- Activation with UV laser (high absorption coefficient for metals)

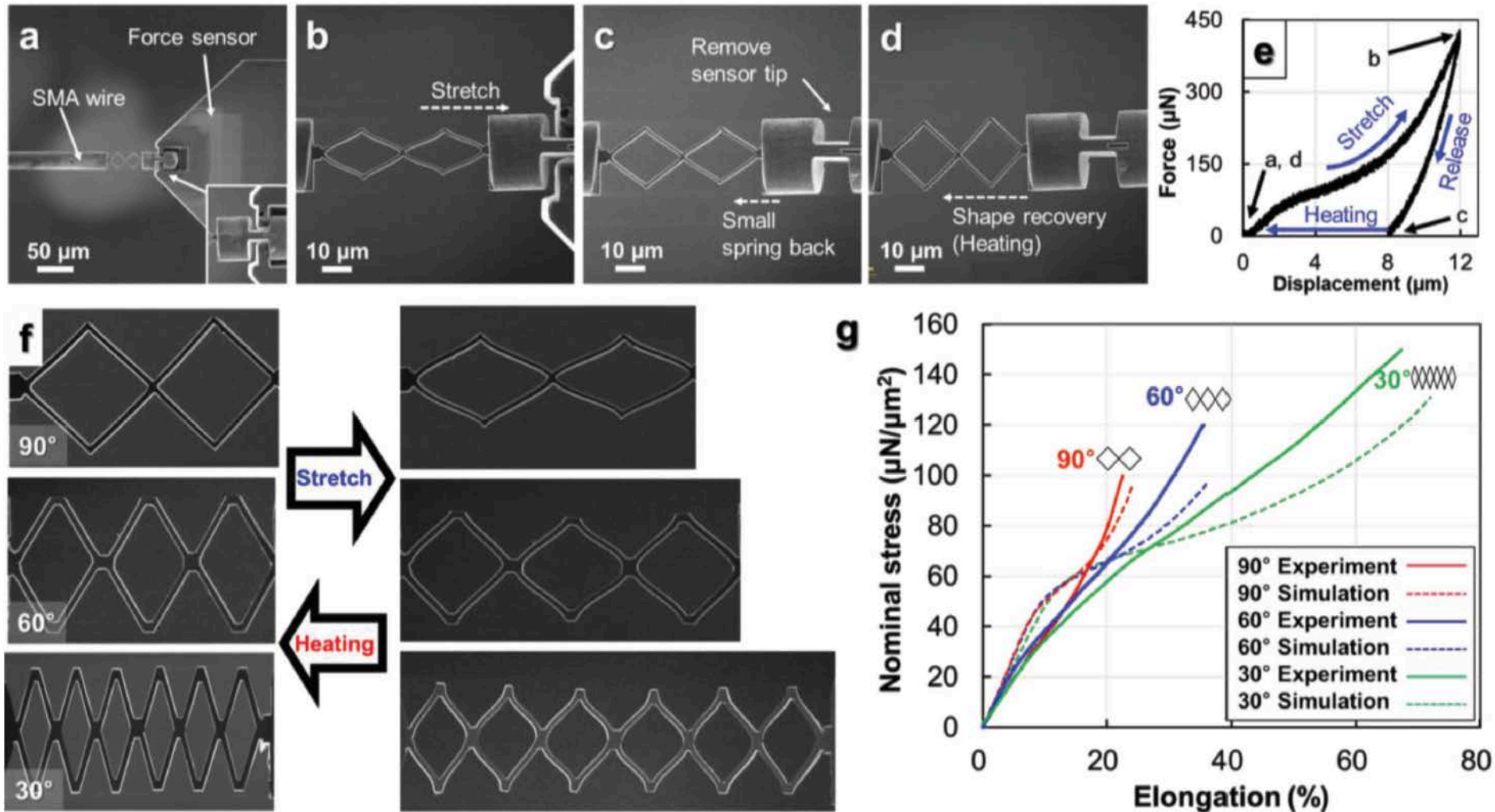


Focused Ion Beam Milling

- In electron microscopy, relatively low-mass electrons interact with a sample non-destructively to generate secondary electrons which, when collected provide high-quality images (sub nanometer res)
- Focused ion beam (FIB) instrument uses a beam of ions
- Lightest ion has 2000 times the mass of an electron
- Control the energy and intensity of the ion beam
- Capable of cutting away or building up structures on a surface with a resolution of 50 nm. Structures can be imaged in real-time using scanning electron microscopy mode.

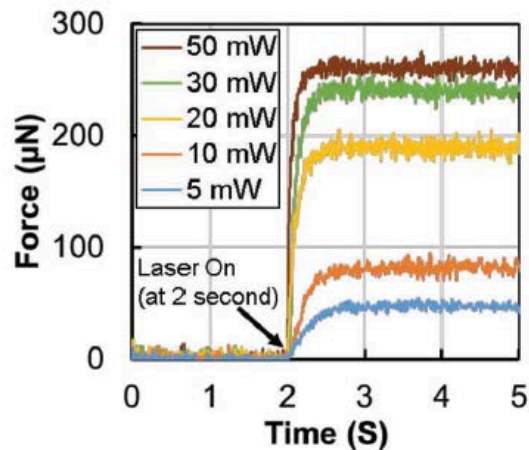
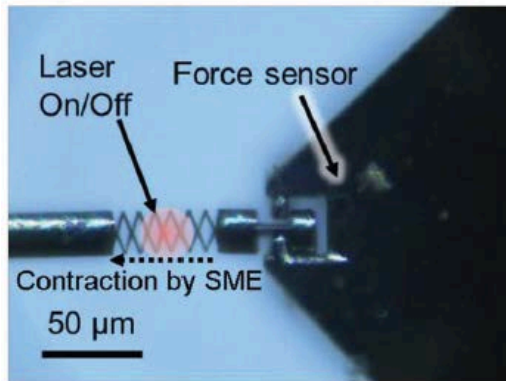


SMA Microactuators



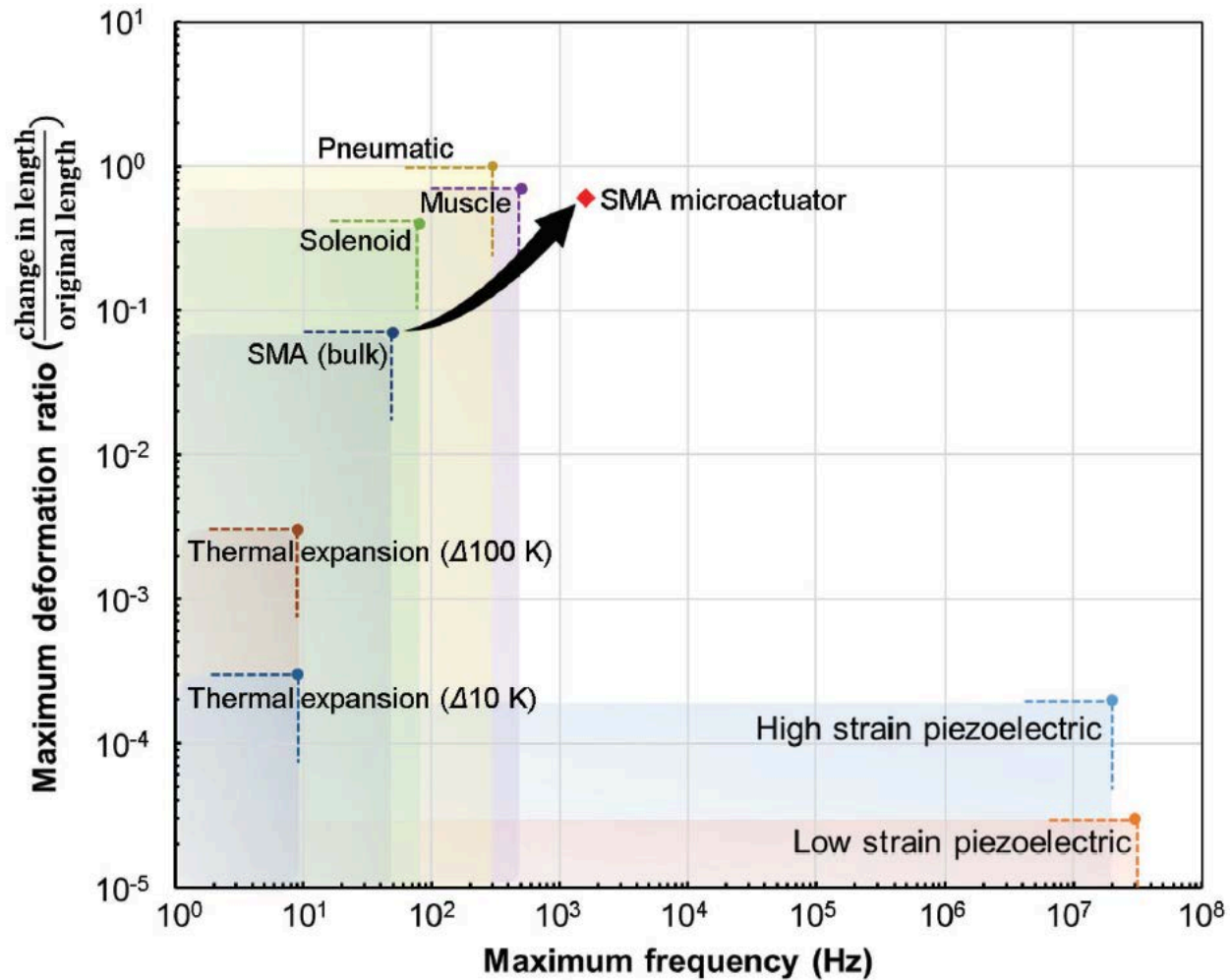
SMA Microactuators

video



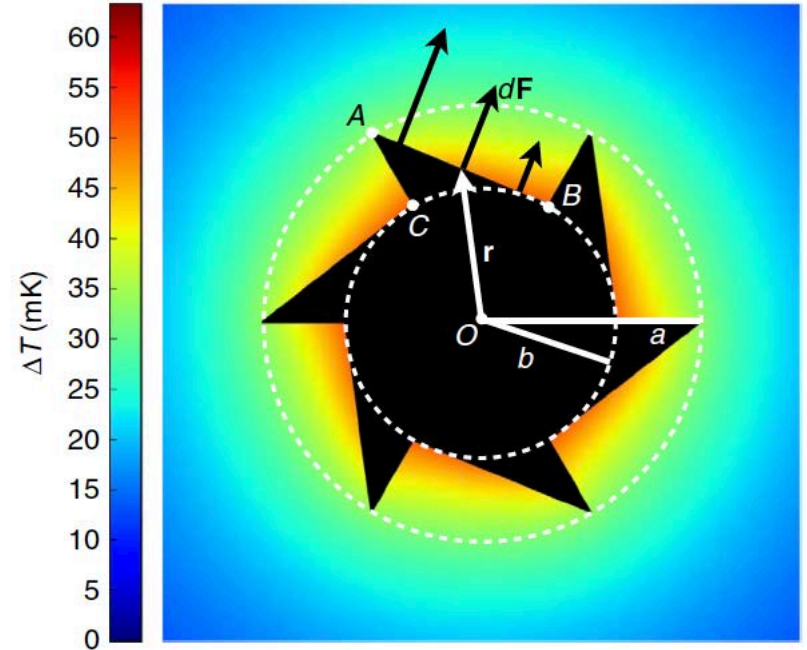
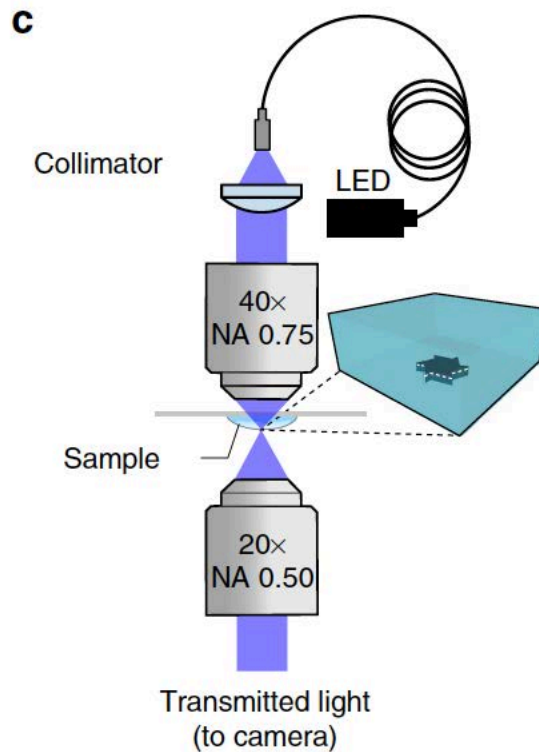
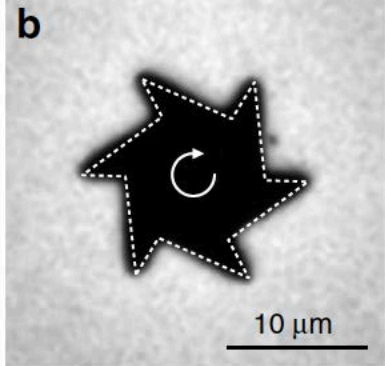
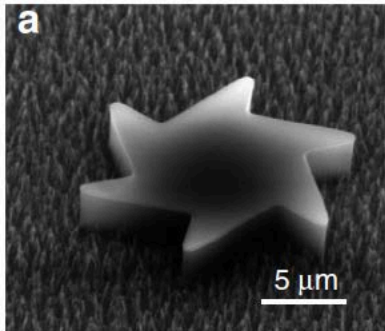
Specification	Muscle fiber	SMA microactuator [unit cell]
Maximum frequency [Hz]	500 ^[2]	1600
Maximum actuation stress [MPa]	0.1–0.4 ^[2]	0.75
Diameter [μm]	24.4 ± 1.1 ^[29] (myofibril)	25
Length [μm]	1.6–2.5 ^[30] (length of sarcomere)	8–25
Maximum deformation ratio	0.25–1.4 ^[31,32]	0.15–0.6

SMA Microactuators: Performance



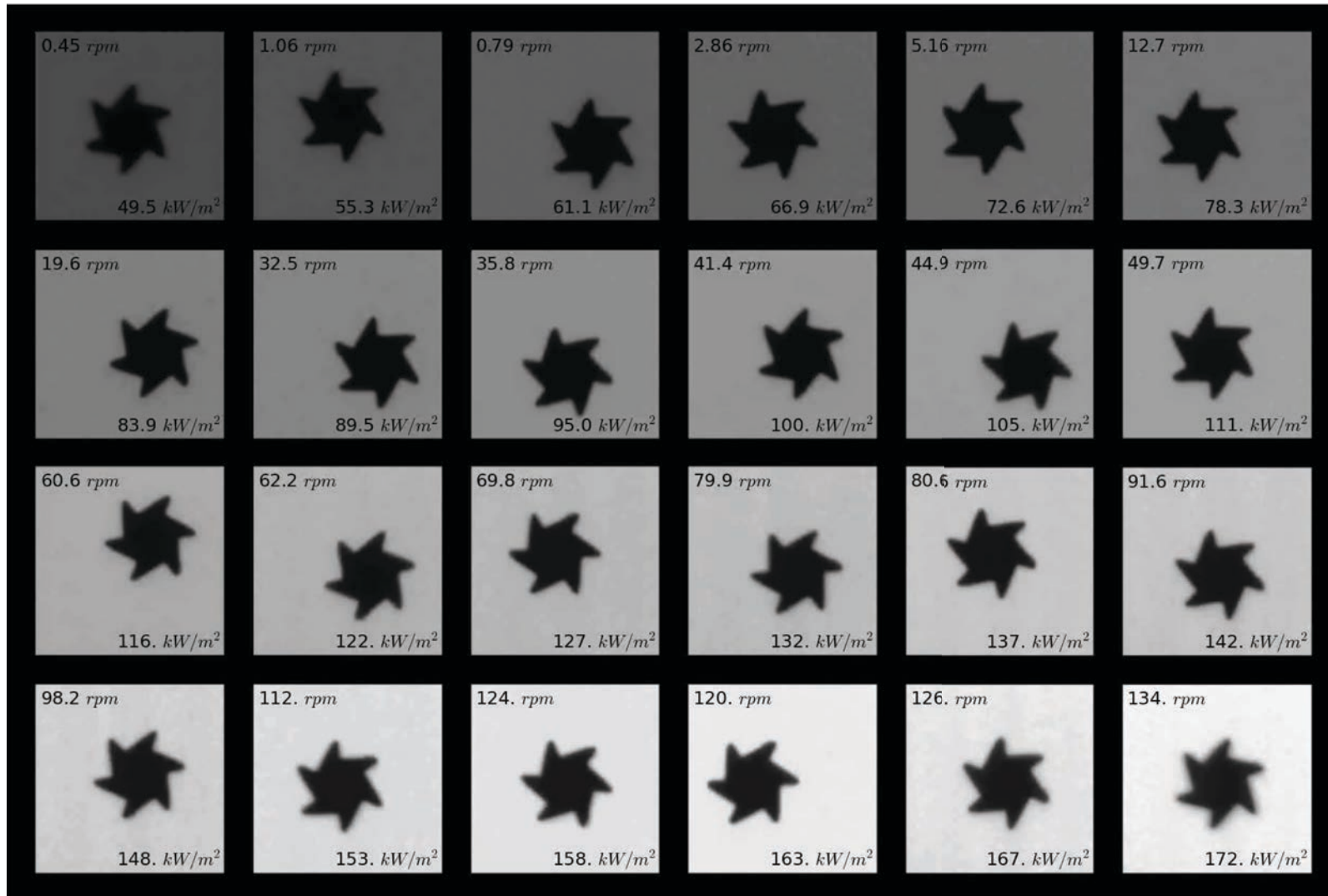
Thermocapillary Forces

- Microgear at the liquid-air interface
- Carbon coating to increase absorption
- Marangoni effect



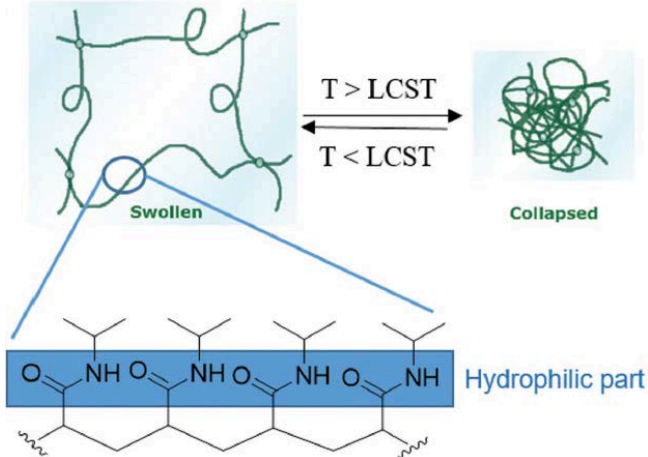
$$\mathcal{T} = \int \mathbf{r} \times d\mathbf{F} = \int \mathbf{r} \times \hat{\mathbf{n}} \gamma(T) ds,$$

Thermocapillary Forces



Smart hydrogels

- Gels made of networks of cross-linked long polymer chains
- Soft material: Young's modulus in the kPa range
- Swell-deswell water in response to an external stimulus
 - Temperature, pH, chemicals

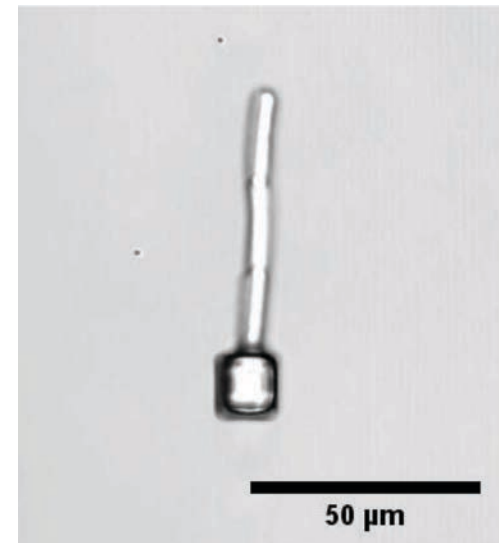
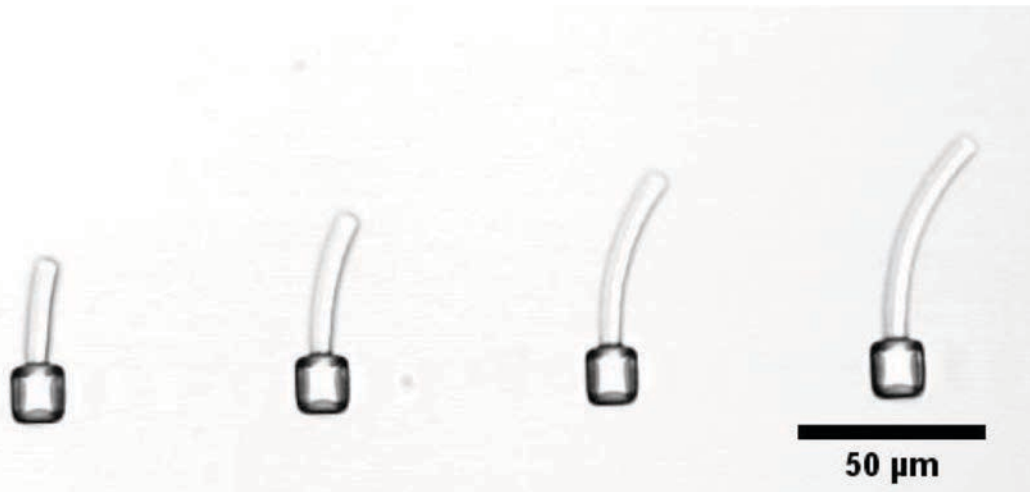
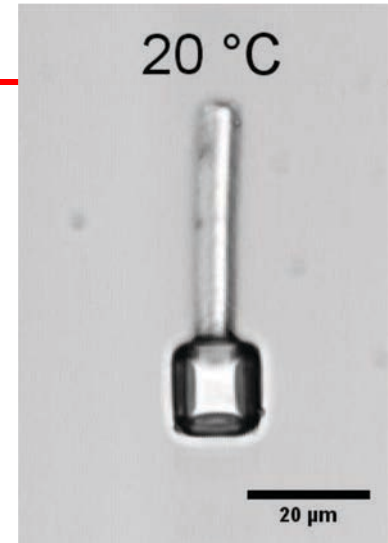
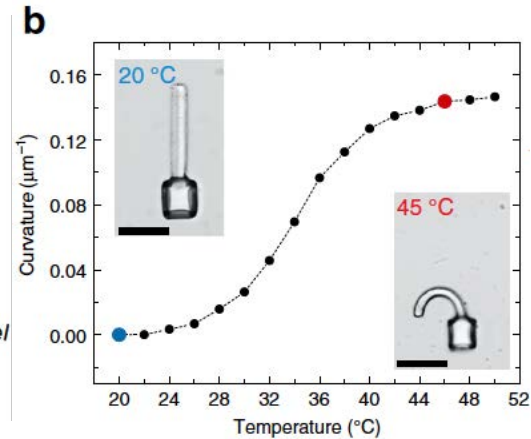
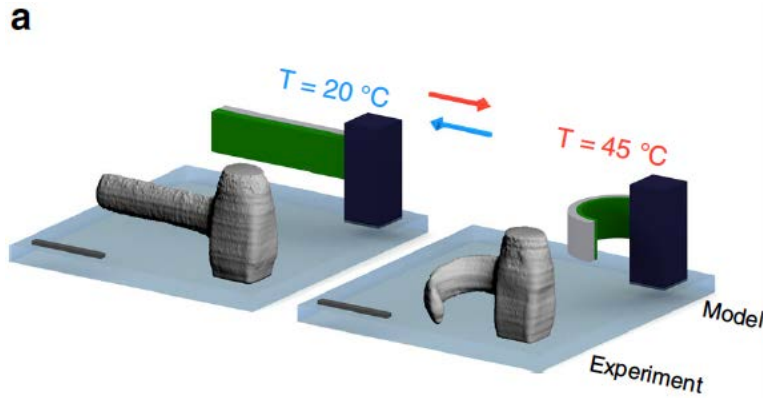


- Relatively small forces but high volumetric change
 - Energy densities up to 460 kJ m^{-3}
 - Strains of up to 90% under 4 MPa load
 - Can be stretched up to 1200%
 - Response is diffusion limited: millimeter sized gels \sim seconds
 - Chemical stability and performance degradation in time

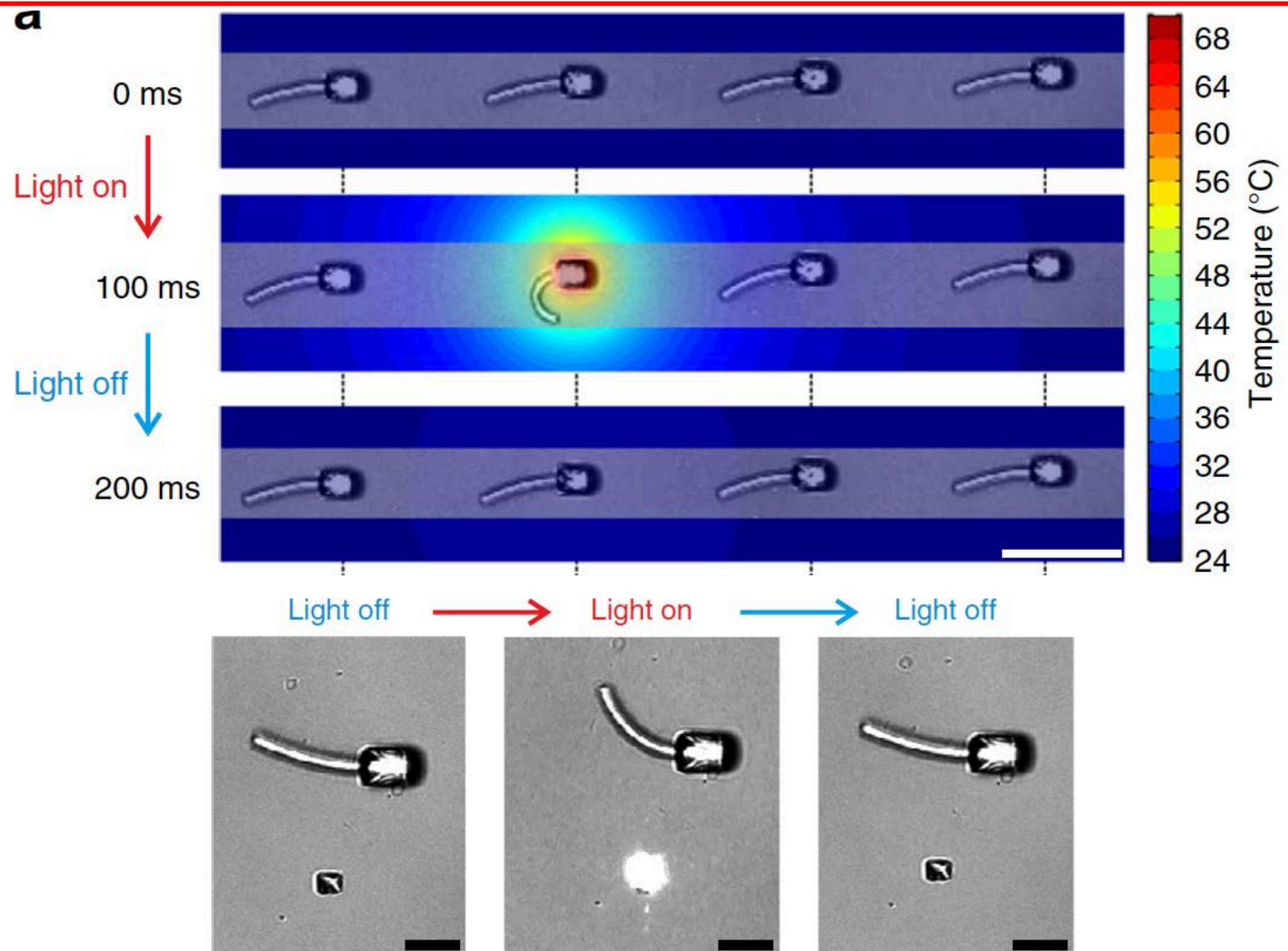
Thermoresponsive Hydrogels

- Lower critical solution temperature (LCST) and upper critical solution temperature (UCST)
- poly(N-isopropylacrylamide) or pNIPAM: a combination of hydrophilic and hydrophobic segments in the polymer chain
 - At temperatures below LCST, swell due to domination of hydrophilic interactions with water
 - At temperature above LCST, the hydrogen bonds with water are broken and hydrophobic interactions among the polymer chains dominate, which result in deswelling

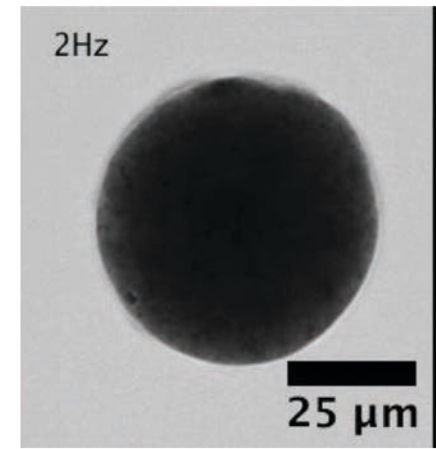
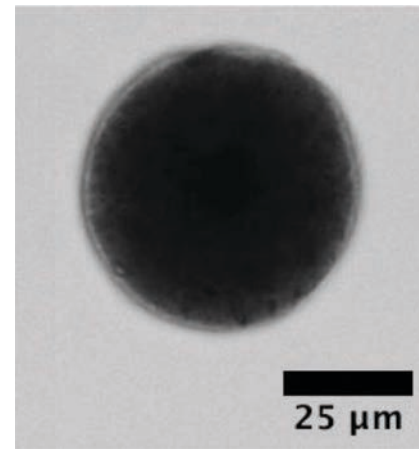
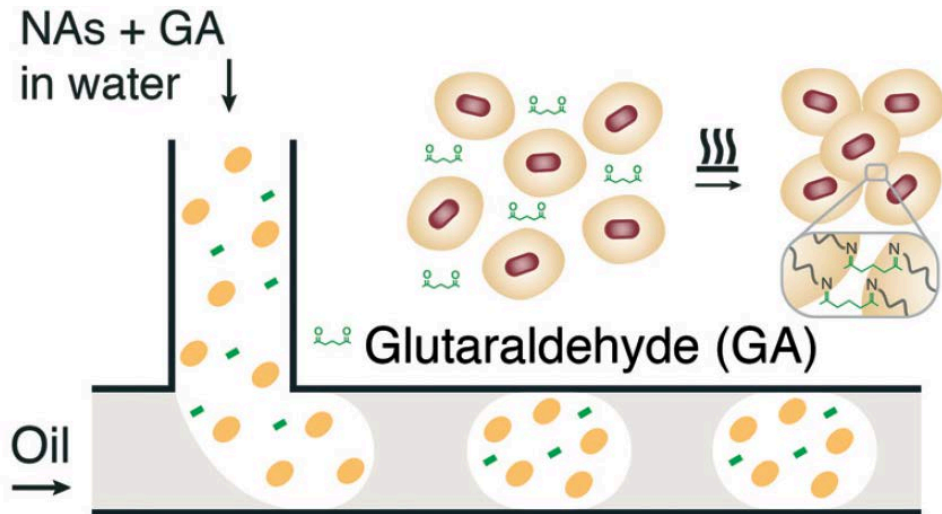
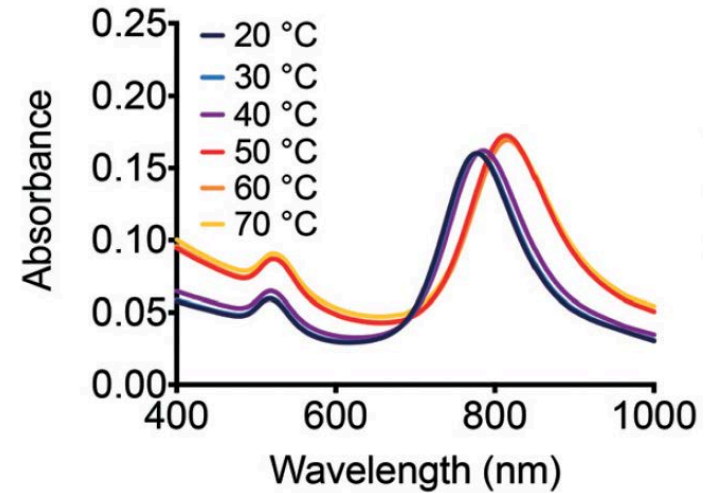
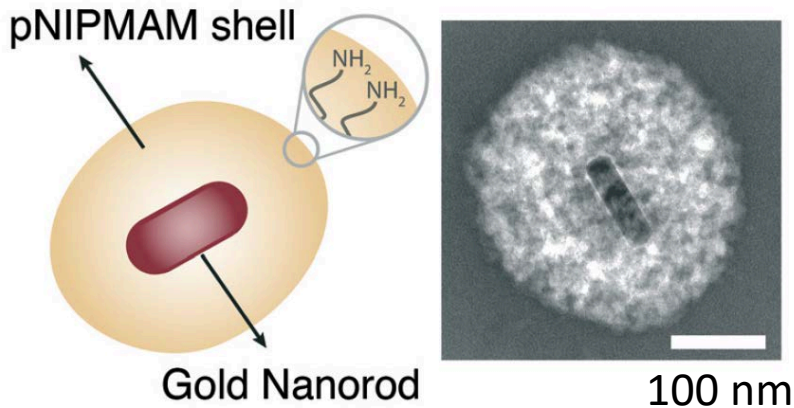
Direct Laser Writing of Actuators



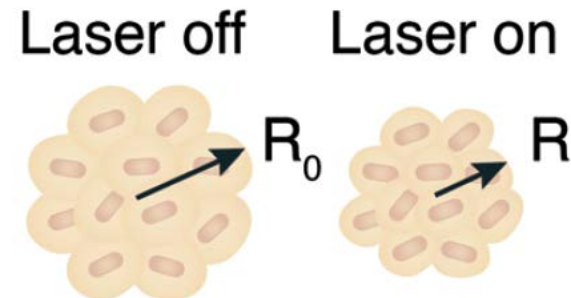
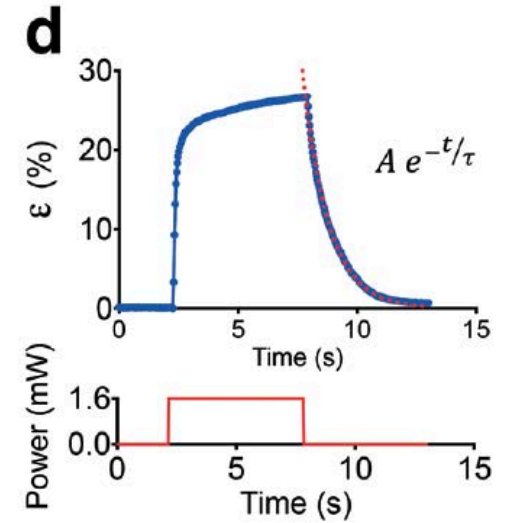
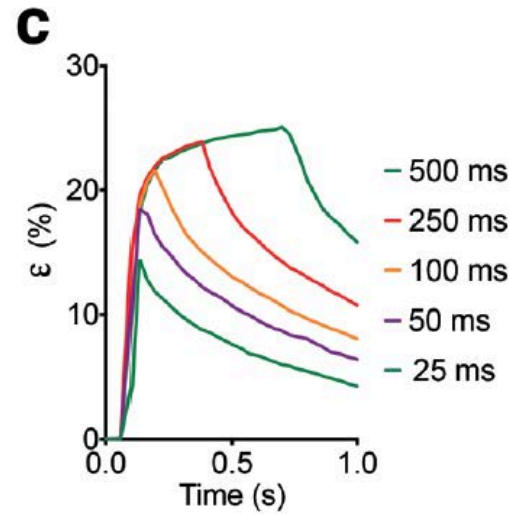
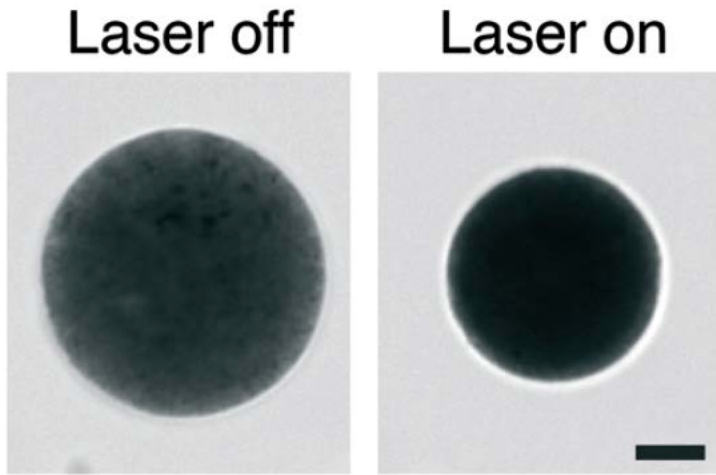
Laser-induced Actuation



Optomechanical Nanoactuators

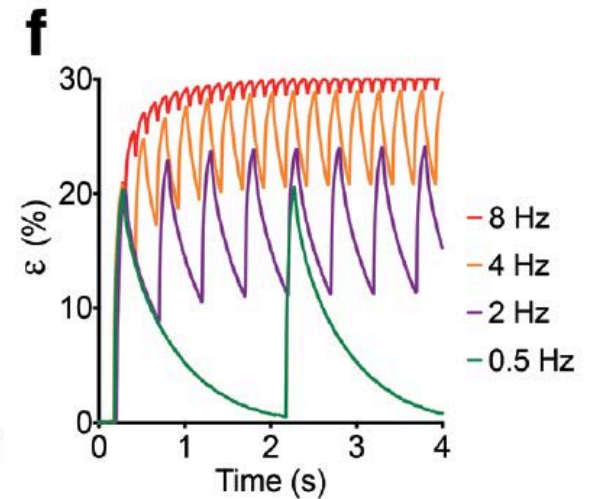
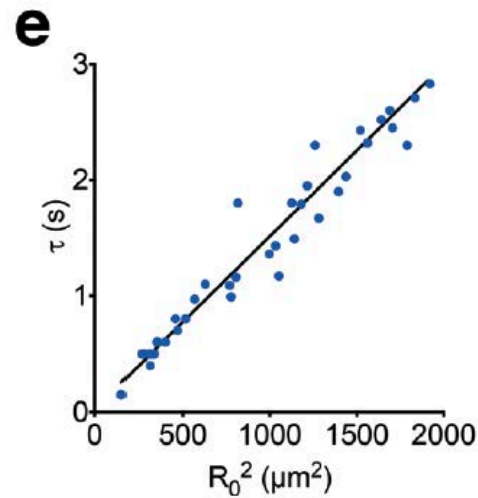


Plasmon Resonance

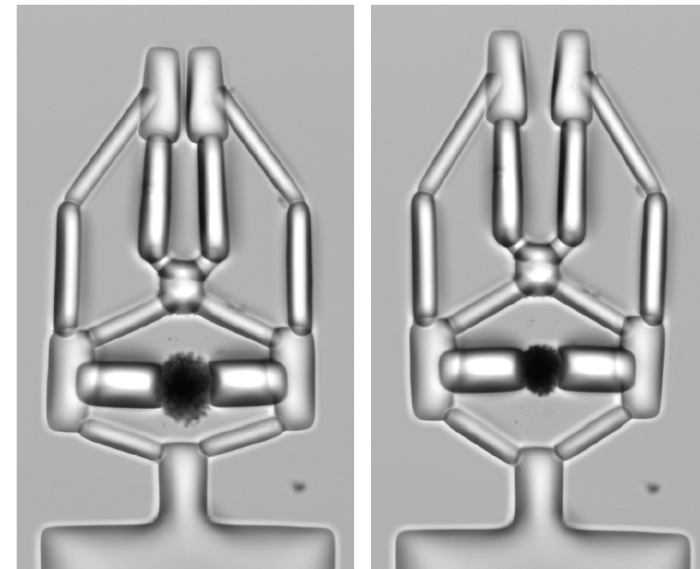
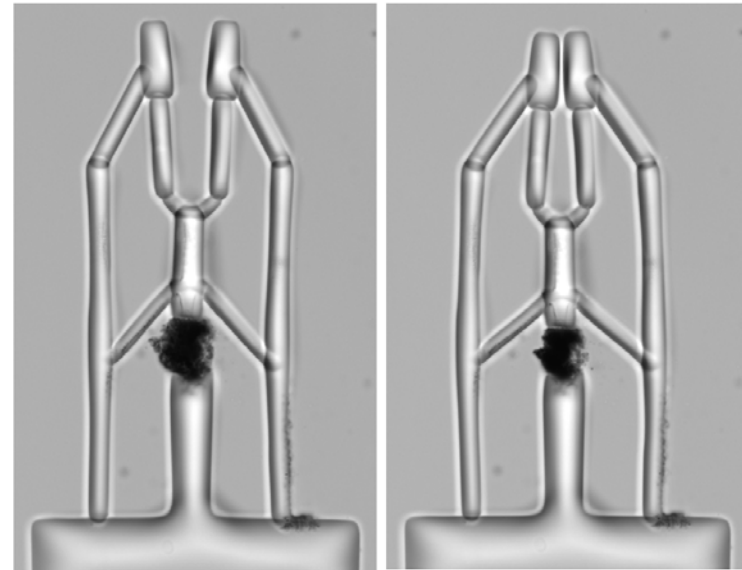
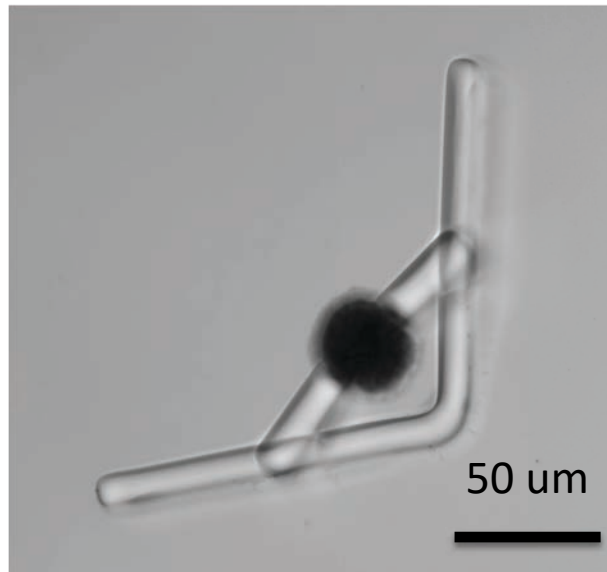
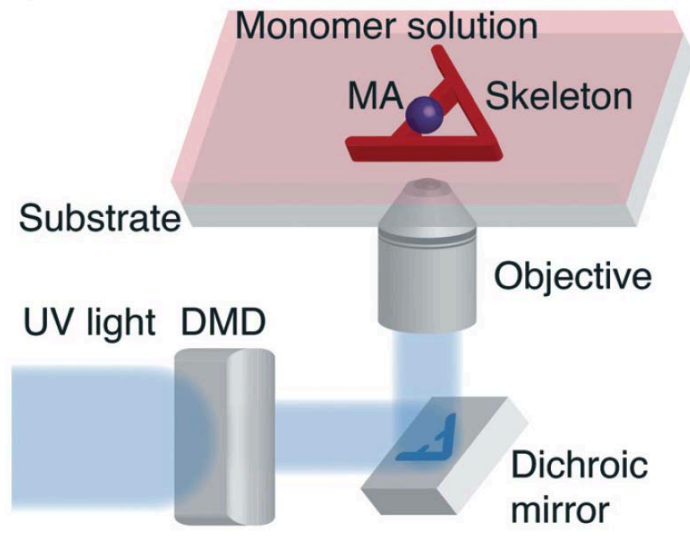


Actuation strain (%)

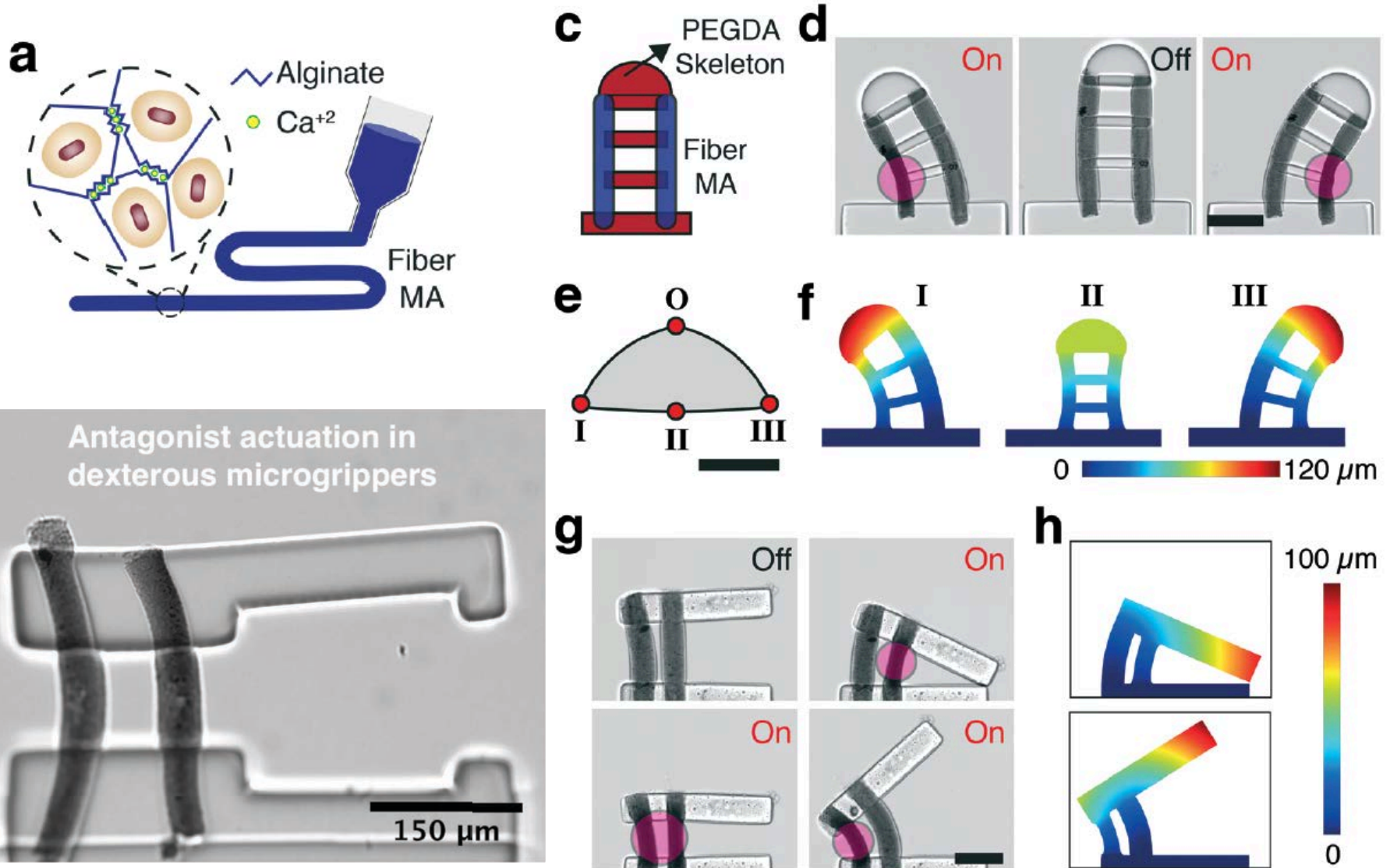
$$\epsilon = \frac{R_0 - R}{R_0} \times 100$$



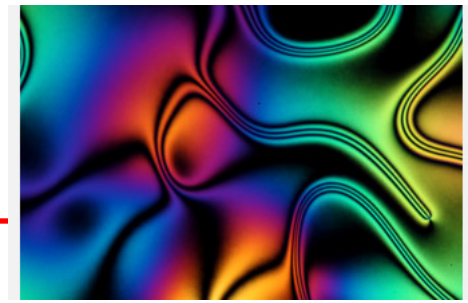
Hierarchical Assembly and Control



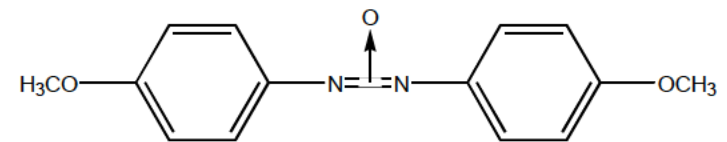
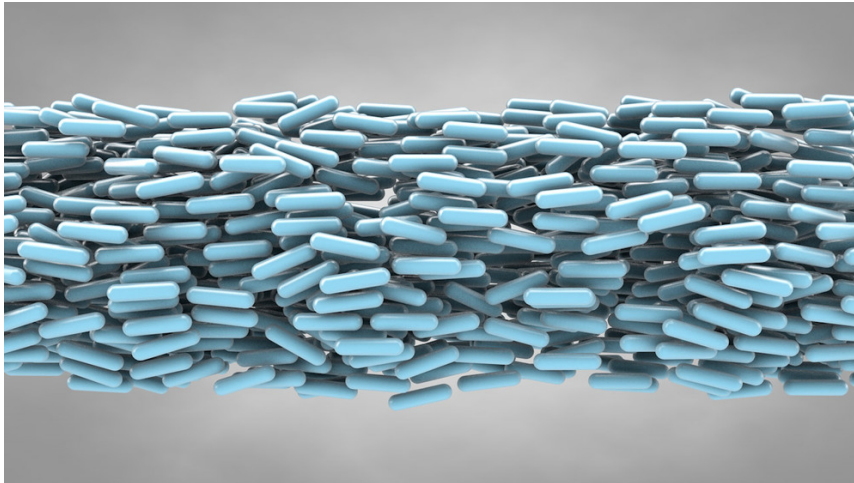
Hierarchical Assembly and Control



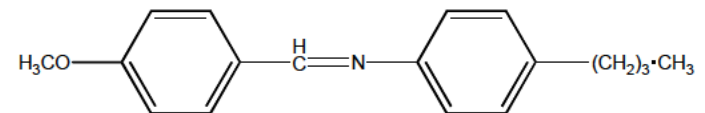
Nematic Liquid Crystals



- Comes from the Greek word for thread
- Preferred molecular orientation defines the director \mathbf{n}
 - Rod-like molecules are spontaneously and collectively aligned into a certain direction
- Director \mathbf{n} varies from point to point at macroscale
- 1D order where molecule centers are not oriented



PAA: p-azoxyanisole

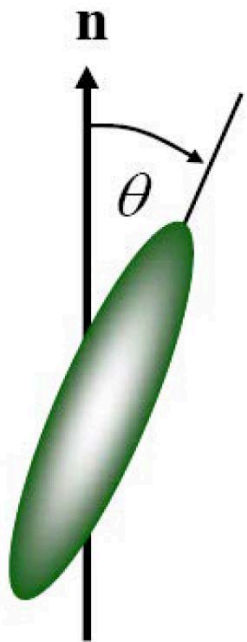


MBBA: n-(p-methoxybenzylidene)-
p-butylaniline

Order Parameter

- Quantitative description of the orientation of the mesogens
- Director \mathbf{n} : Anisotropy is defined by the symmetry axis of the orientation distribution

$$S = (3\cos^2\theta - 1)/2$$



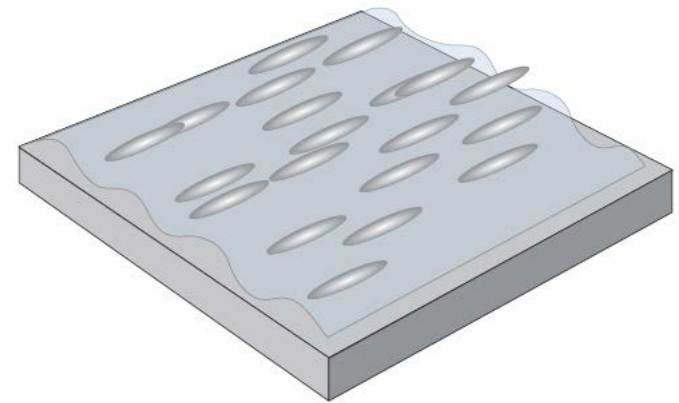
θ = Average deviation angle of the mesogen axes from the director

- All molecules aligned parallel to the director: $S = 1$
- Random distribution: $S = 0$
- Nematic phase: $0.45 < S < 0.65$
- Smectic phase: $0.85 < S < 0.95$

Hierarchy of Orientation

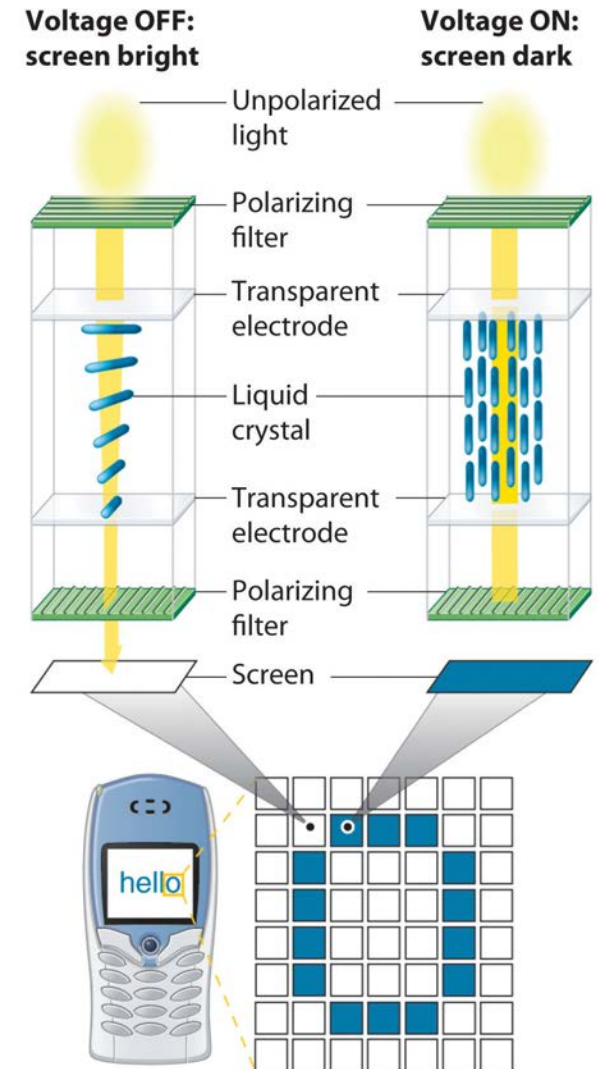
- Orientation of mesogens in domains
 - Domain size in the μm range
 - Orientation of the molecular axes with respect to the director inside each domain
- The directors of the domains are statistically distributed
- Uniform alignment of the domains
 - Rubbing
 - Aligned substrates
 - Application of magnetic or electric field
 - Viscous fingering

Planar alignment



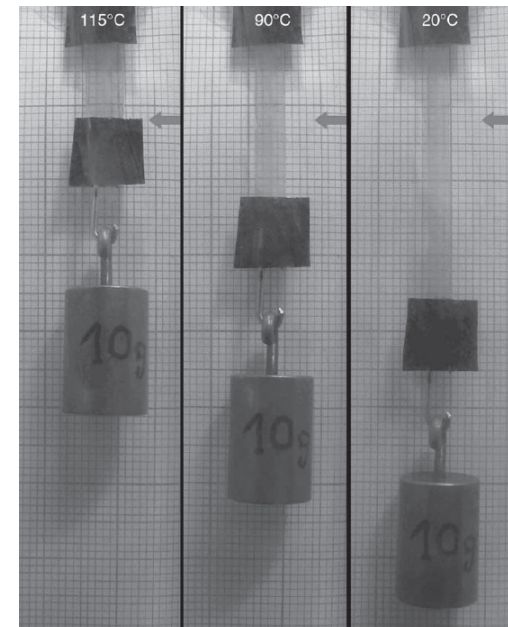
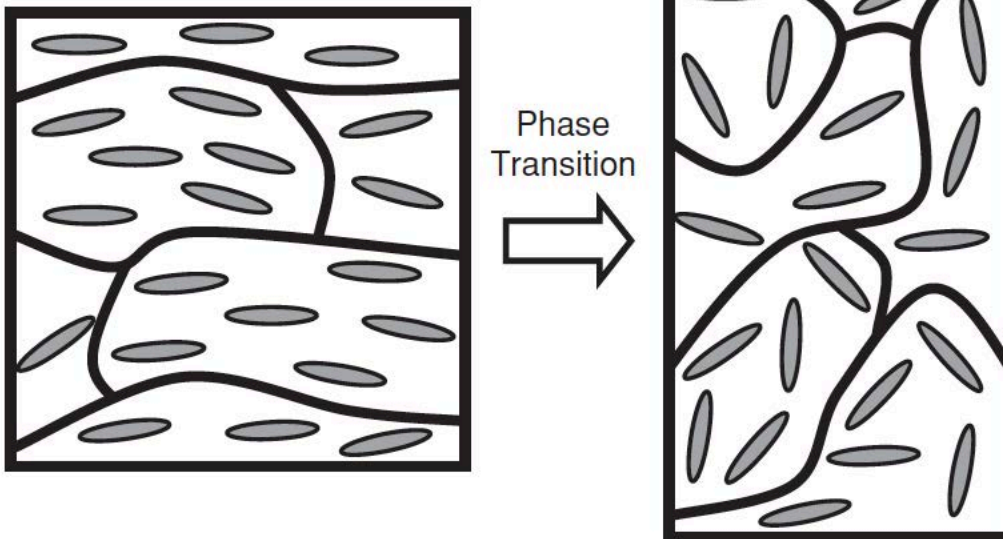
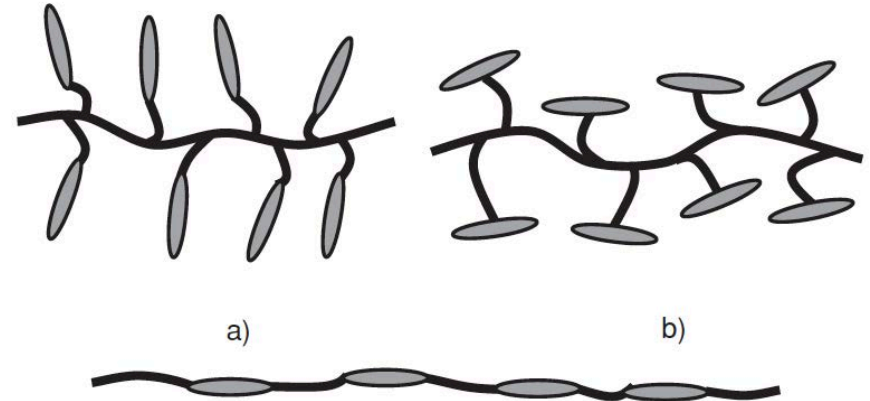
Liquid Crystal Displays

- Mesogens are polar,
 - interact with an electric field
 - change the orientation
- Nematic liquid crystals tend to be relatively translucent
- They become opaque when an electric field is applied and the molecular orientation changes
- This behavior is ideal for producing dark images on a light or an opalescent background



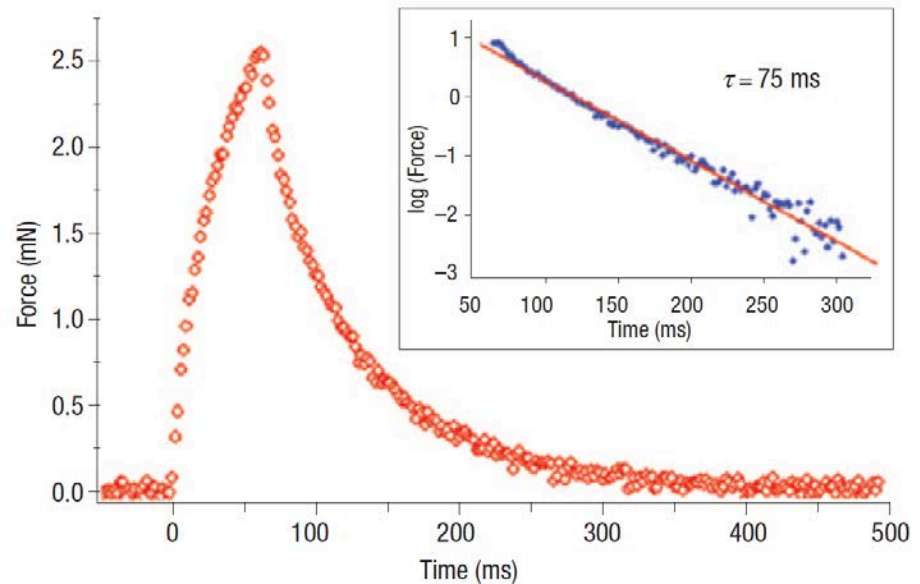
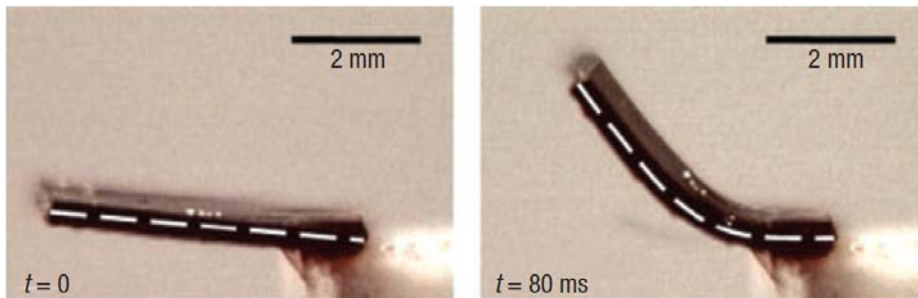
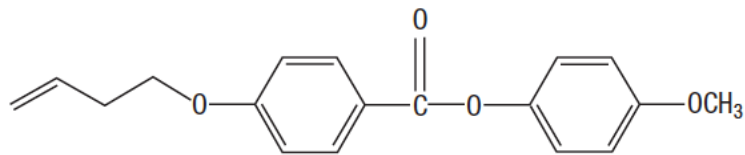
Liquid Crystal Elastomers

- Coupling between the mesogens and polymer chains
 - (a) end-on
 - (b) side-on
 - (c) main-chain



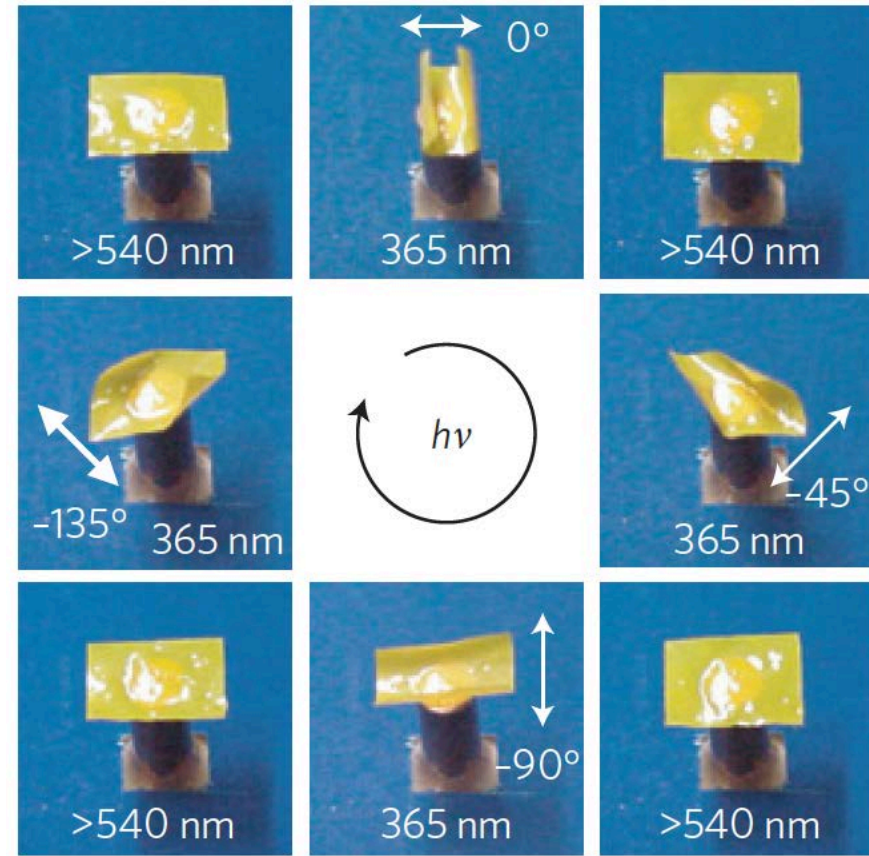
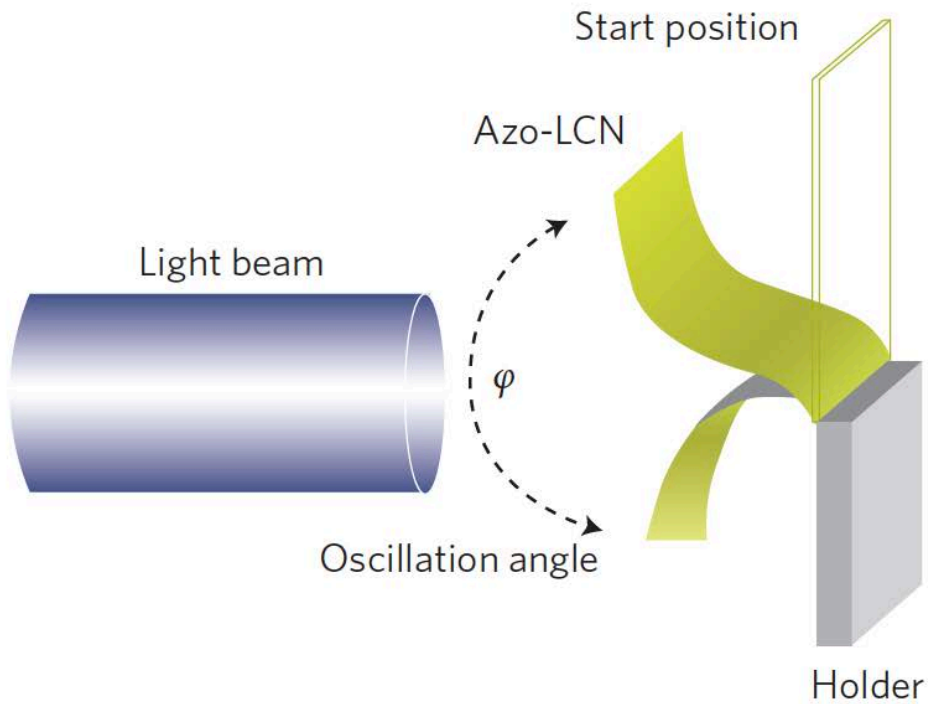
External control with light

- Dopants containing azobenzene moieties: covalent bonding or dissolving
- Change in the degree of order
 - Photoisomerization of the dissolved dye
 - Photoisomerize between trans- and cis-states in the presence of linear polarized light at specific wavelengths



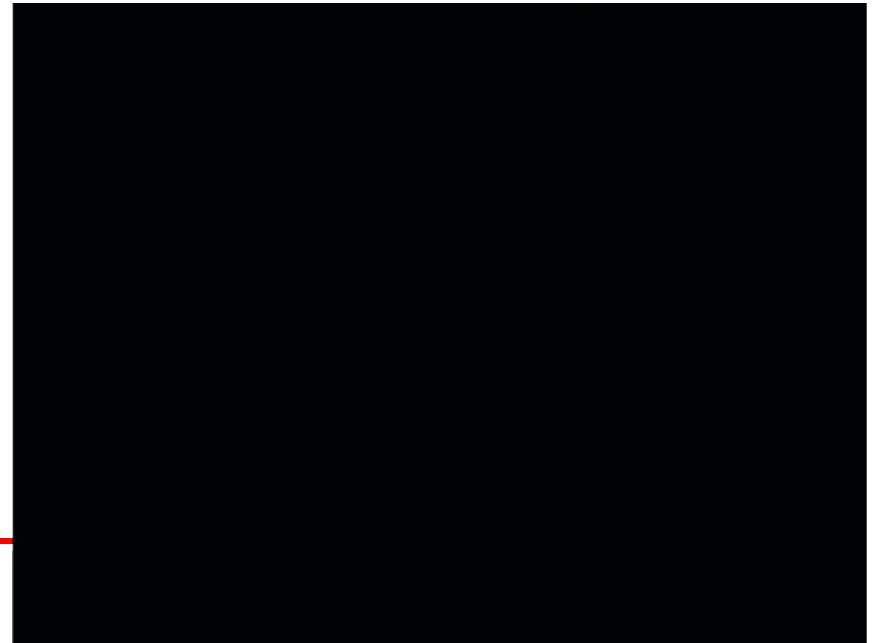
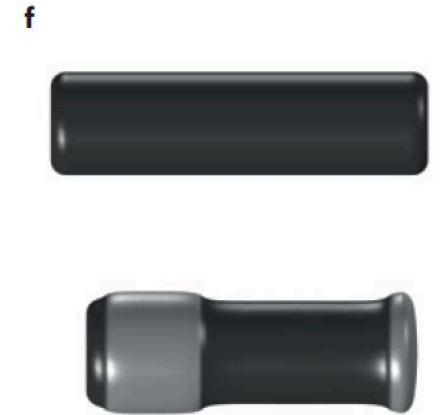
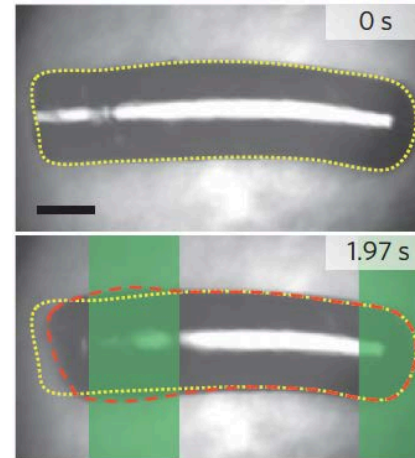
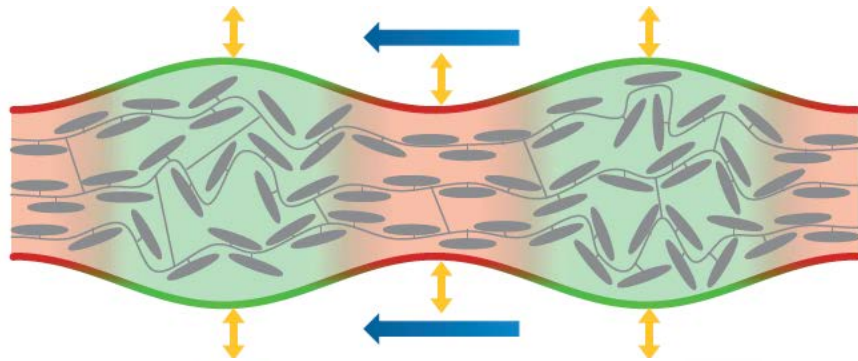
External control with light

- Intensity, polarization, and wavelength of light



Biomimetic Swimming

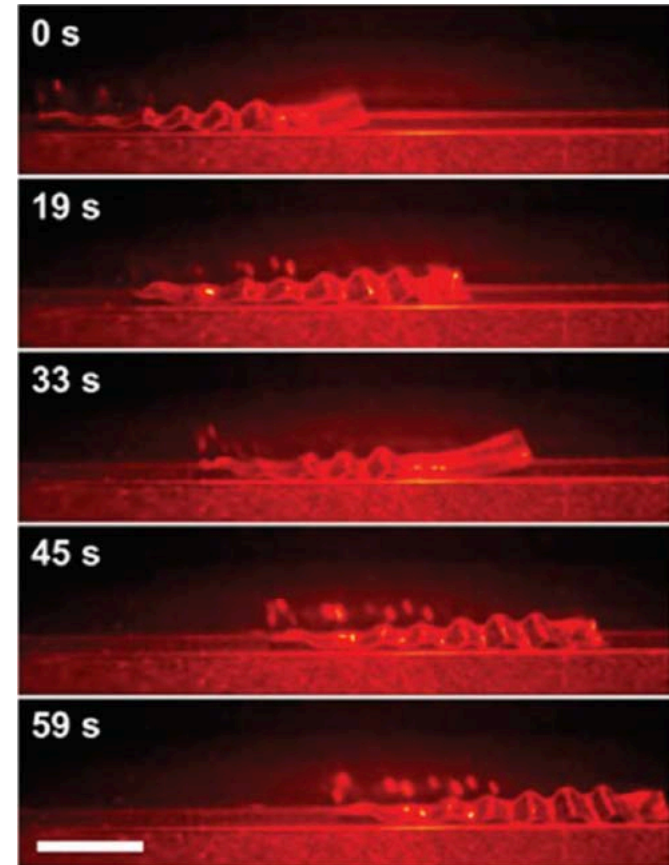
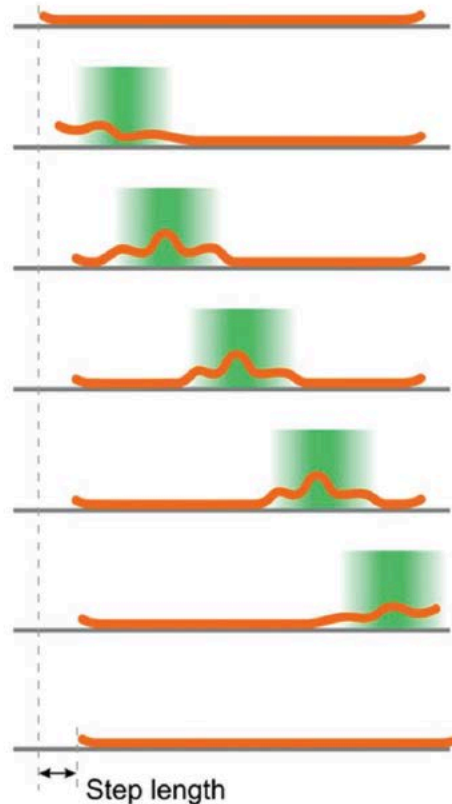
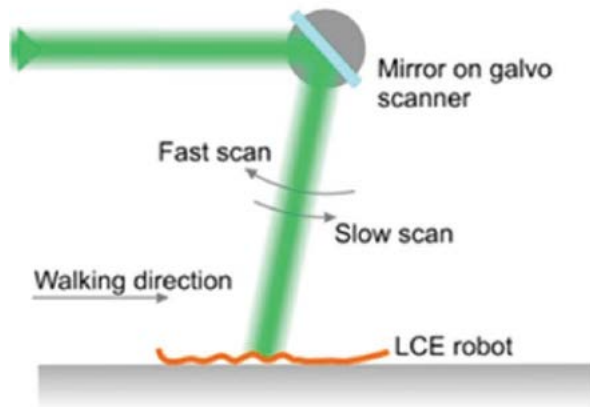
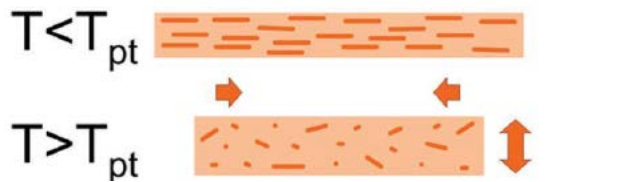
- Generating of a travelling wave under periodic light pattern



Biomimetic Crawling

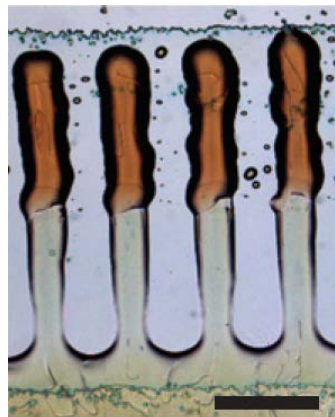
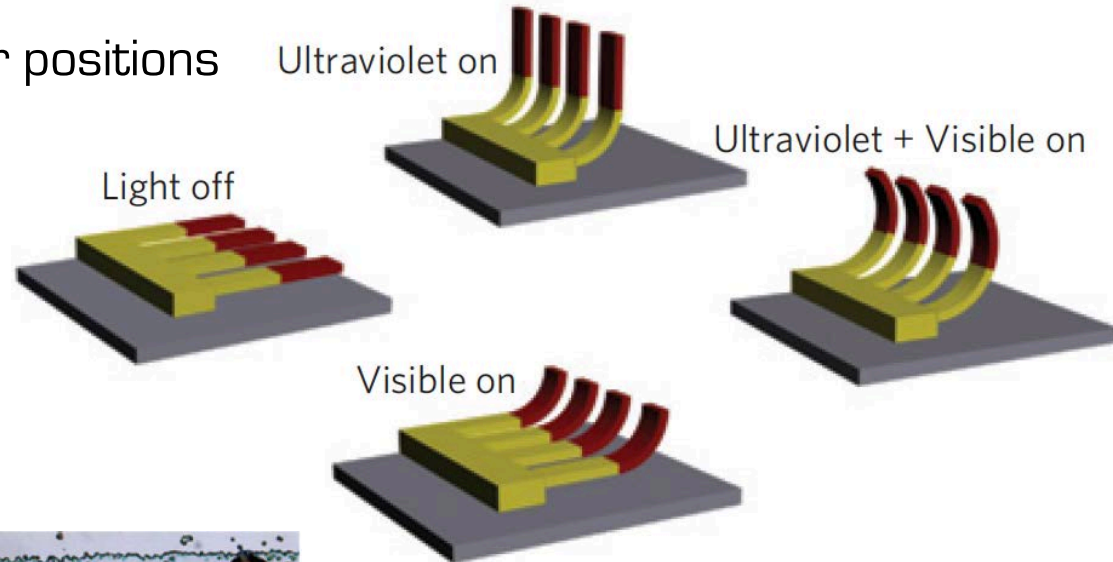
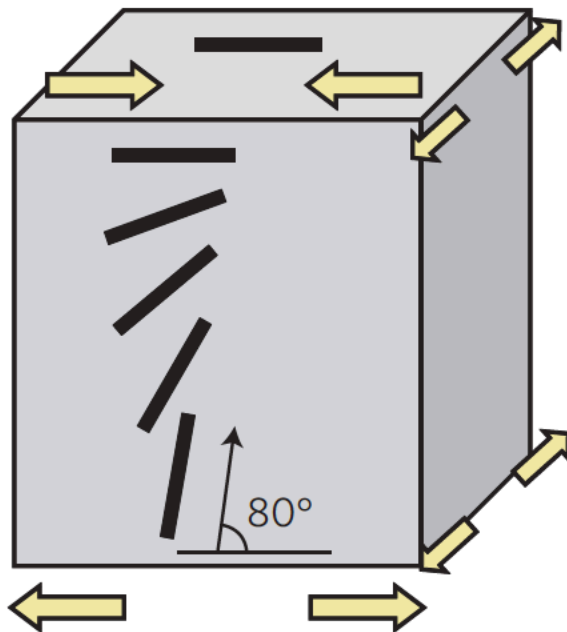
movie

- Spatially modulated light field to trigger synchronized, time-dependent body deformations
- Scanning a laser beam

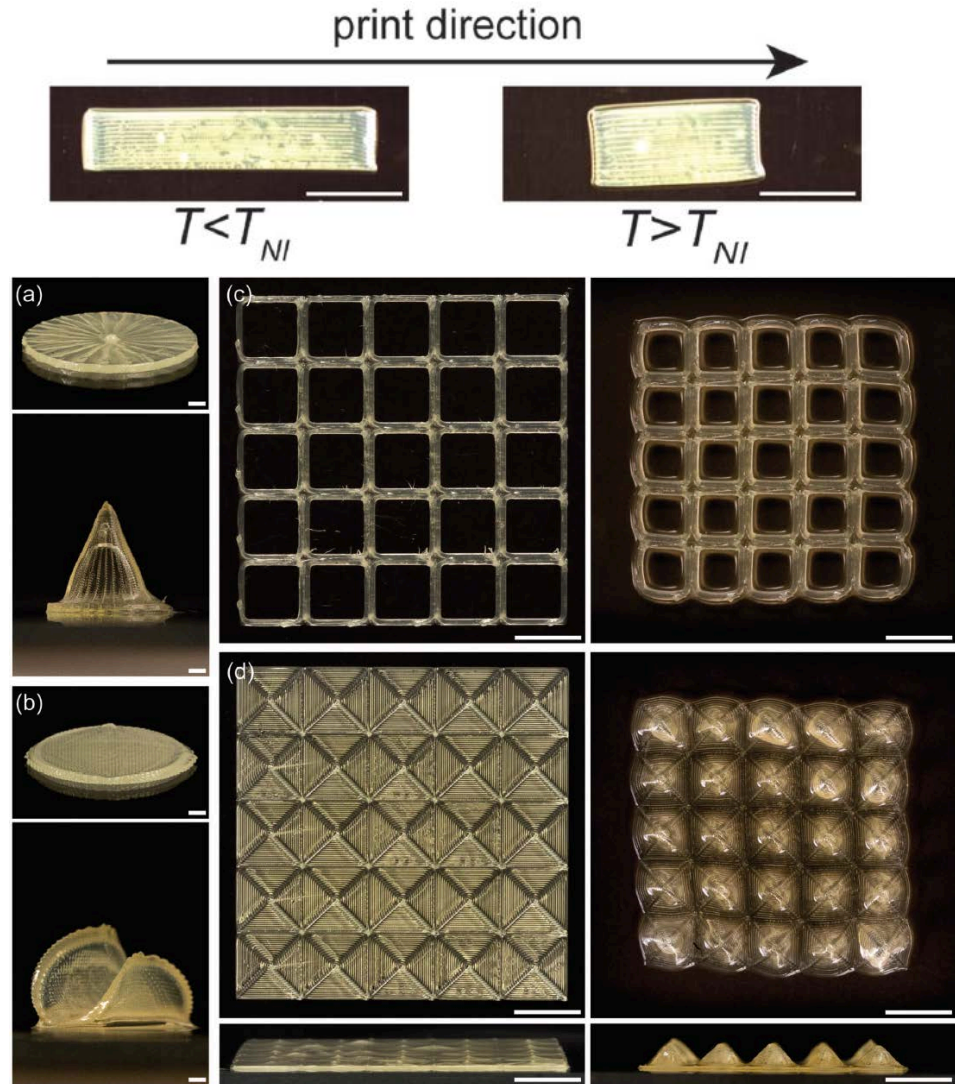
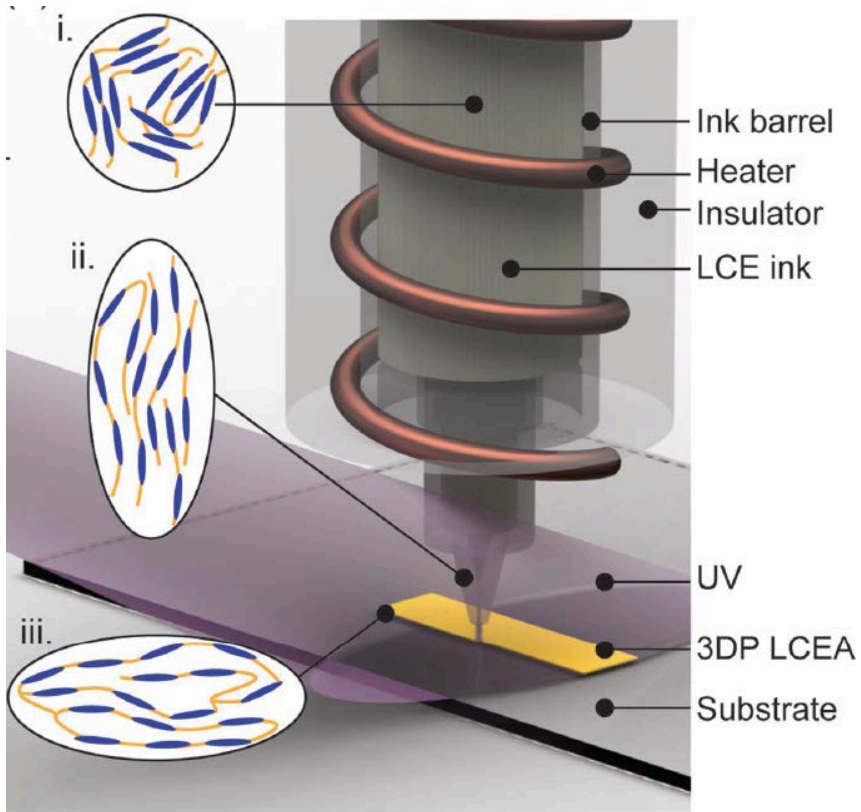


Artificial Cilia

- Asymmetric motion controlled by the spectral composition of light
 - Two different dyes
 - Switching between four positions



3D Printing LCE Actuators

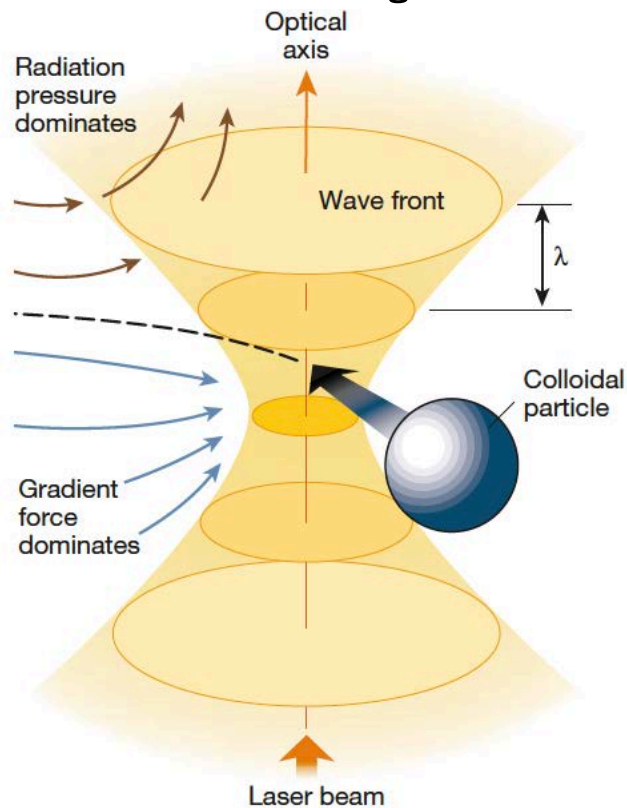


Optical tweezers

- **Maxwell:** Momentum transfer from the electromagnetic field to an object, due to absorption or reflection, should result in a radiation pressure in the propagation direction of the wave.
- Optical potential well or optical bottle
 - Tailor the properties of electromagnetic field to generate a pattern of intensity gradients that can act as a 3D trap
 - Adjusting the location of the trap allows the particle to be moved
 - Optical forces act in a highly localized space
 - Particle size and refractive index difference matter
- Spatial light modulators create holographic optical patterns and multiple optical traps

Optical tweezers

- Non-uniform spatial distribution of light in the vicinity of the beam focus: a gradient force
- A scattering levitation force along the beam axis: harmonic oscillator



Optical force at a single point on the surface

$$\langle \mathbf{f} \rangle = \frac{1}{4} |E|^2 \Delta \epsilon \delta(\mathbf{n}) \hat{\mathbf{n}}$$

E : total electric field acting on the surface element

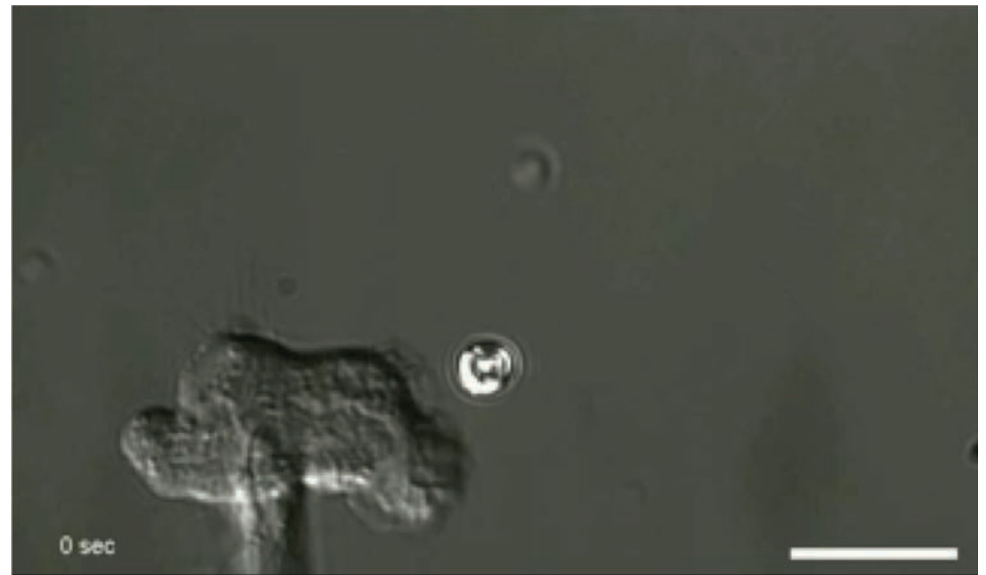
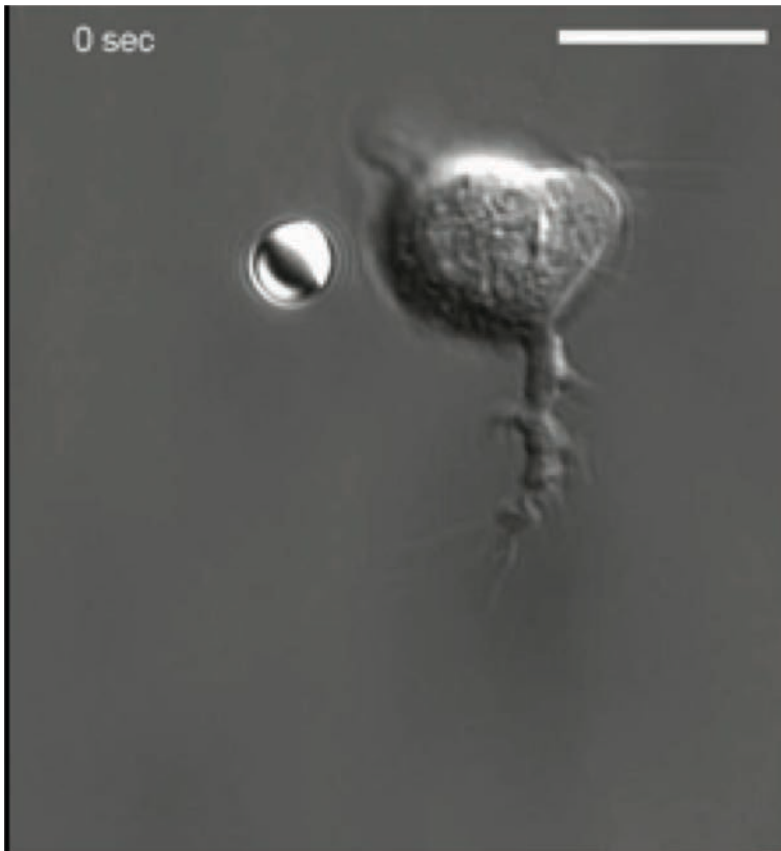
ϵ : Dielectric constant

n : Unit surface normal

δ : Dirac delta function centered at the material surface

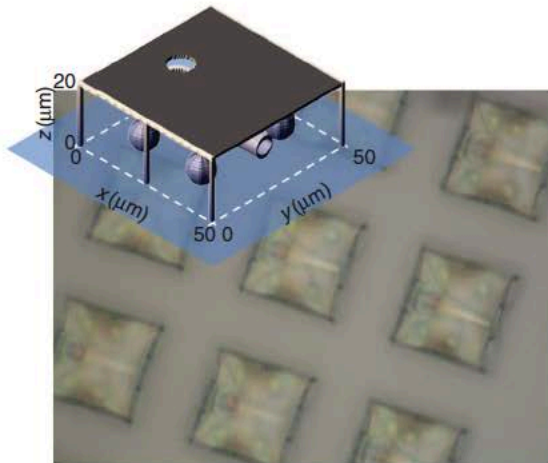
Optically actuated microtools

- Cell stimulation with optically manipulated drug-loaded polymer particles (2 μm)

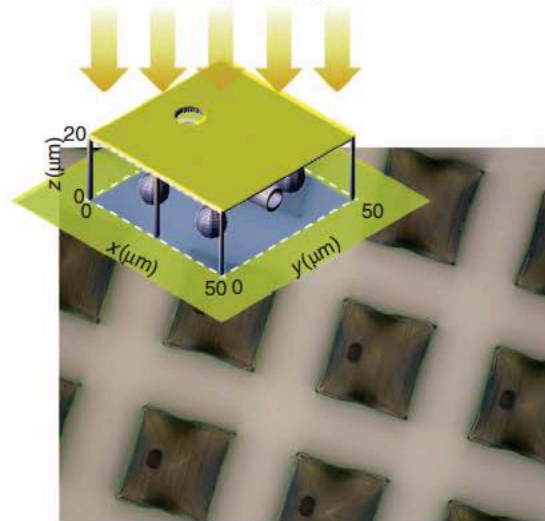


Optically actuated microtools

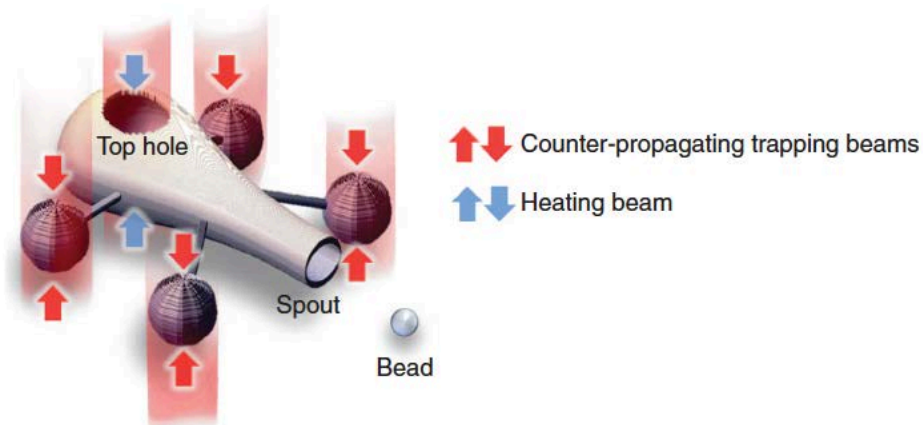
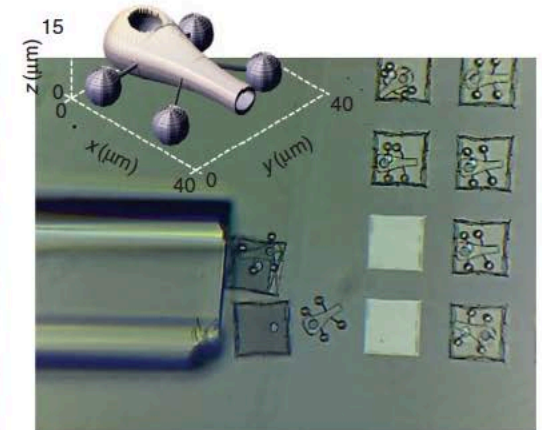
a Two-photon-polymerization of micro-tools and masks



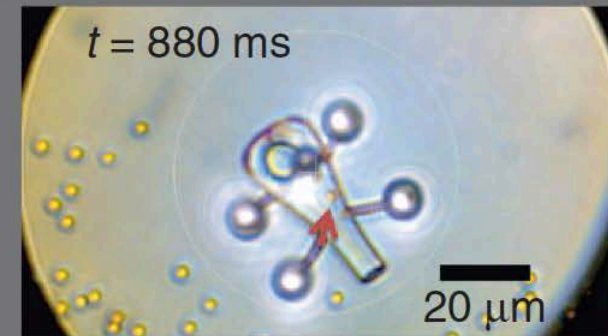
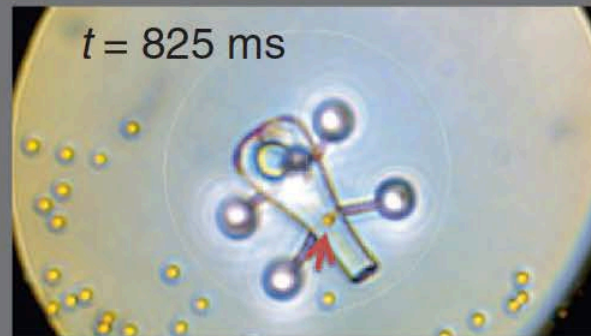
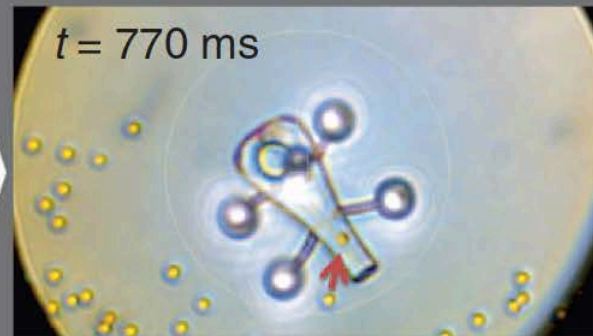
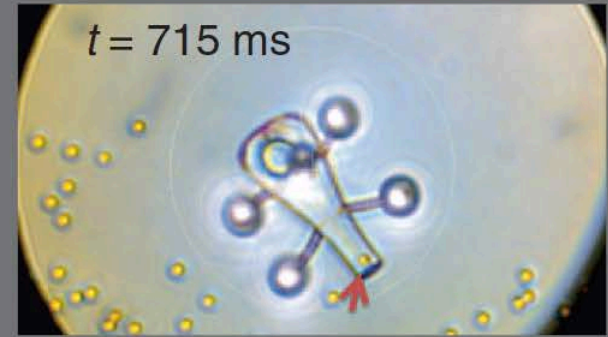
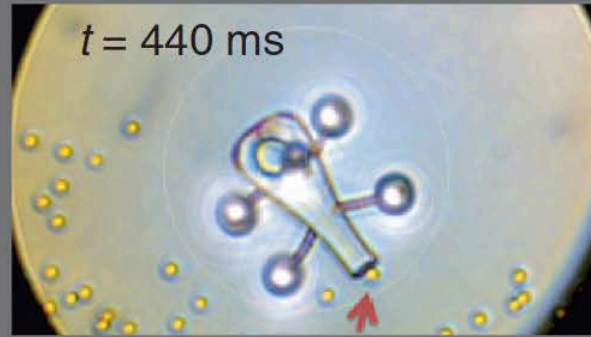
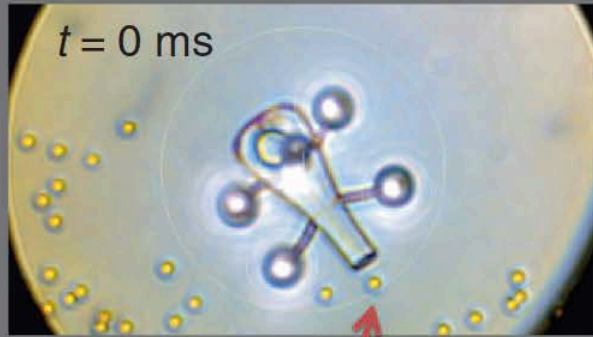
b Electron beam physical vapor deposition



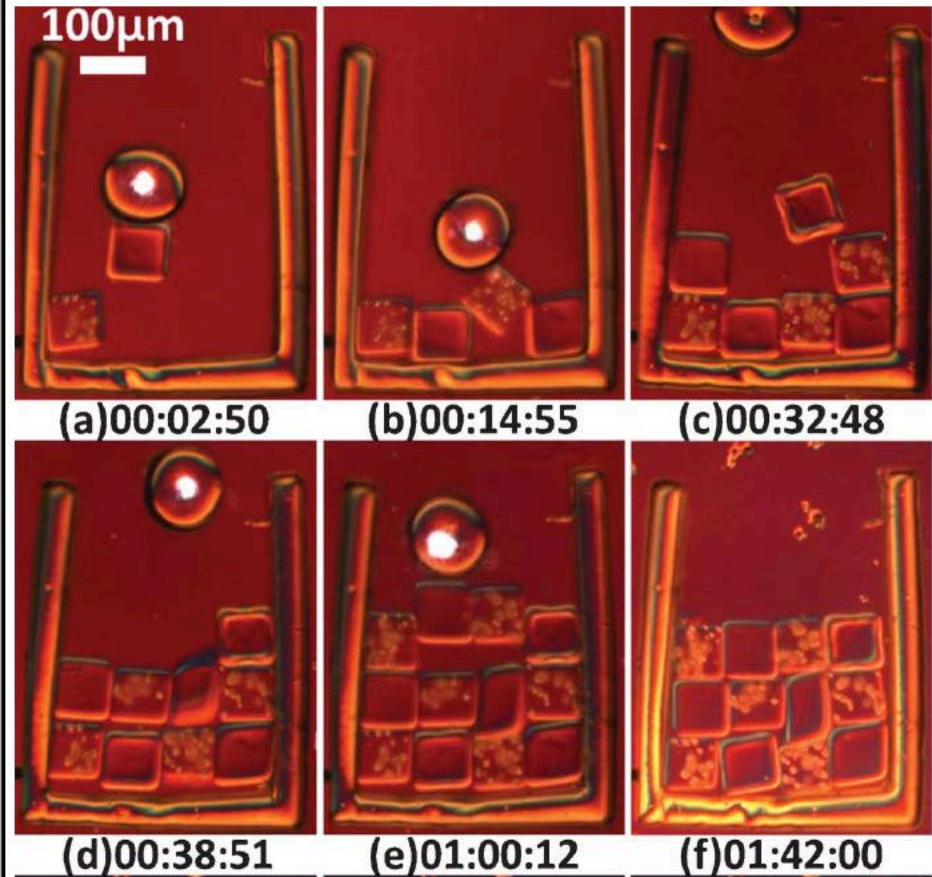
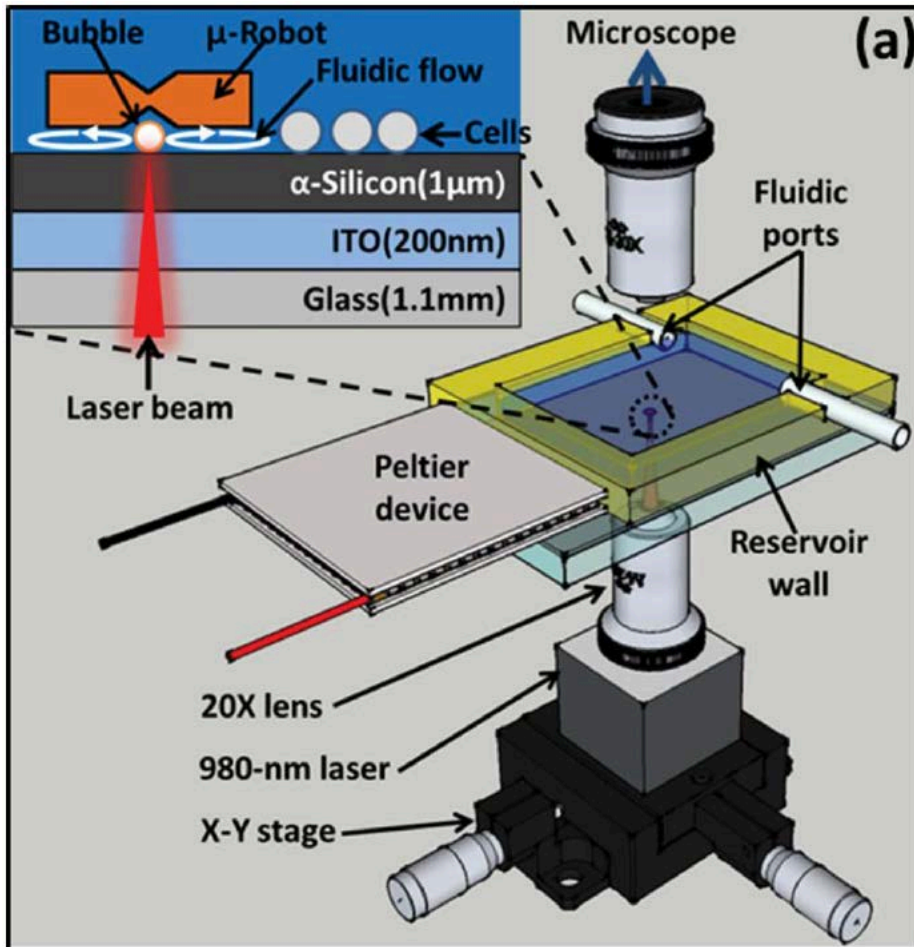
c Collection of micro-tools



Optically actuated microtools



Optically actuated microtools



Beam-powered propulsion or Light craft

- Solar (light) Sails
 - Radiation pressure exerted by the light source
 - Einstein's relation: $p = E/c$ (E: energy of the photon or flux, c: speed of light)
 - Thin reflective mirror
 - Analogous to sailing boat; light-mirror vs wind-sail

Optical reaction turbine

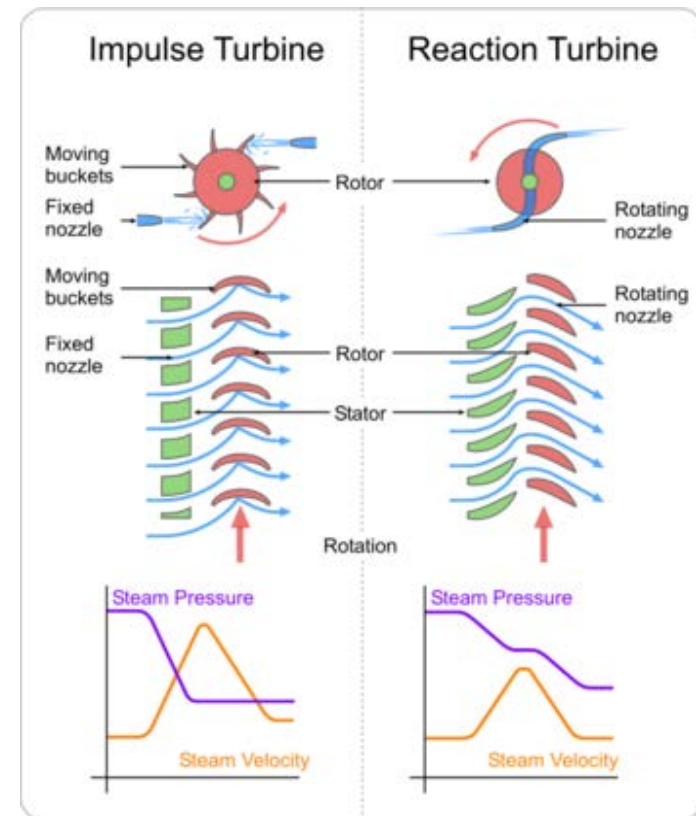
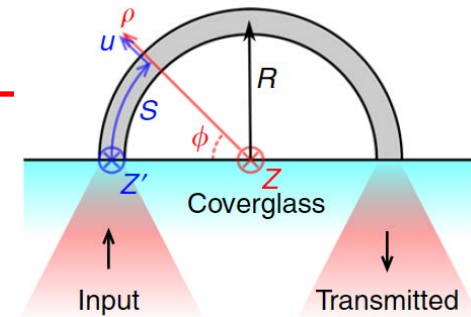
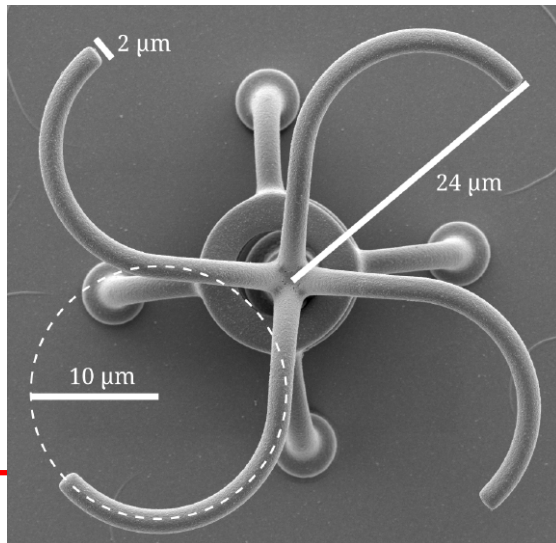
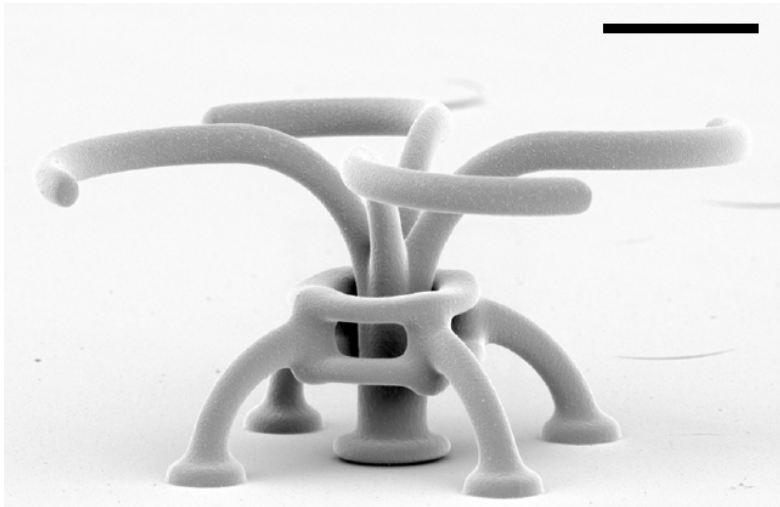
- Exploiting light's momentum to generate torque

$$T_z = \frac{Pn}{c} \left(k_\phi^{\text{out}} r^{\text{out}} - k_\phi^{\text{in}} r^{\text{in}} \right)$$

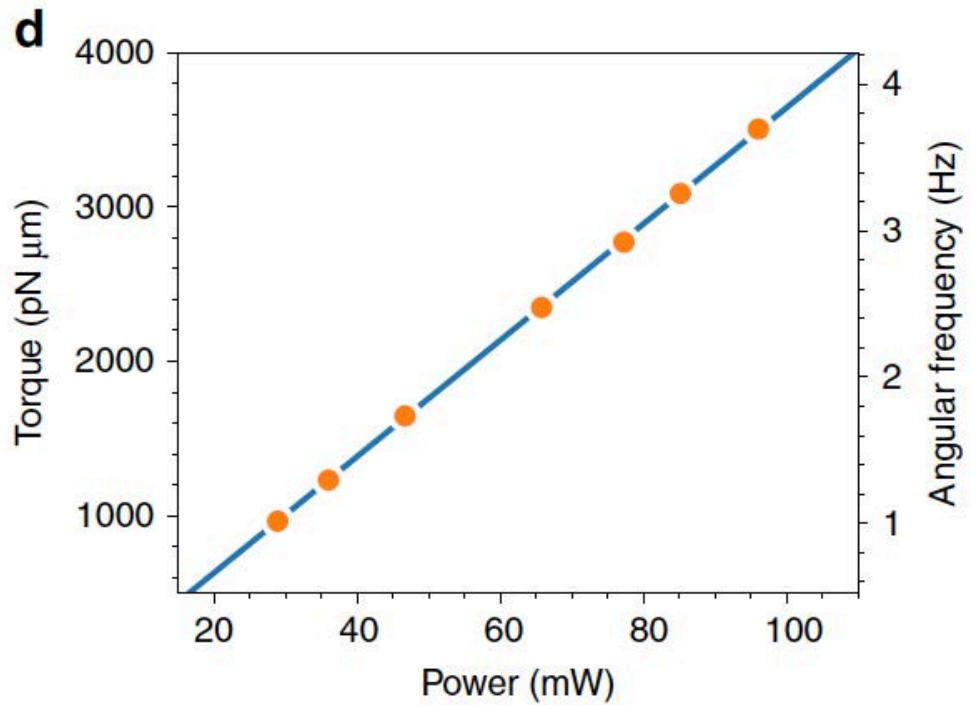
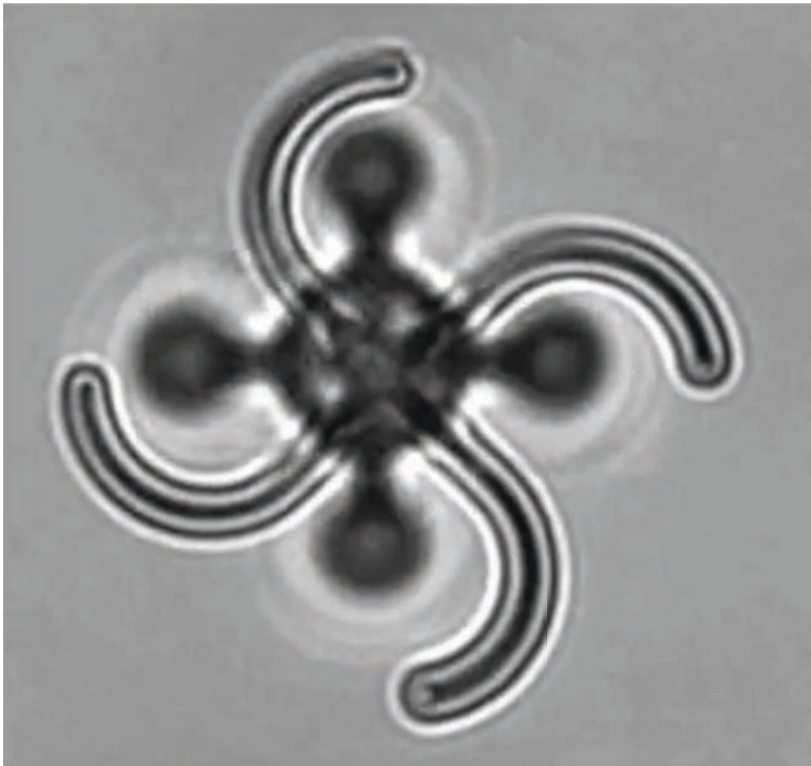
where P is the optical power, n is the refractive index of the surrounding medium, z is the direction of the rotor axis, ϕ the azimuthal coordinate, k_ϕ^{in} and k_ϕ^{out} the azimuthal components of respectively incoming and outgoing light directions and r^{in} and r^{out} the radial distances of inlet and outlet (Fig. 1a). Equation (1) is formally very similar to the Euler turbomachine equation¹ expressing torque in hydraulic turbines and where P is replaced by mass flow and nk_ϕ^{in}/c , nk_ϕ^{out}/c by the azimuthal components of inlet and outlet velocities.

Optical reaction turbine

- Design to optimize momentum transfer (garden sprinkler)



Optical reaction turbine



Magnetic Actuation

- For small bodies, e.g. microrobots, we assume:
 - Uniform distribution of the applied field \mathbf{B} throughout the body
 - \mathbf{M} is a single vector (body is viewed as a dipole)

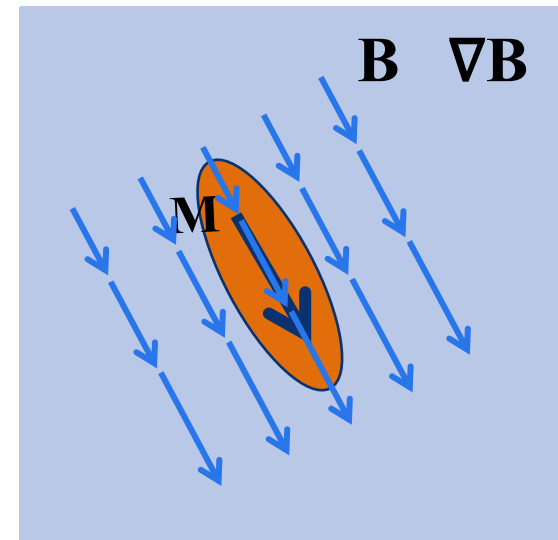
■ Magnetic Torque: $\mathbf{T} = v \mathbf{M} \times \mathbf{B}$

Object System

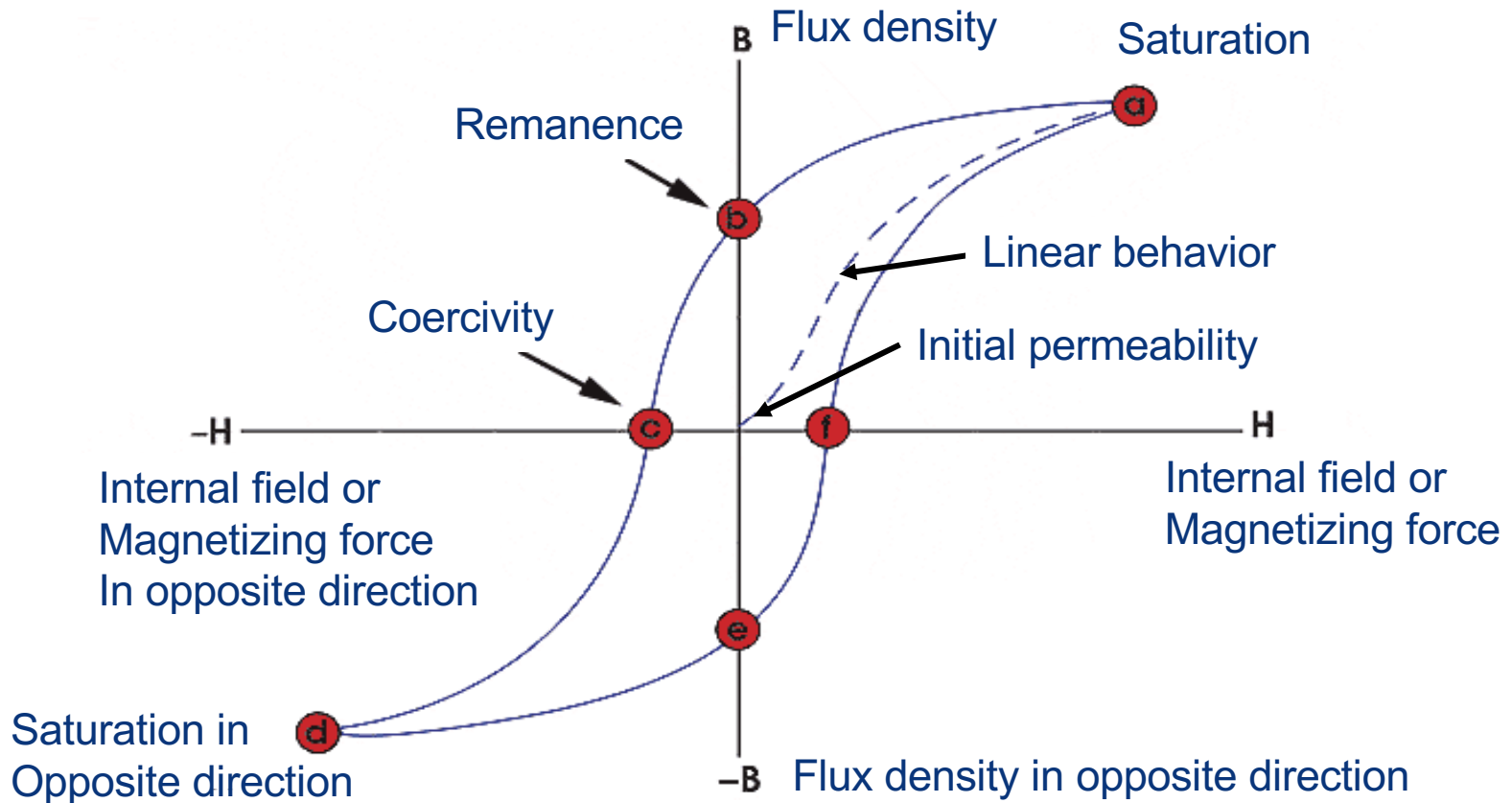
■ Magnetic Force: $\mathbf{F} = v (\mathbf{M} \cdot \nabla) \mathbf{B}$

$\nabla \times \mathbf{B} = 0$

$$\mathbf{F} = v \left[\begin{array}{ccc} \frac{\partial \mathbf{B}}{\partial x} & \frac{\partial \mathbf{B}}{\partial y} & \frac{\partial \mathbf{B}}{\partial z} \end{array} \right]^T \mathbf{M}$$



Hysteresis Loop

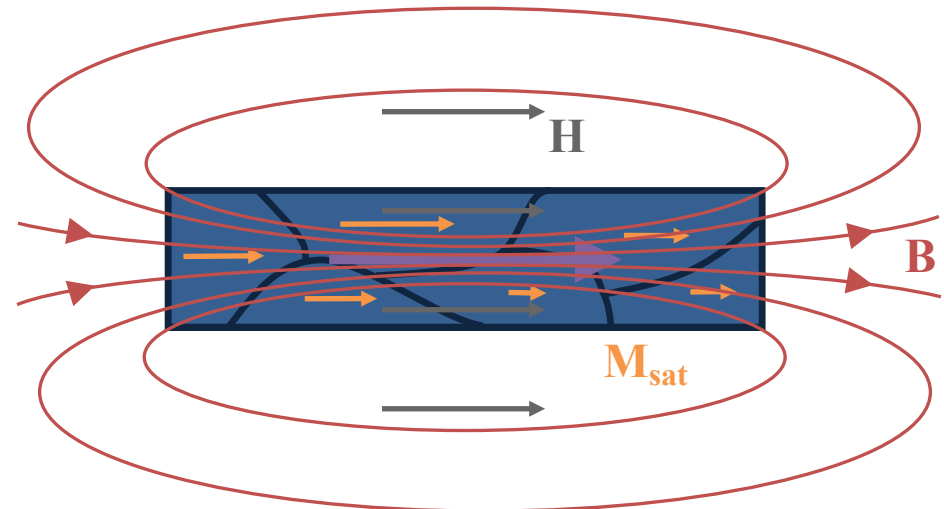
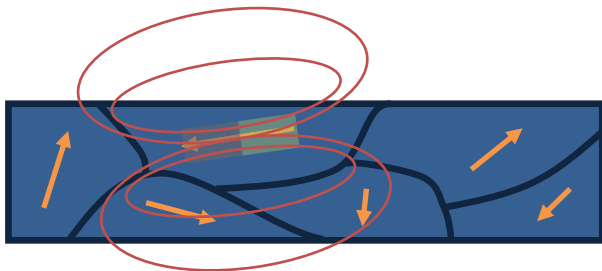


Remanence and Coercivity

- They depend on sample shape, surface roughness, microscopic defects, and thermal history
- Also depends on the rate at which the field is swept in order to trace the hysteresis loop

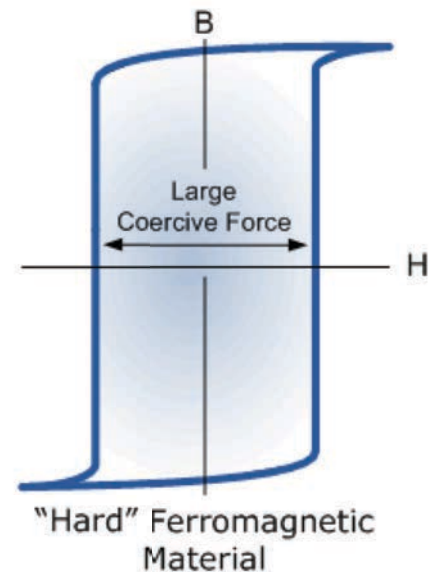
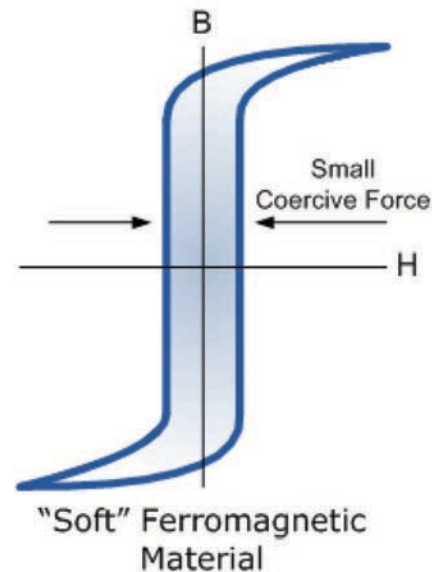
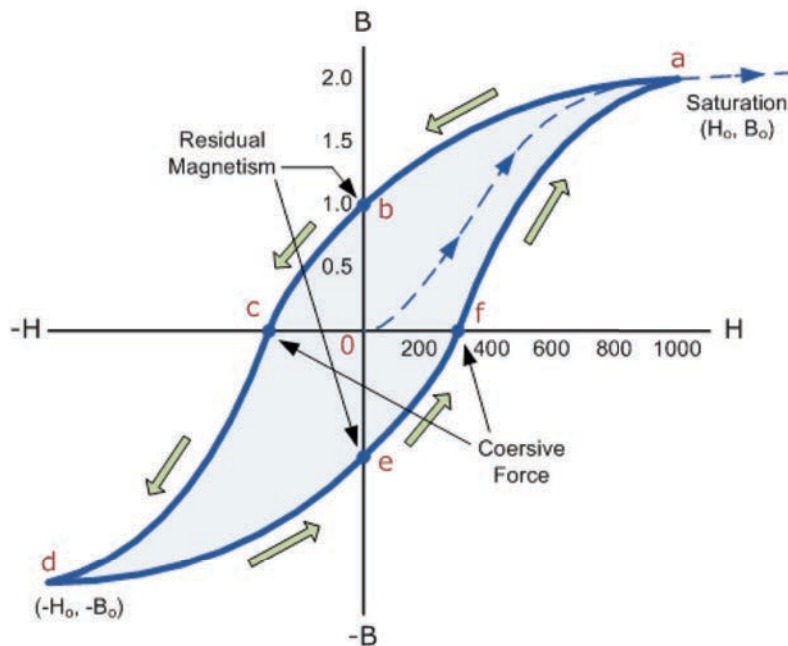
Magnetization

- What happens when a ferromagnetic material is placed in a sufficiently strong magnetic field?
 - The domain walls move
 - The domains reorient in parallel with the applied field and a net field is generated. If all domains are oriented, the saturation occurs. Increasing the applied field further has no effect anymore.
 - The phenomenon that the material undergoes when it is placed in the magnetic field is called magnetization (and denoted by the vector \mathbf{M}).



Magnetization

- Magnetization is a vector field $\mathbf{M} = \mathbf{M}(x,y,z)$ (as are \mathbf{B} and \mathbf{H})
- In hard magnetic materials (permanent magnets)
 - Once magnetized: M is independent of H
- In soft magnetic materials, \mathbf{M} and \mathbf{H} are related
- The forces and torques depend on the field around the body

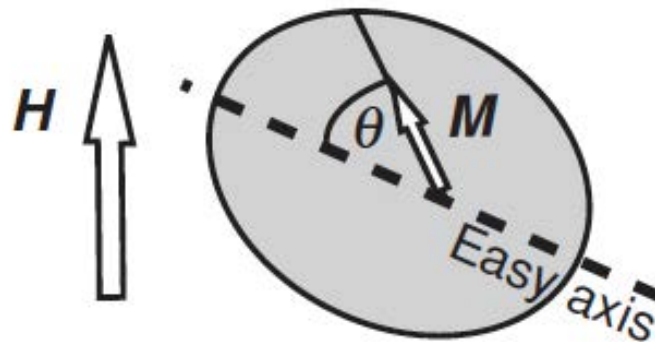


Easy Axis

- The natural direction of magnetization is usually constrained to lie along one or more easy axes
- This tendency is represented by the anisotropy energy

$$E_a = K_u \sin^2 \theta$$

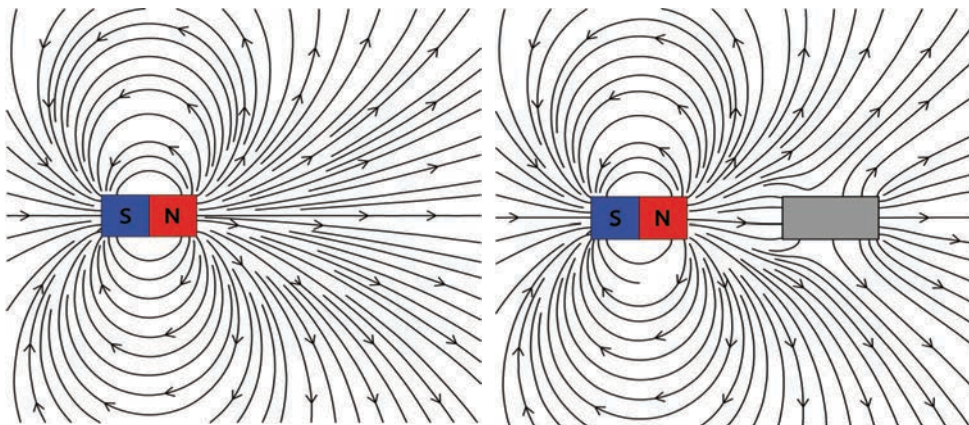
- Shape matters: Magnetization of the object is not necessarily parallel to the applied field



Magnetic Field Generation

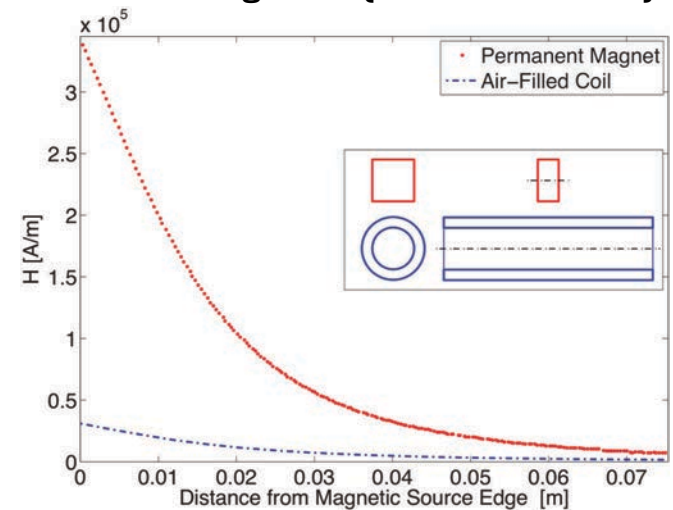
Permanent Magnets

- + Strong field on a per volume basis
- + Miniaturization
- Interaction between adjacent magnets
- Actuation required to control the field strength
- Magnets always on, special shielding mechanism needed to turn field off



Electromagnets

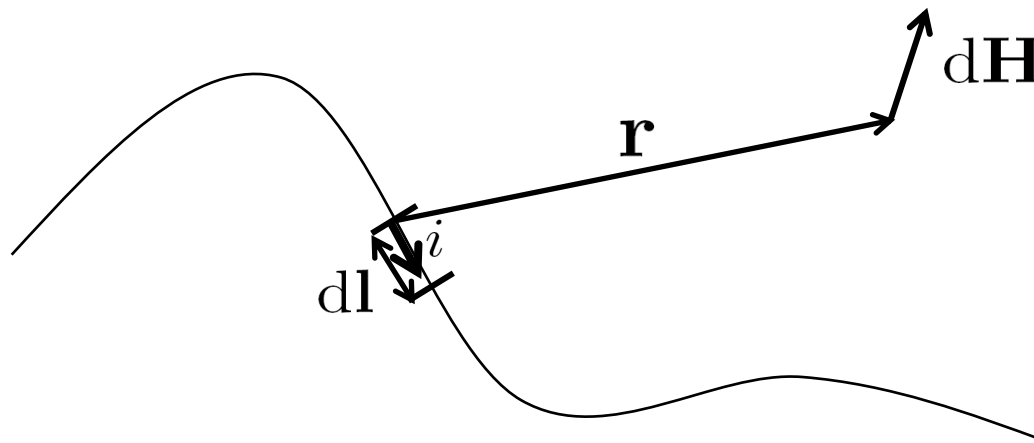
- + Linear superposition of individual field contributions with air core
- + Field strength can be adjusted through current
- + Field can “immediately” be switched on and off
- Weak field strength compared to permanent magnets (for same size)



Biot-Savart Law

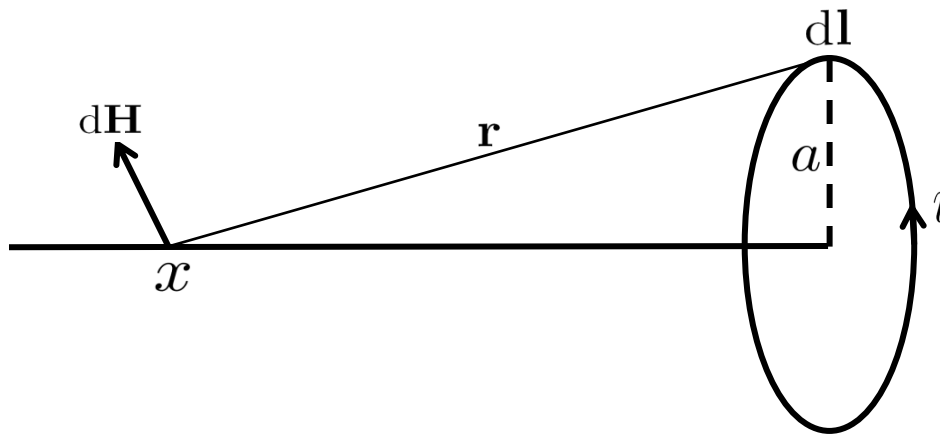
- Calculates the magnetic field \mathbf{H} generated by an electrical current i :

$$d\mathbf{H} = \frac{1}{4\pi|\mathbf{r}|^2} i d\mathbf{l} \times \hat{\mathbf{r}}$$



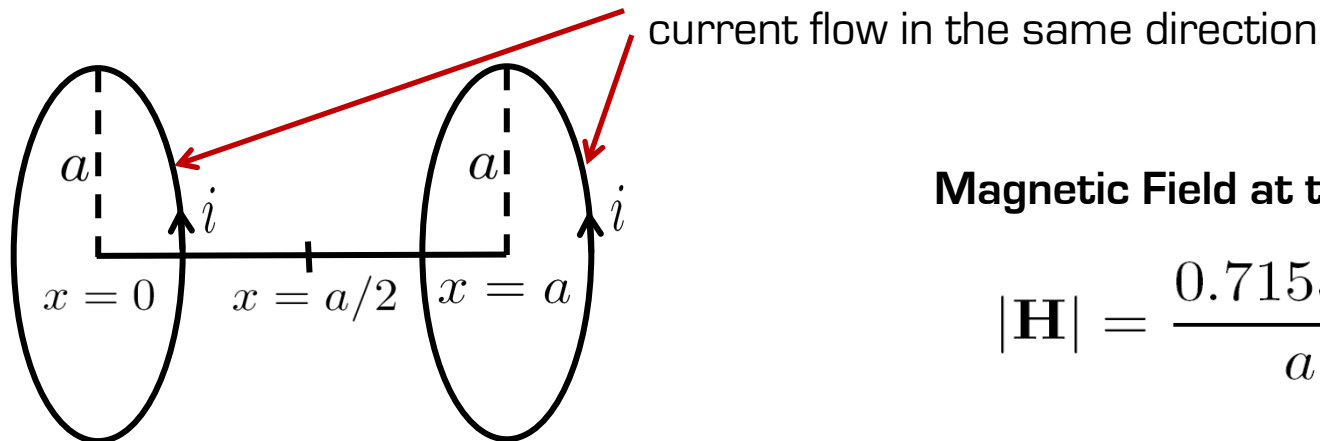
Helmholtz Coil

- Magnetic field \mathbf{H} at a distance x along the centerline:



$$|\mathbf{H}| = \frac{ia^2}{2(a^2 + x^2)^{3/2}}$$

$$= \left(\frac{i}{2a}\right) \left(1 + \frac{x^2}{a^2}\right)^{-1.5}$$

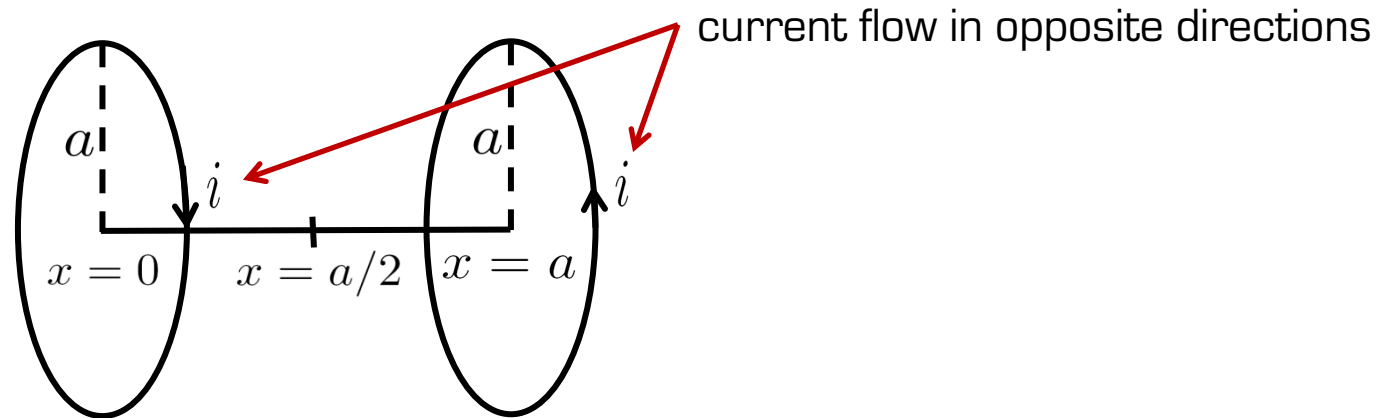


Magnetic Field at the center

$$|\mathbf{H}| = \frac{0.7155Ni}{a}$$

Maxwell Coil

- Uniform magnetic field gradient in the center



Magnetic Field at the center

$$|\mathbf{H}| = \left(\frac{Ni}{2a} \right) \left[\left(1 + \frac{x^2}{a^2} \right)^{-1.5} - \left(1 + \frac{(a-x)^2}{a^2} \right)^{-1.5} \right] = 0$$

Control with Stationary Electromagnets

- Within a given static arrangement of electromagnets, every electromagnet creates a field throughout the workspace that can be pre-computed
- Field magnitude at a given point P can be expressed as a unit-current vector [T/A] multiplied by a scalar current value [A]:

$$\mathbf{B}_e(\mathbf{P}) = \tilde{\mathbf{B}}_e(\mathbf{P})i_e \quad e: \text{denotes } e^{\text{th}} \text{ electromagnet}$$

- $\mathbf{B}_e(\mathbf{P})$: Field due to current flowing through electromagnet e and due to soft-magnetic cores in all other electromagnets

Control with Stationary Electromagnets

- Assumptions:
 - Field contribution of a given electromagnet was precomputed
 - Use of soft-magnetic core material with negligible hysteresis
 - Operation of the system with the cores in their linear magnetization region
- Field contributions of the individual currents (each of which affect the magnetization of every core) superimpose linearly

$$\mathbf{B}(\mathbf{P}) = \sum_{e=1}^n \mathbf{B}_e(\mathbf{P}) = \sum_{e=1}^n \tilde{\mathbf{B}}_e(\mathbf{P}) i_e$$

$$\mathbf{B}(\mathbf{P}) = \left[\tilde{\mathbf{B}}_1(\mathbf{P}) \quad \cdots \quad \tilde{\mathbf{B}}_n(\mathbf{P}) \right] \begin{bmatrix} i_1 \\ \vdots \\ i_n \end{bmatrix} = \mathcal{B}(\mathbf{P}) \mathbf{I}$$

Control with Stationary Electromagnets

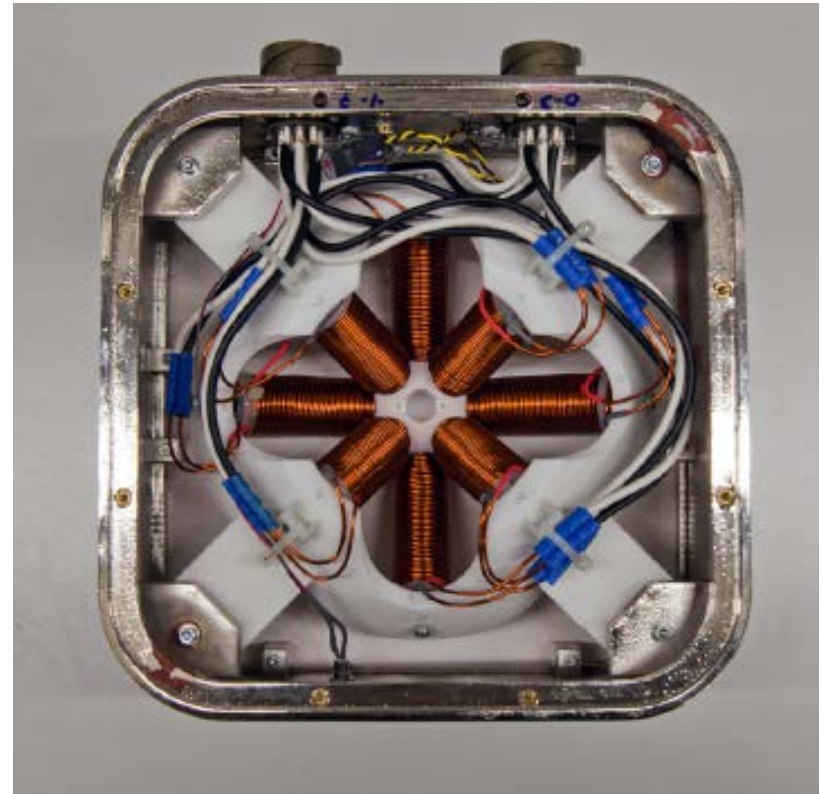
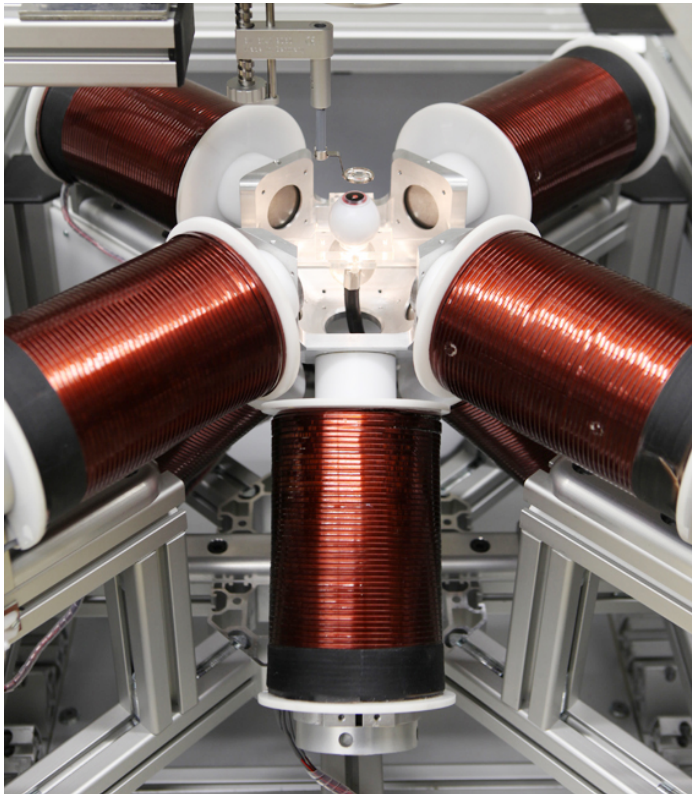
- The derivative of the field in a given direction in a specific frame can also be expressed as the contributions from each of the currents:

$$\frac{\partial \mathbf{B}(\mathbf{P})}{\partial x} = \begin{bmatrix} \frac{\partial \tilde{\mathbf{B}}_1(\mathbf{P})}{\partial x} & \dots & \frac{\partial \tilde{\mathbf{B}}_n(\mathbf{P})}{\partial x} \end{bmatrix} \begin{bmatrix} i_1 \\ \vdots \\ i_n \end{bmatrix} = \mathcal{B}_x(\mathbf{P})I$$
$$\frac{\partial \mathbf{B}(\mathbf{P})}{\partial z} = \begin{bmatrix} \frac{\partial \tilde{\mathbf{B}}_1(\mathbf{P})}{\partial z} & \dots & \frac{\partial \tilde{\mathbf{B}}_n(\mathbf{P})}{\partial z} \end{bmatrix} \begin{bmatrix} i_1 \\ \vdots \\ i_n \end{bmatrix} = \mathcal{B}_z(\mathbf{P})I$$
$$\frac{\partial \mathbf{B}(\mathbf{P})}{\partial y} = \begin{bmatrix} \frac{\partial \tilde{\mathbf{B}}_1(\mathbf{P})}{\partial y} & \dots & \frac{\partial \tilde{\mathbf{B}}_n(\mathbf{P})}{\partial y} \end{bmatrix} \begin{bmatrix} i_1 \\ \vdots \\ i_n \end{bmatrix} = \mathcal{B}_y(\mathbf{P})I$$

$\mathcal{B}(\mathbf{P}), \mathcal{B}_x(\mathbf{P}), \mathcal{B}_y(\mathbf{P}), \mathcal{B}_z(\mathbf{P})$: 3-by-n matrices that are known at each point in the workspace and can be precomputed or calculated online

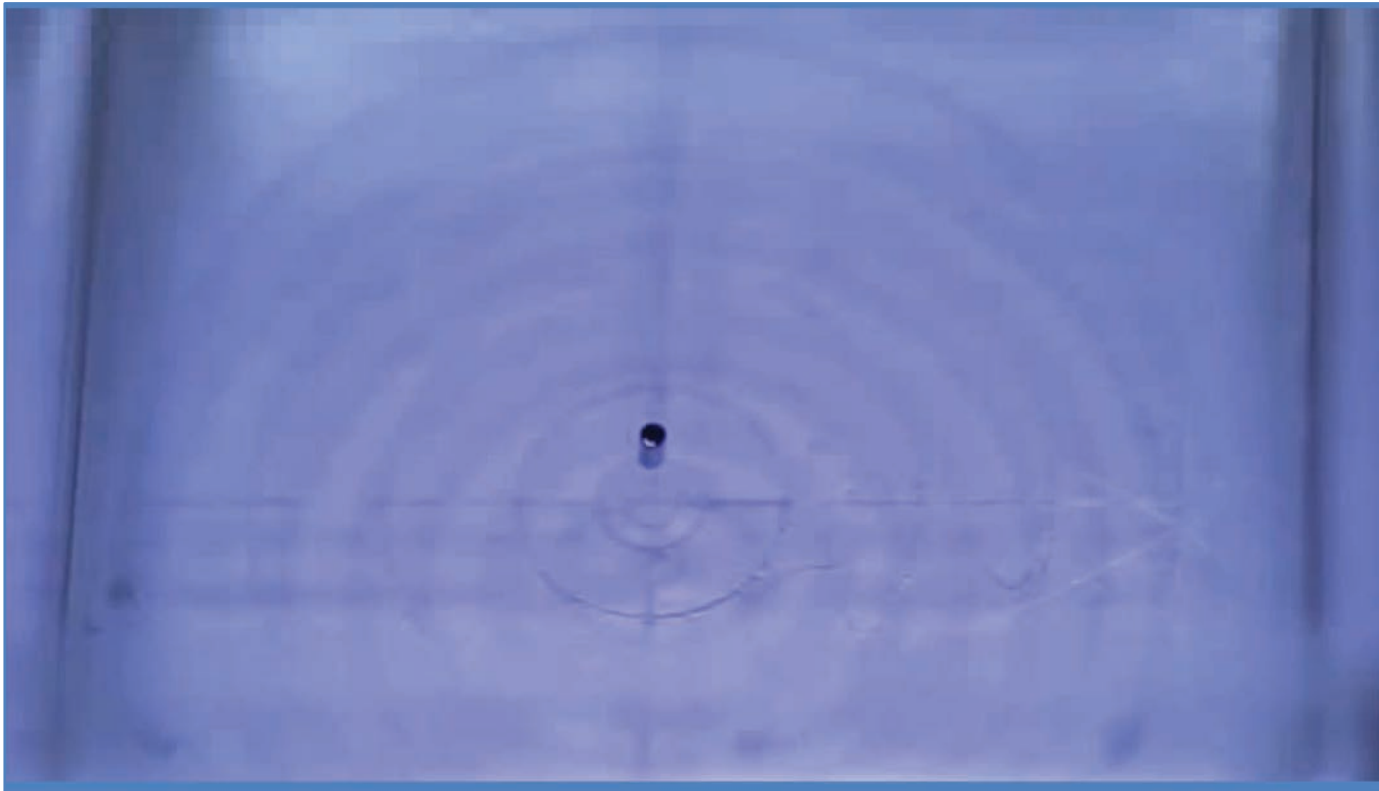
Electromagnetic Control Systems

- 8 electromagnetic coils (minimum required for 6DOF)
- Independent control over orientation and position
- Coil size (and power) vs workspace

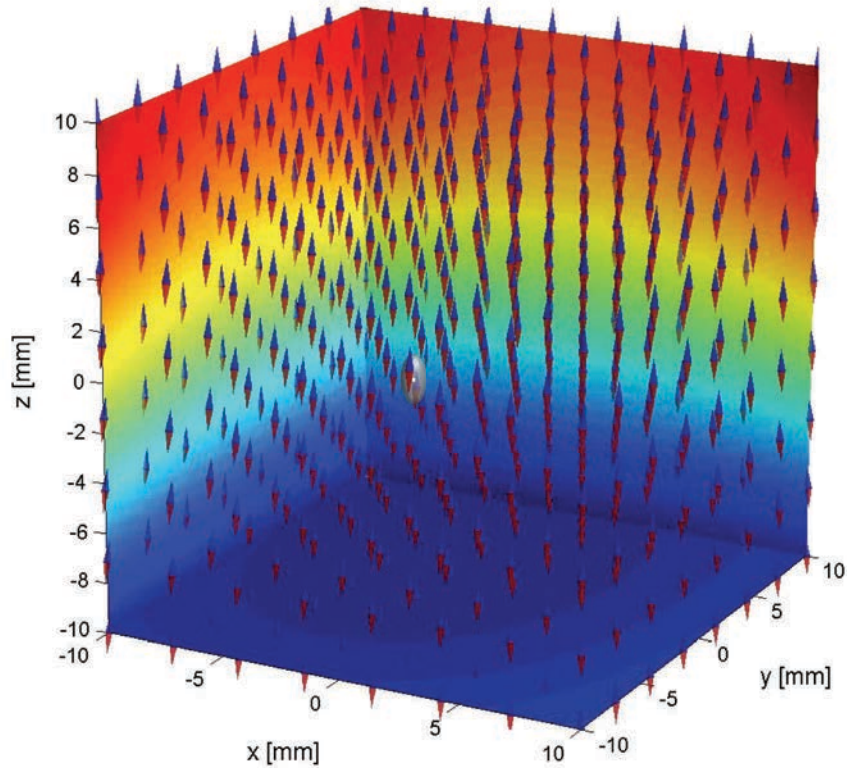


Demonstration of 5-DOF control

- Controlling 6th DOF (roll) is not possible for an object with single magnetization axis



Demonstration of 5-DOF control

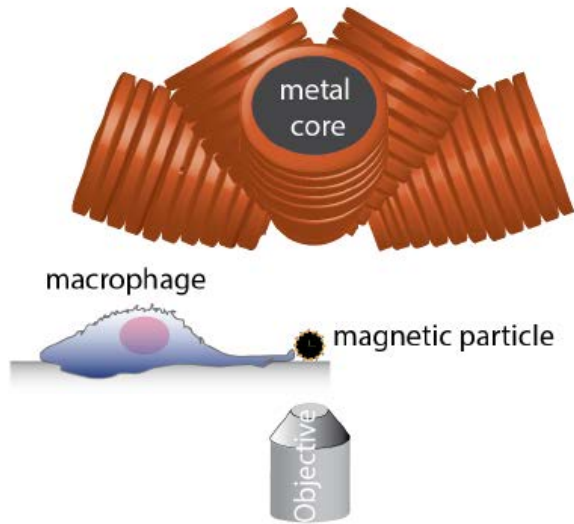


Magnetic Traps

Science Robotics, 2017

a

setup (side view)



bead displacement:
 $F = x * k$

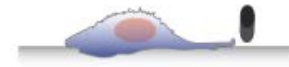


bead out of target threshold (target grey)

bead within target threshold (target green)

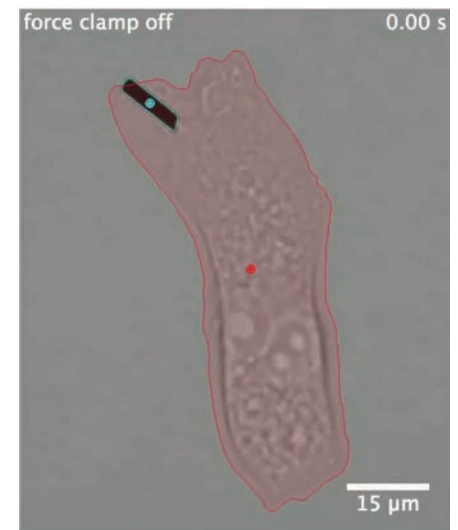
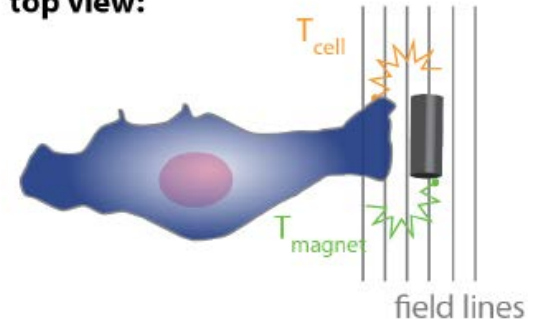


Orientation clamp of non-spherical, rod-shaped foreign bodies



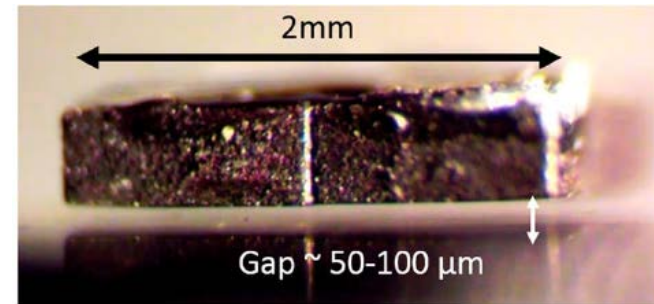
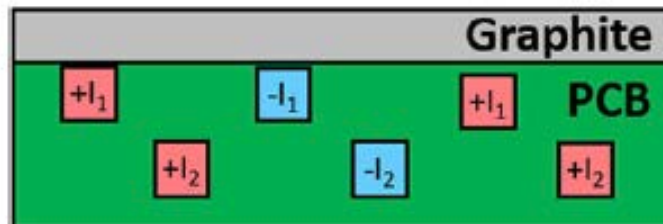
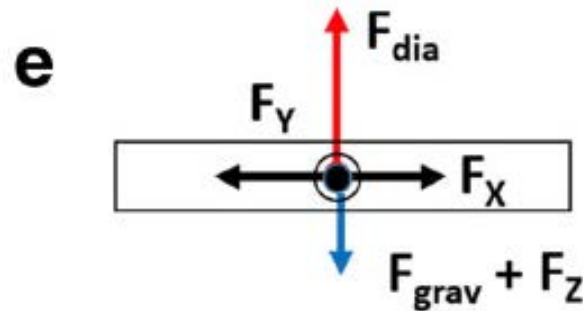
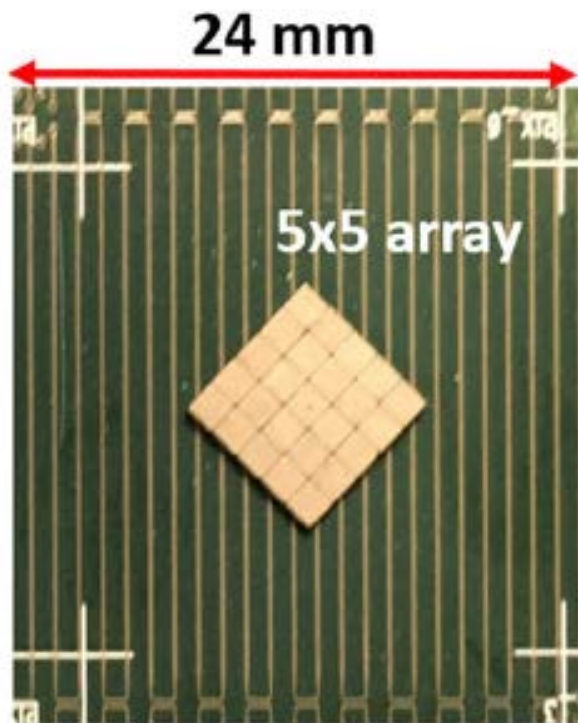
$$T = m \times B$$

top view:



Magnetic Levitation

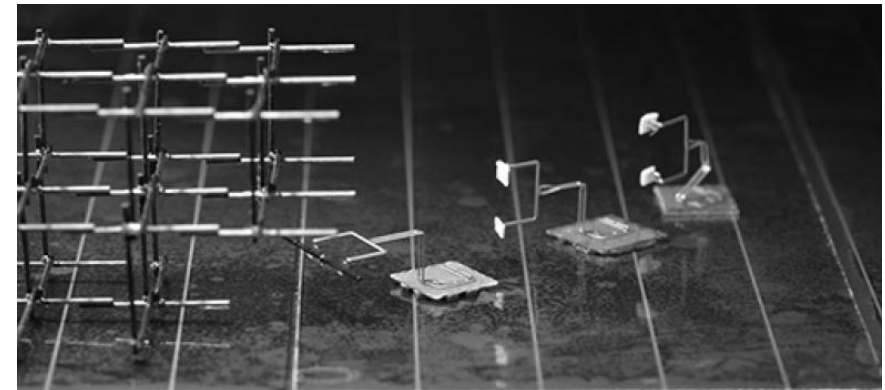
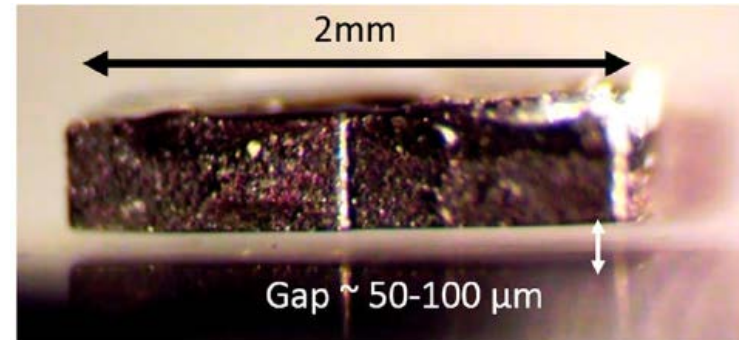
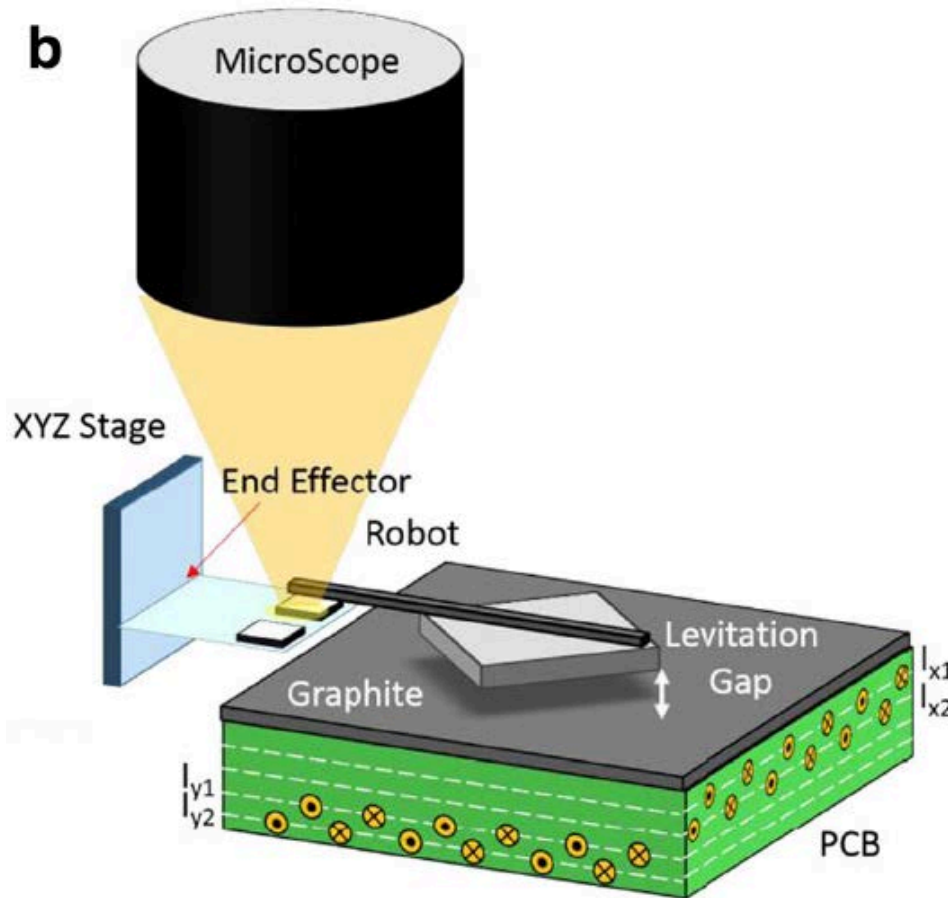
- Assembled arrays of NdFeB magnets (1.4mm) arranged in an alternating north-south configuration
- Serpentine electrical traces pattern within PCB board
- Two sets of traces for controlling x and y position



Magnetic Levitation

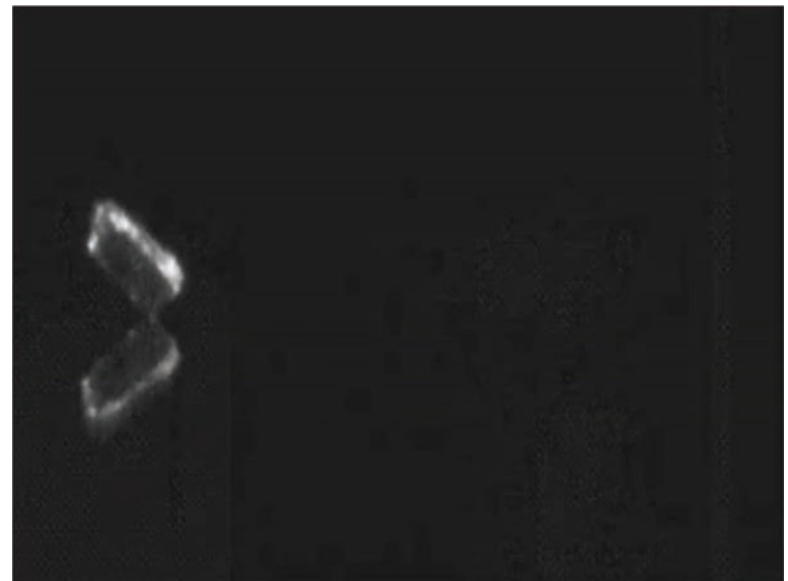
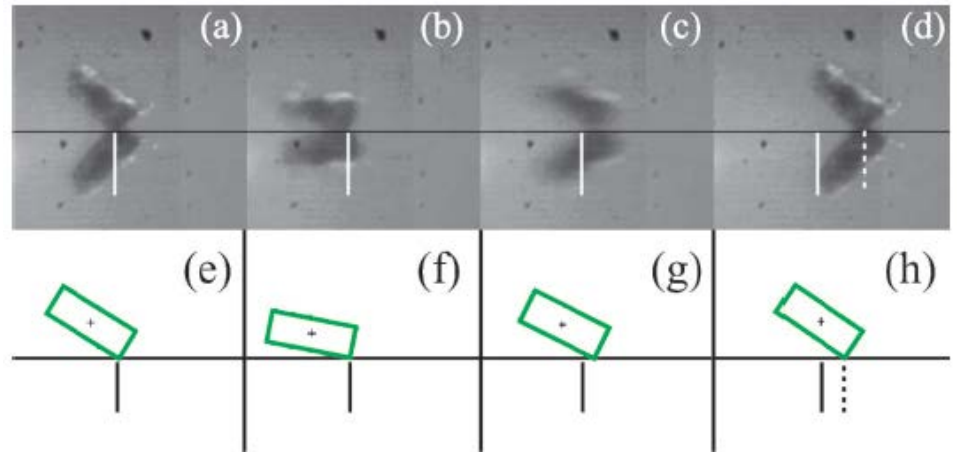
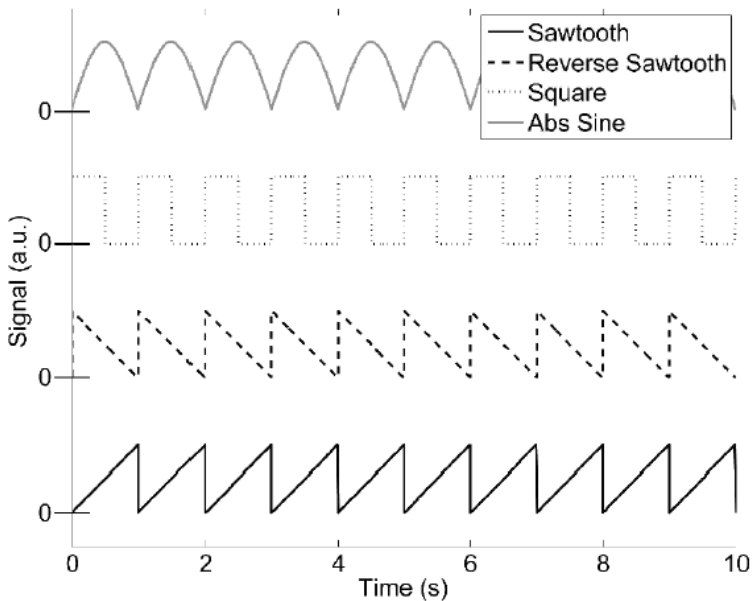
- [SRI Video](#)

- Silicon microtools as end-effectors



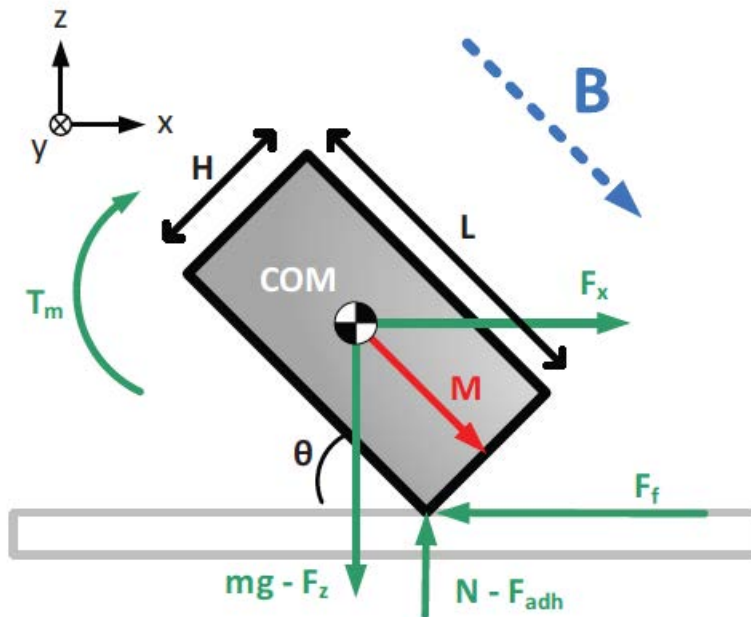
Rocking Motion

In-plane uniform magnetic field
Out-of-plane magnetic torque (pulse)
Asymmetric pulsing waveform
Stick-slip motion



Free Body Diagram

Floyd et al, *IJRR*, 2013



Magnetic Forces (F_x and F_z)
 Magnetic Torque (T_y)
 Damping Force (L_x and L_y)
 Rotational Damping Force (D_y)
 Coulomb Friction Force (F_f)
 Adhesion (F_{adh})

Magnetic Forces are negligible (nN)
 Magnetic Torque dominates motion (μN)

$$m\ddot{x} = F_x - F_f - L_x,$$

$$m\ddot{z} = F_z - mg + N - F_{adh} - L_z,$$

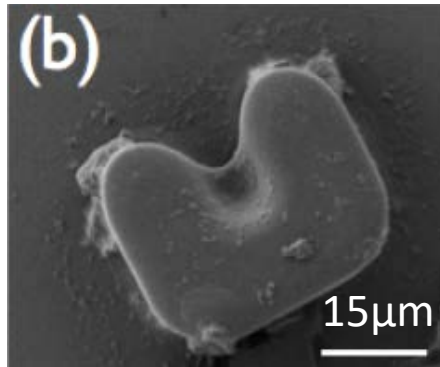
$$J\ddot{\theta} = T_y + F_f \cdot r \cdot \sin(\theta + \phi) - (N - F_{adh})r \cdot \cos(\theta + \phi) - D_y,$$

$$J = m(H^2 + L^2)/12.$$

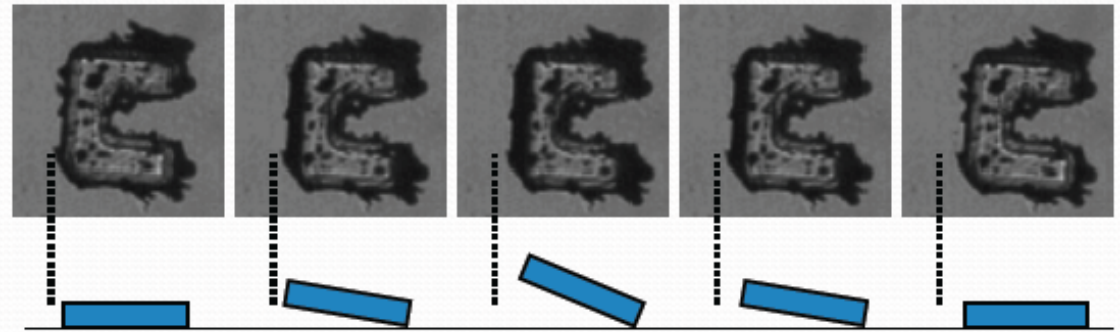
Gravitational Rest Torque (ρ : density)

$$T_g = \rho_{\text{eff}} V_m g \frac{L}{2} \quad \rho_{\text{eff}} = \rho - \rho_{\text{fluid}}$$

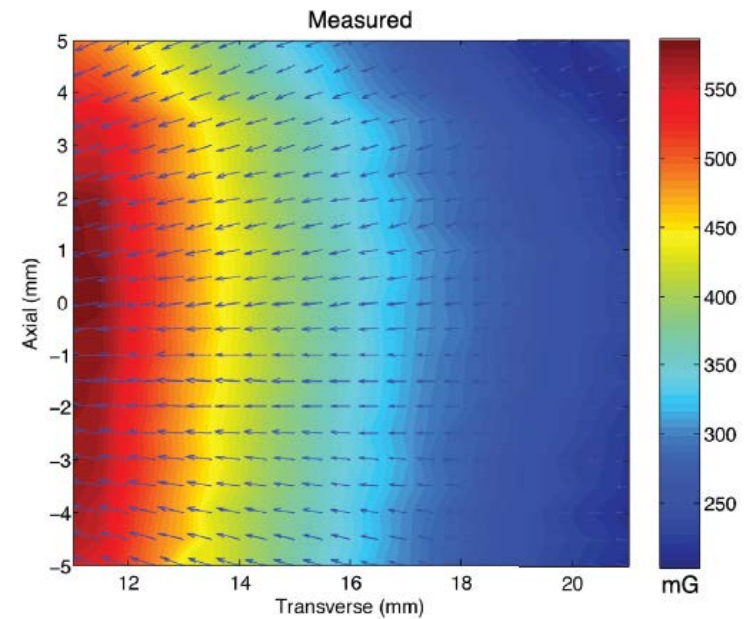
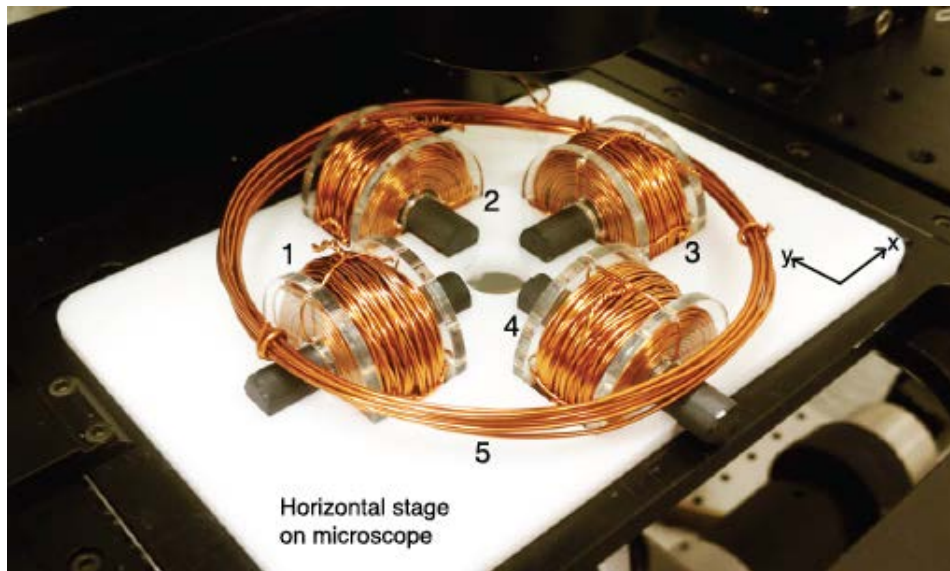
Microtransporters



In-plane magnetic force and out-of-plane magnetic torque (clamping coil)

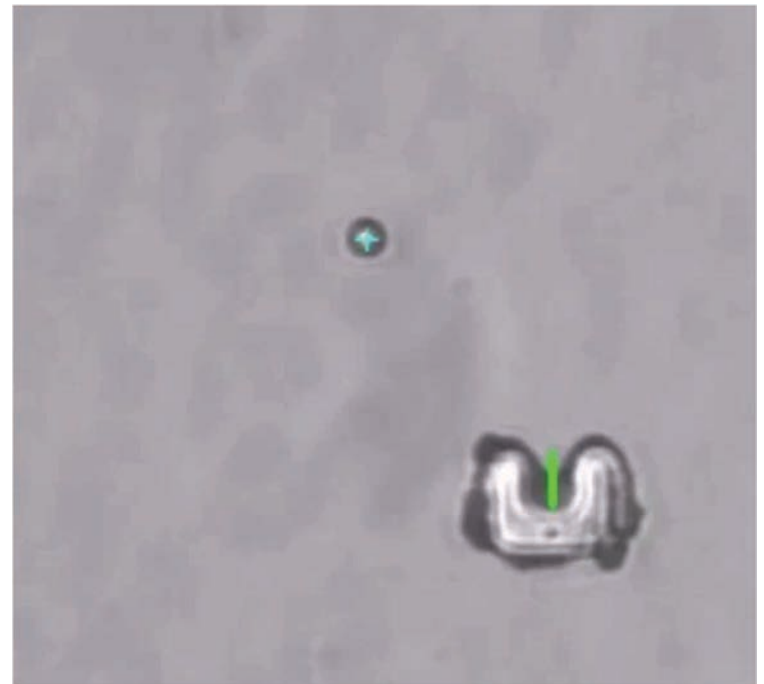
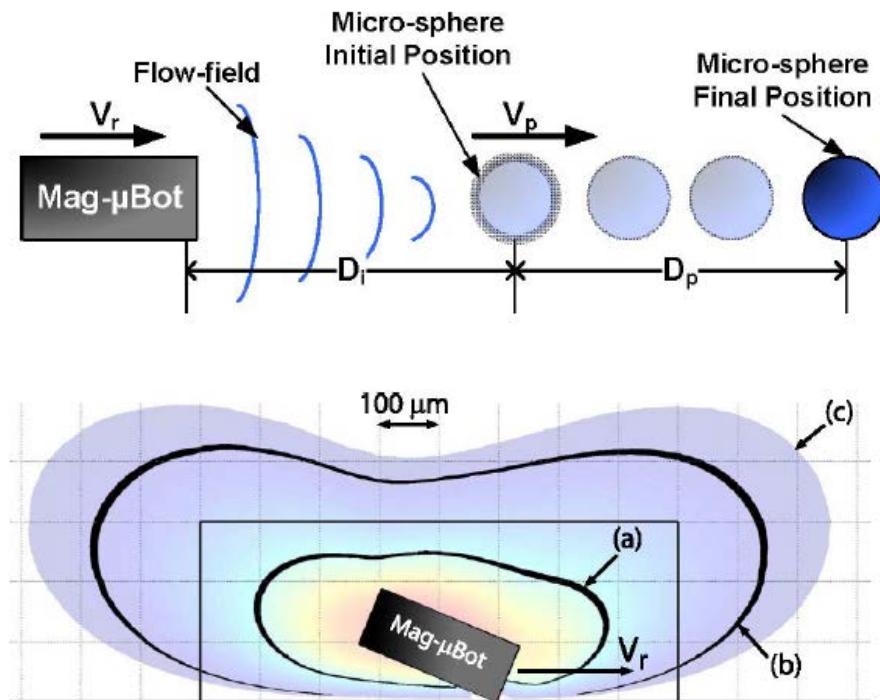


Magnetic Field Gradient (single coil)



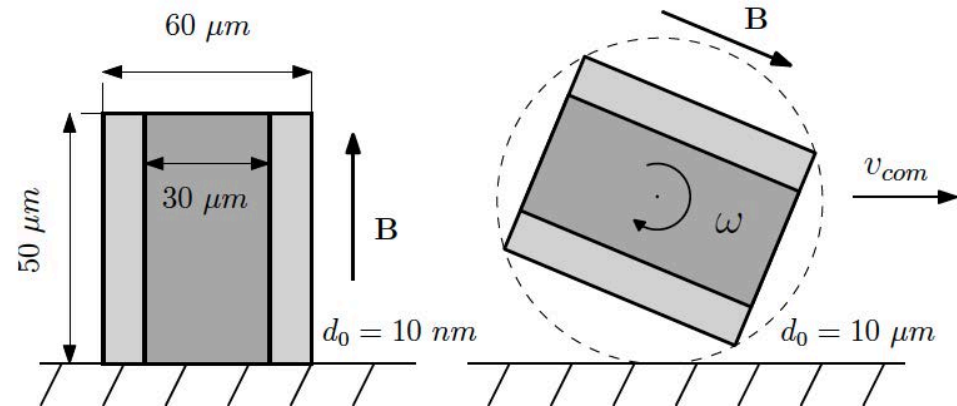
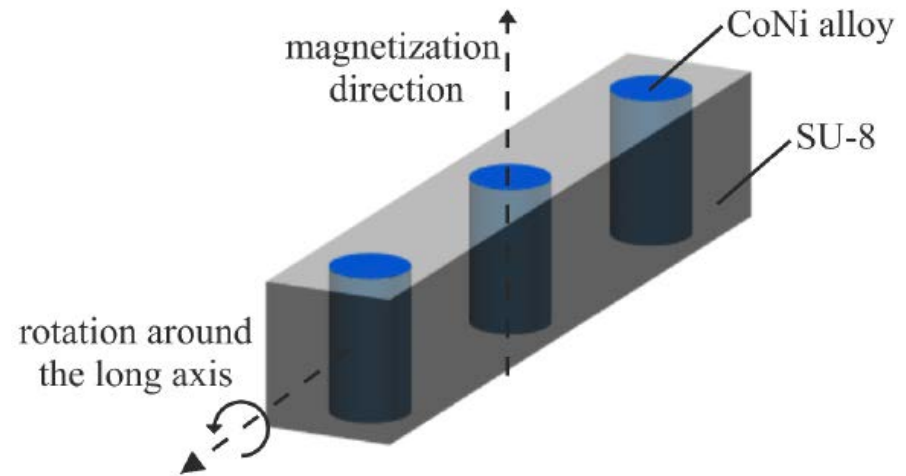
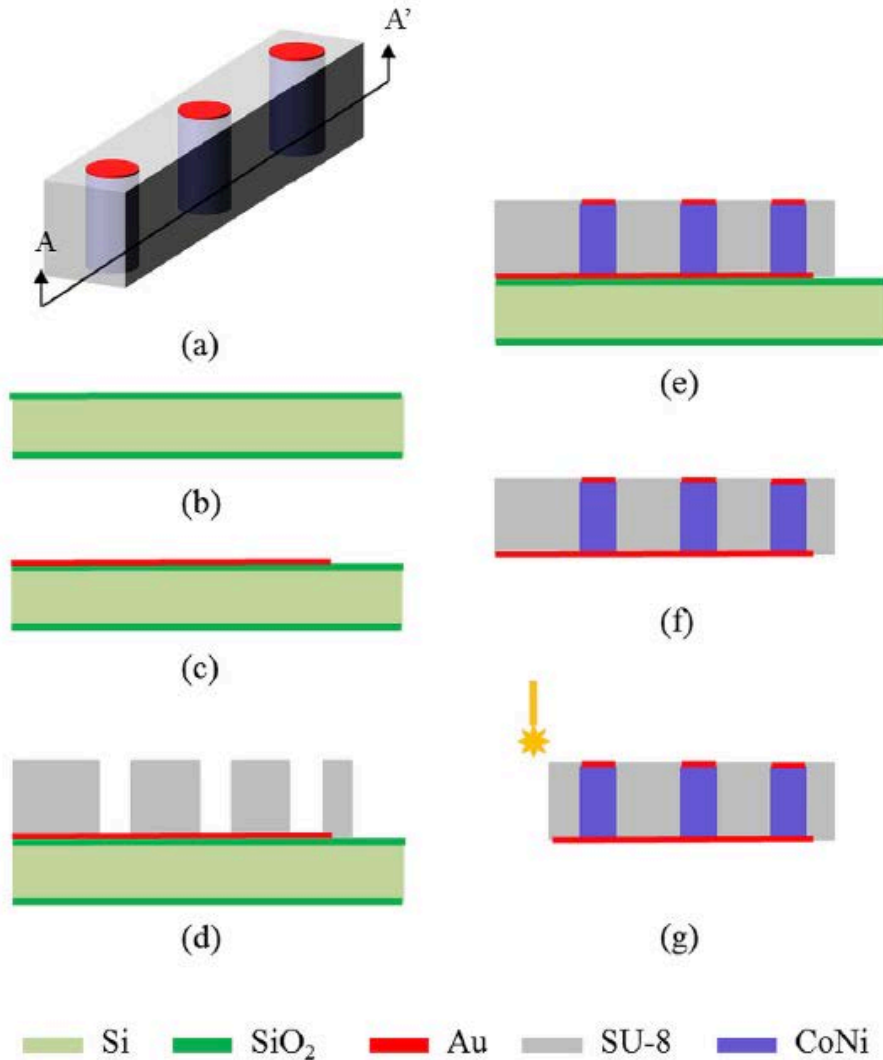
Microtransporter (non-contact mode)

- Compartmentalization (robot and payload)
- Fluidic coupling

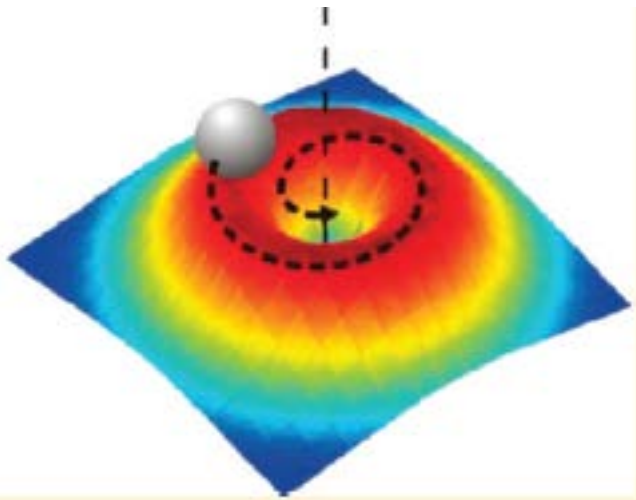


Rolling Robot

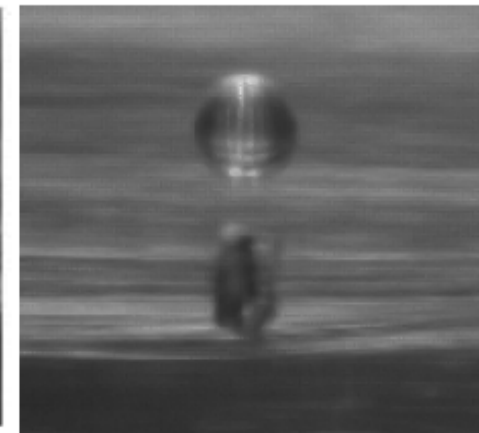
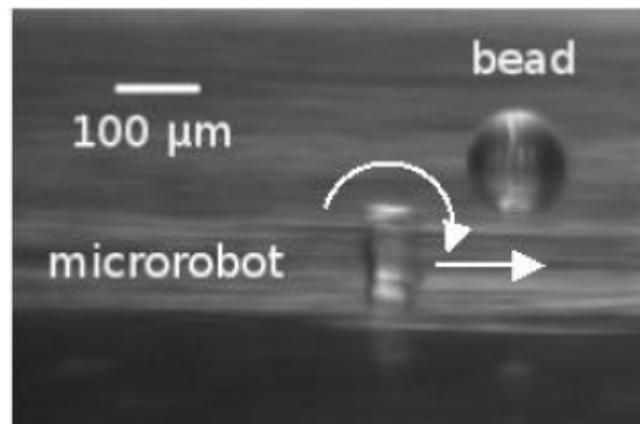
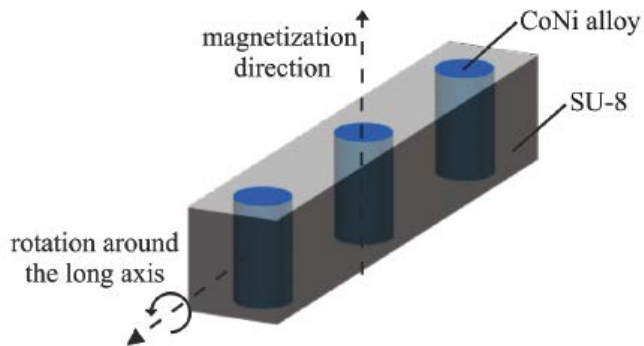
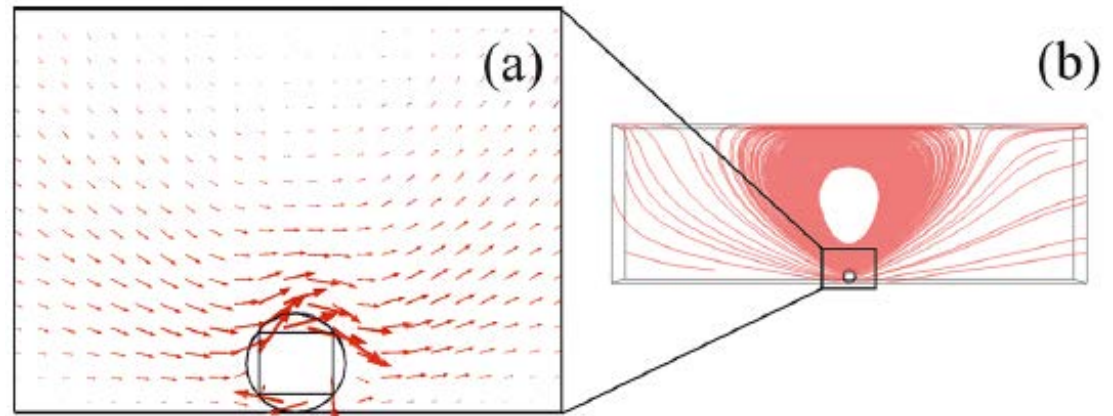
- Video



Generating Mobile Microvortices

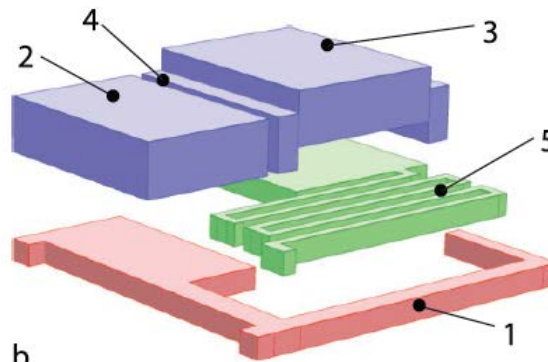
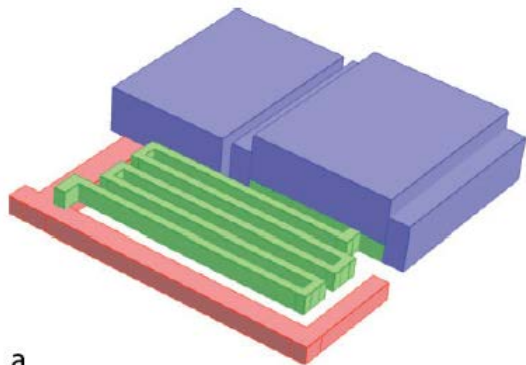
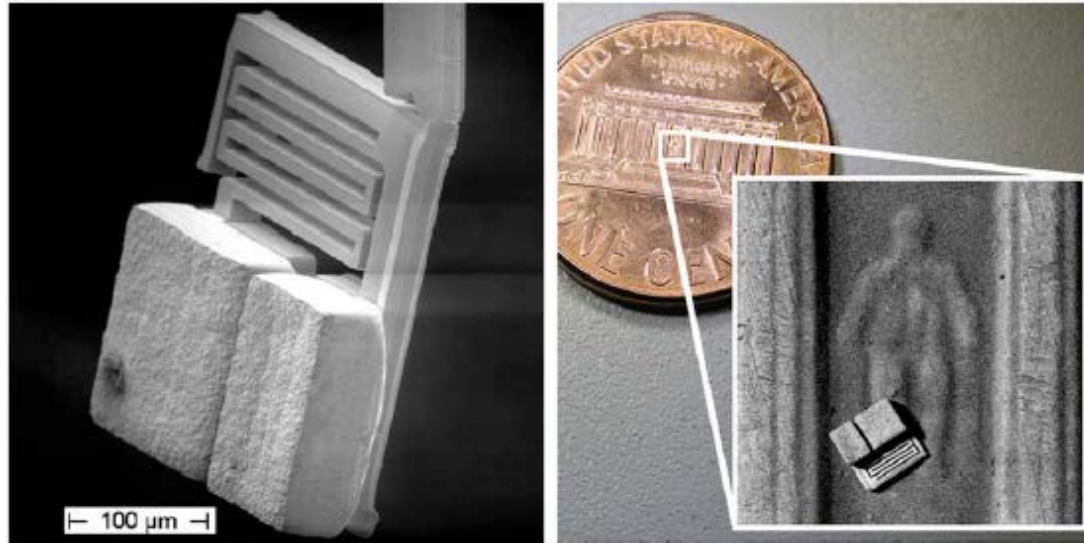


$$\nabla p = \eta \nabla^2 U + f,$$



Tung et al, APL, 2013

Resonant Actuators



1. Gold Base Frame
2. Nickel Attractor
3. Nickel Swinging Mass (hammer)
4. 10-20 μm gap
5. Gold Spring (6 μm above ground)

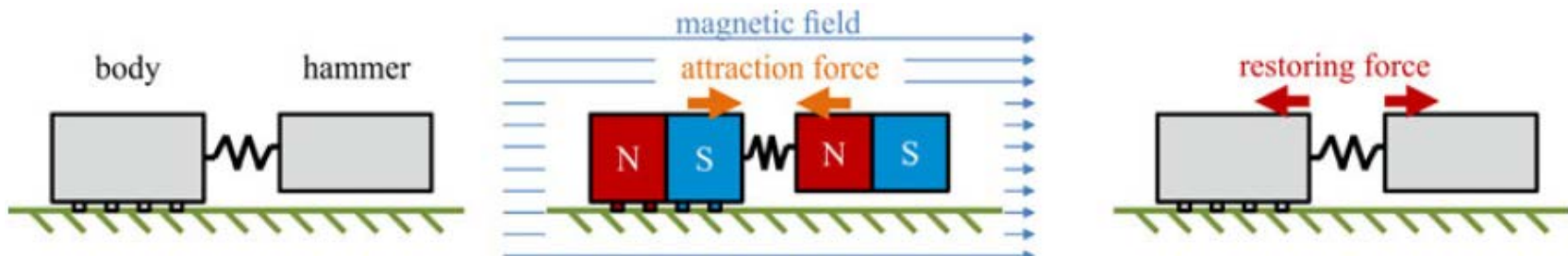
Vollmers et al, *APL*, 2008

Magnetic Impact Drive

- [video](#)

- Power transmitted by oscillating magnetic field
 - Soft magnetic bodies in close proximity create interaction forces in the gap between them
 - Forces narrow the gap and deflect a spring separating the bodies
- Resonant Actuator: Absorb large amount of energy from the driving signal when the signal matches a natural resonant frequency

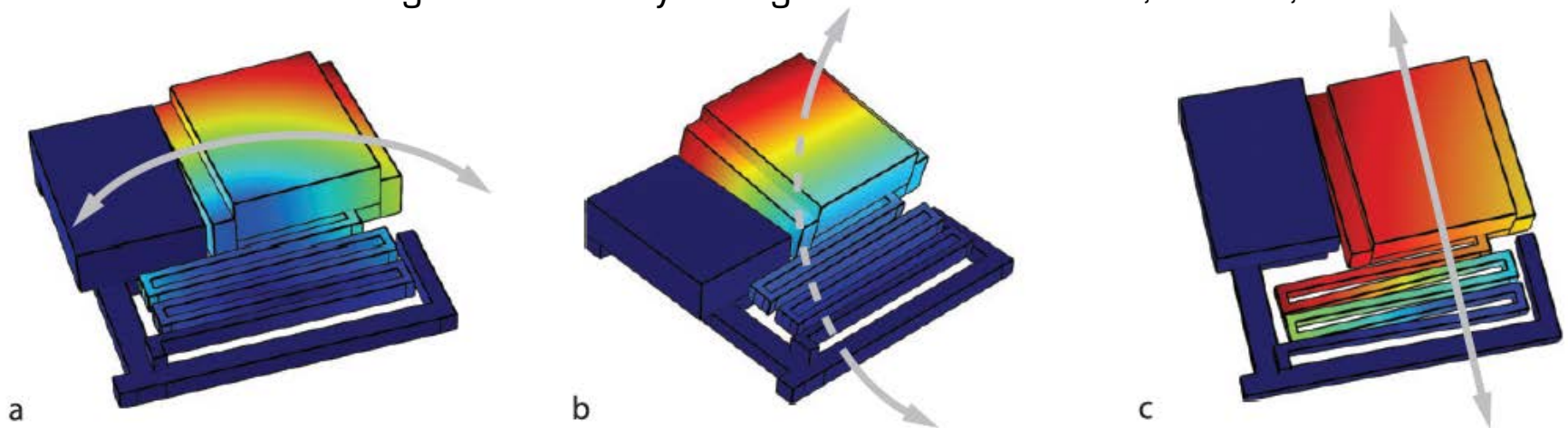
Magneto-mechanical spring-mass system



Mode of Action

- If the device is perfectly symmetrical in its oscillatory motion and actuated on a frictionless surface, it would vibrate in place
- To generate motion in a particular direction, hammer is located above the substrate and friction is controlled through an electrostatic clamp
- Electrically conducting gold base frame (clamping force)
- Dimples minimize friction (good sliding behavior)

Structural FEM eigenmode analysis. Eigenmodes at 1.5kHz, 1.7kHz, and 3.9kHz



Physics of Swimming

- Moving through a fluid is affected by two fundamental phenomena
 - **Inertial effects:** Moving (i.e. accelerating) the fluid away from where we want to be
 - **Viscous effects:** Overcoming the friction between the fluid layers that are moving with us and those that are not



Navier-Stokes Equation

- The Navier-Stokes equations is a formulation of Newton's second law applied to a fluid to describe its motion
 - For an incompressible Newtonian fluid:

unsteady
acceleration

Viscosity
term

$$\rho \left(\frac{\partial \mathbf{V}}{\partial t} + \mathbf{V} \cdot \nabla \mathbf{V} \right) = -\nabla p + \mu \nabla^2 \mathbf{V}$$

Convective
acceleration

Pressure
gradient

Reynolds Number

- The Reynolds (Re) number is a dimensionless number that describes the relative importance of inertial and viscous effects:

$$\left(\frac{\rho U \delta}{\mu}\right) \frac{d\tilde{\mathbf{V}}}{dt} = -\nabla \tilde{p} + \nabla^2 \tilde{\mathbf{V}}$$

$$Re = \frac{\rho U \delta}{\mu}$$

where ρ is fluid density [kg/m³]
 U is characteristic speed [m/s]
 δ is characteristic length [m]
 μ is fluid viscosity [Ns/m²]

- Re \ll 1: Viscous forces dominate Inertial Forces
- Navier-Stokes becomes time-independent (Stokes Flow)

$$\nabla p = \mu \nabla^2 V$$

Intermediate Reynolds Number

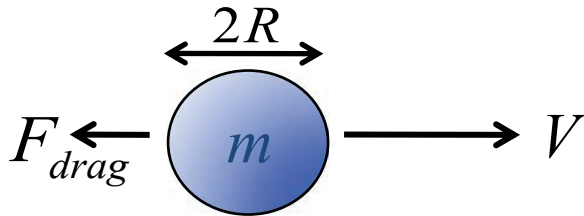
- $1 < Re < 1000$
- Both viscous and inertial effects play an important role.
- Examples:
 - Insect flight
 - Micro aerial vehicles (MAV)



Drosophila melanogaster

Stokes Flow

- Describes the drag force on a sphere in Stokes flow

$$F_{drag} = 6\pi\mu RV$$


The diagram shows a blue sphere of radius R moving to the right with velocity V . A drag force F_{drag} acts to the left. The diameter of the sphere is labeled $2R$.

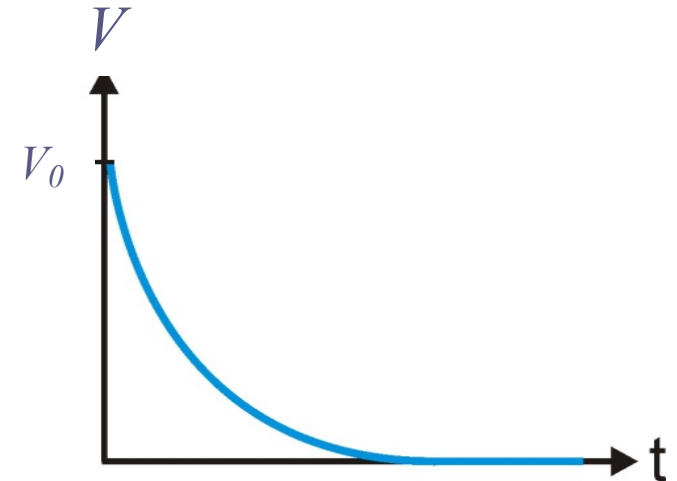
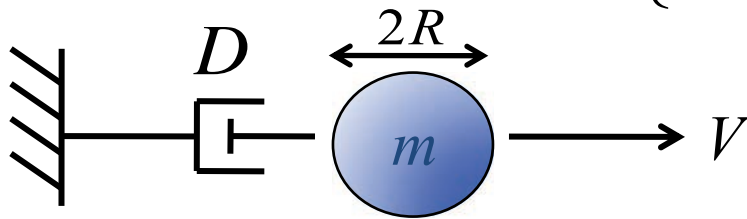
- The force is linearly proportional to the radius of the object
- Microsphere ($R = 1 \mu\text{m}$, $\rho = 10^4 \text{ kg/m}^3$) being pulled through water ($\mu = 10^{-3} \text{ Pa}\cdot\text{s}$, $\rho = 10^3 \text{ kg/m}^3$) at a speed of $V = 10 \mu\text{m/s}$

$$F_{pull} = F_{drag} = DV \approx 20 \text{ pN}$$

Stokes Flow

- Velocity of the sphere
 - Behaves like a critically damped system

$$V(t) = V_0 \exp\left\{-\frac{D}{m}t\right\}$$



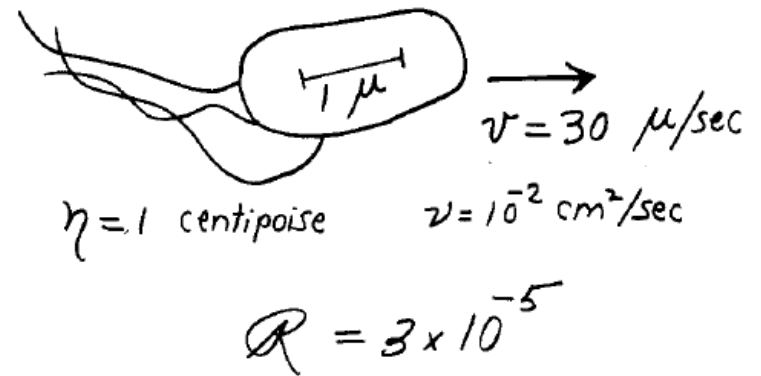
- Coasting distance and time

$$d_{coast} = \int_0^{\infty} V(t) dt = V_0 \frac{m}{D} \approx 2 \cdot 10^{-11} m \quad t_{coast} \approx 2 \mu s$$

- Coasting distance is only $d_{coast} = 10^{-5}$ of the sphere's radius!
- Steady state is reached almost immediately

Swimming at low Reynolds Number

- Bacteria swim at $Re \approx 10^{-4}$ in water
- What the bacterium is doing at the moment is entirely determined by the forces that are exerted on it at that moment and by nothing in the past
- Reciprocal Motion
 - Time makes no difference
 - If I change quickly or slowly, forward or backwards, the pattern of motion is exactly the same



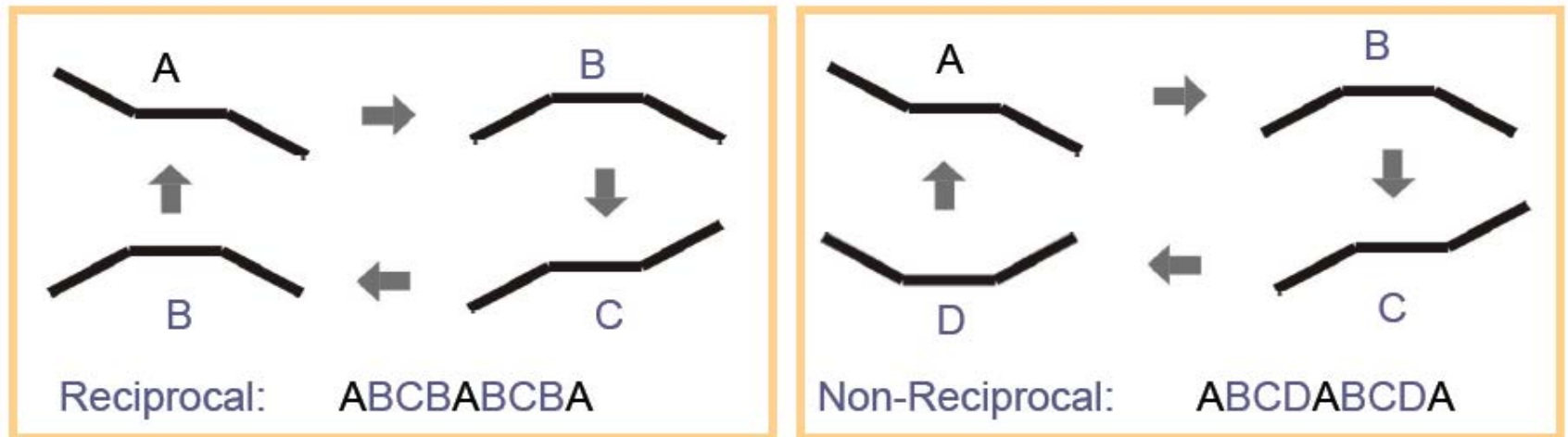
$$\left. \begin{array}{l} \text{coasting distance} = 0.1 \text{ \AA} \\ \text{coasting time} = 0.3 \text{ microsec.} \end{array} \right\}$$

The Scallop Theorem



Swimming at low Reynolds Number

- A micro-swimmer must generate non-reciprocal motion in order to produce a net displacement (in Newtonian fluids)
- More than one degree of freedom is necessary to create non-reciprocal motion
- Example: a swimmer with two hinges
 - Depends on set of configurations



Swimming at low Reynolds Number

- Reciprocal motion
 - No net displacement after one cycle
 - Rigid oar moving left and then right

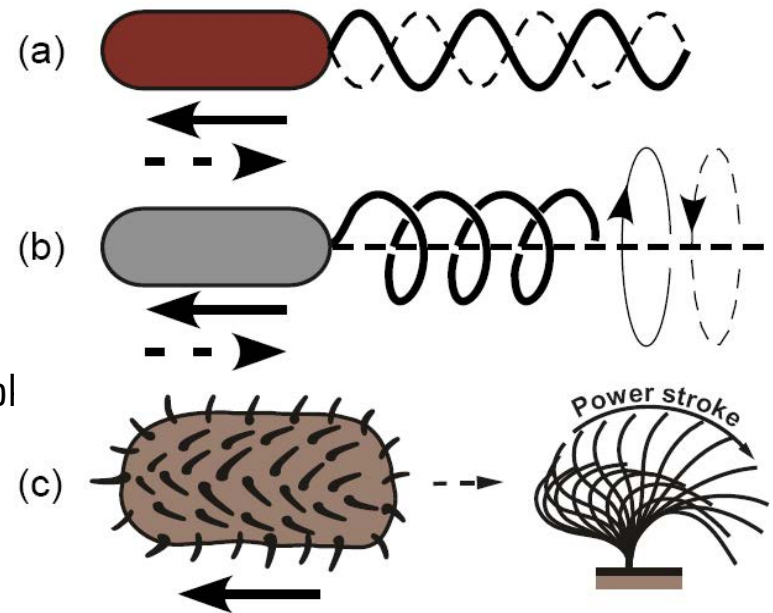


- Non-reciprocal motion
 - Net displacement after one cycle
 - One rotation around helical axis



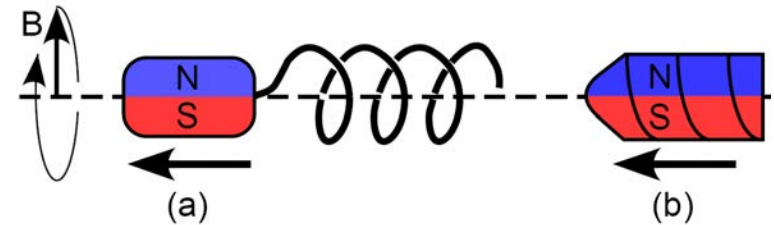
Bioinspired Swimming

- Eukaryotic flagella (a)
 - Active organelles which create traveling waves
 - Swimming direction can be reversed by reversing the direction of the wave
 - Head-to-tail
 - Tail-to-head
- Bacteria flagella (b)
 - Molecular motors turn the flagella
- Cilia (c)
 - Active organelles
 - Held perpendicular during the power stroke
 - Parallel during recovery stroke

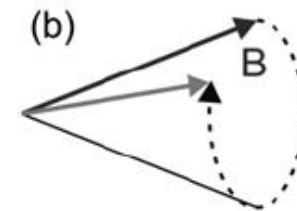
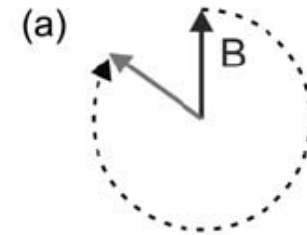


Bioinspired Swimming

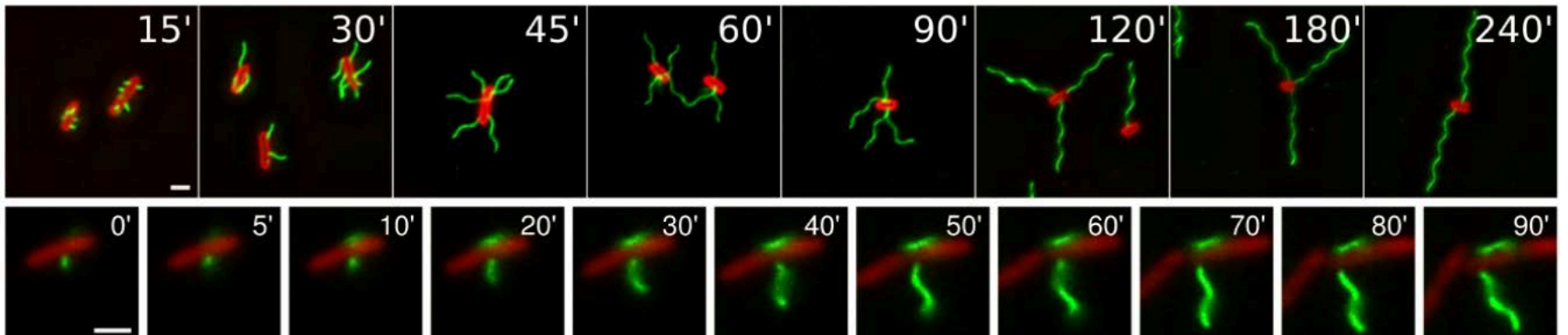
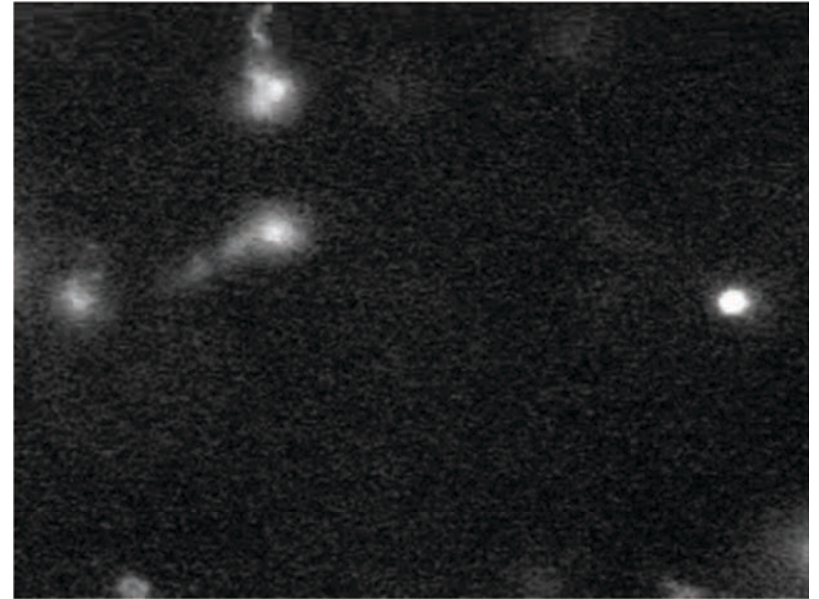
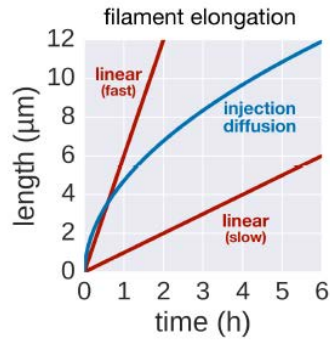
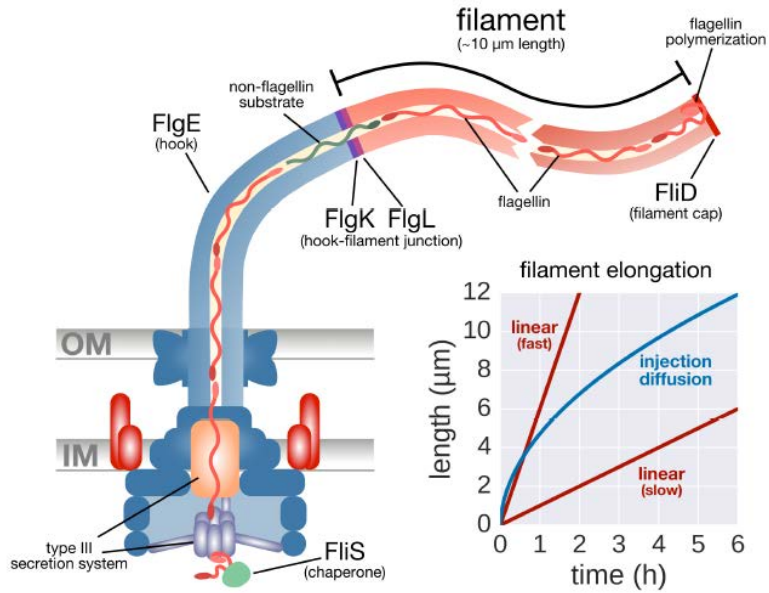
- Another plausible solution is trying to recreate helical swimming, with rotating magnetic fields
- Helical propeller
 - A helical tail can be attached to the “head” of the microrobot
 - The interaction between the magnet and the field causes the magnet to rotate
 - Swimming velocity is linearly related to the field frequency, up until a step-out frequency
 - Velocity decreases dramatically



Rotating fields

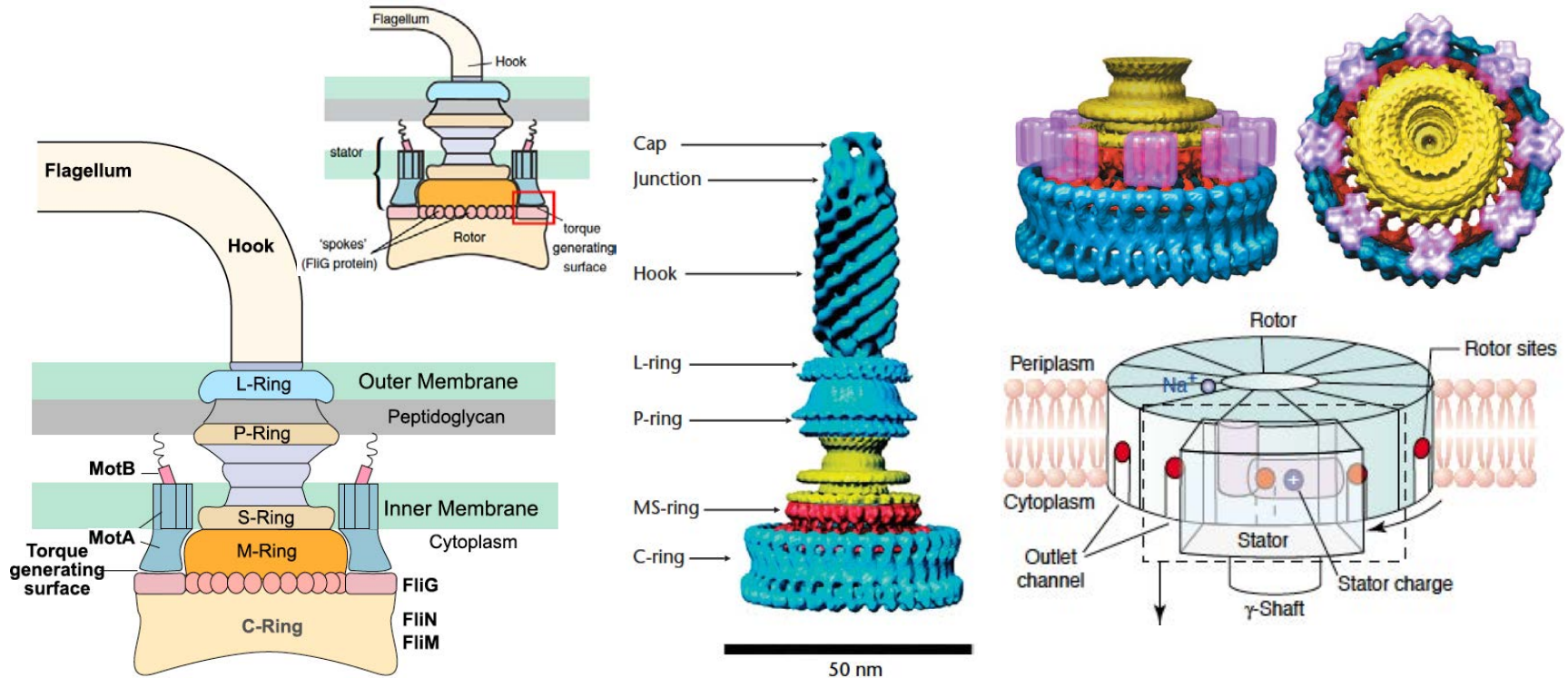


Bacterial Flagella



Flagellar Motor

Stator complex (Mot A and Mot B) – Rotor ring (C ring) – Axial driveshaft (rod) – Universal joint (hook) – Helical propeller (filament)



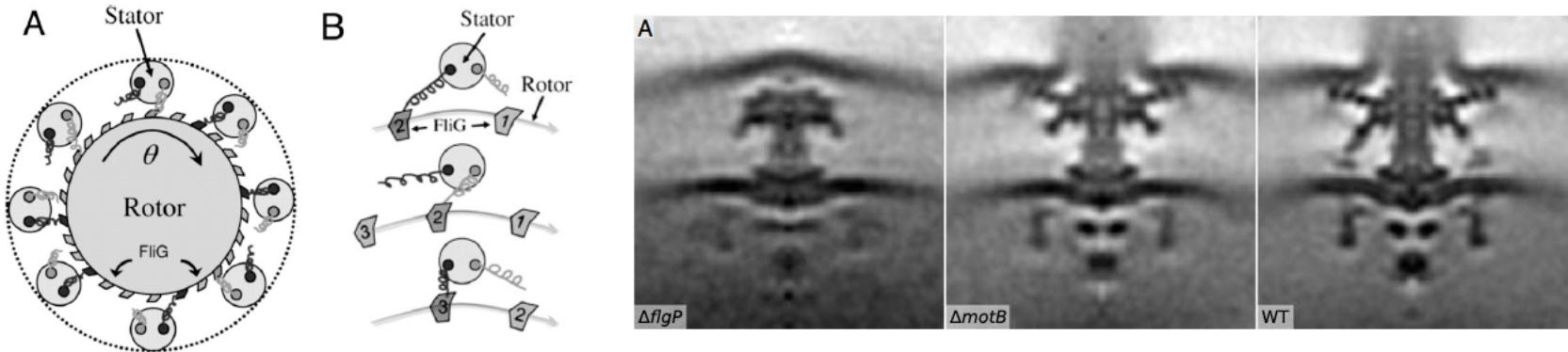
Torque is generated at the interface between transmembrane proteins (stators) and rotor
 Passage of ions down a transmembrane gradient through stator complex provides energy
 Each revolution 1200 protons, each contributing $6k_B T$, 26 steps per revolution, up to 300Hz

Mechanism of Torque Generation

Beeby et al, PNAS, 2016

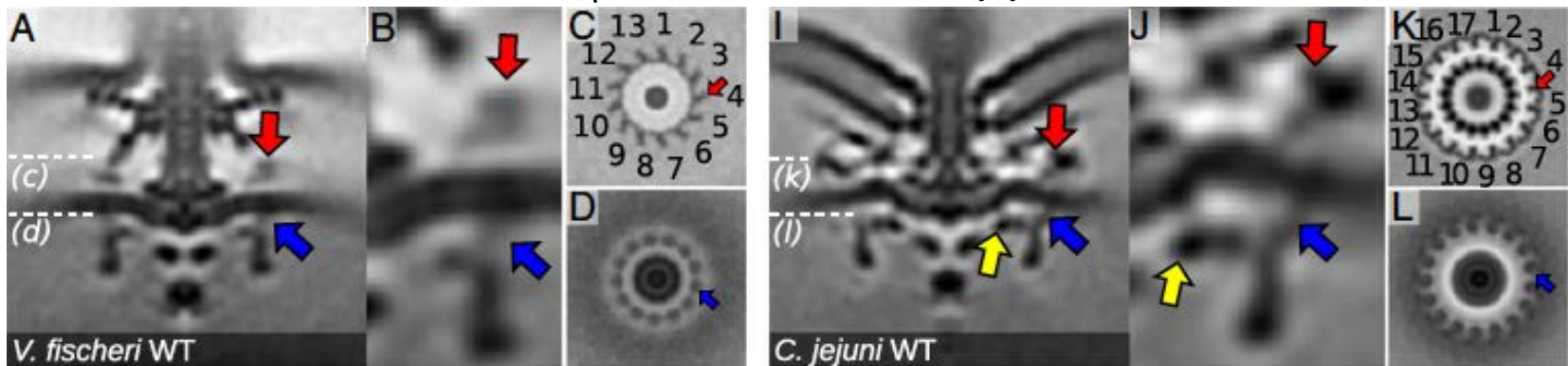
Torques of motors from different bacteria (torque correlates with swimming speed)

C. Crescentus: 350 pN.nm, *E.coli*: 2000 pN.nm, *H. pylori*: 3600 pN.nm,
 spirochetes: 4000 pN.nm

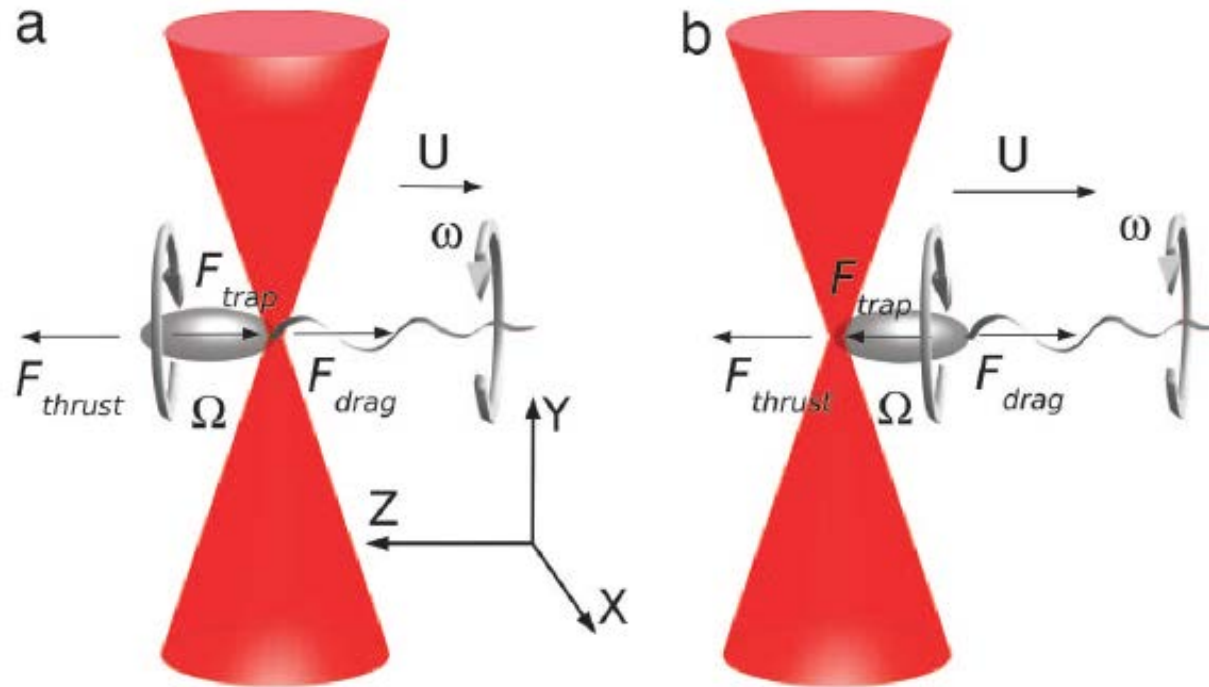


Structural adaptations of flagellar motors

Salmonella: 11 stator complexes, *Vibrio*: 13, *C. jejuni*: 17



Bacterial Flagellum: Optical Traps



Wu et al, *PNAS*, 2006

Swimming at low Reynolds Number

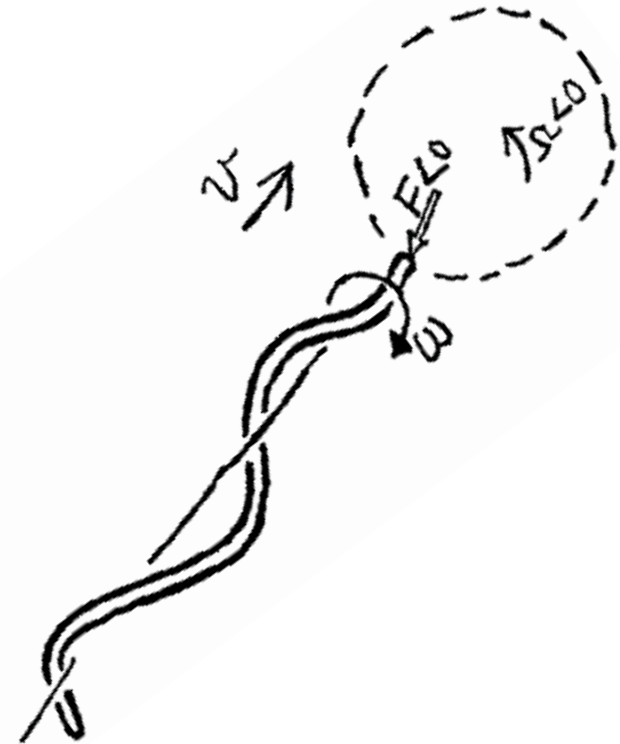
Purcell, *PNAS*, 1997



$$F = Av + B\omega$$

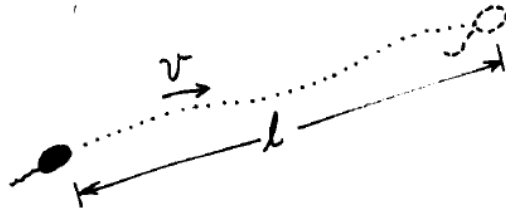
$$N = Cv + D\omega$$

$\begin{pmatrix} A & B \\ C & D \end{pmatrix}$ Propulsion Matrix (Resistance Matrix)



- Thin, perfectly stiff, untwistable axial wire
- The constants of the propulsion matrix are proportional to the fluid viscosity and depend only on the shape and size of the propeller
- The torque and force on the cell must be equal and opposite to the torque and force on the propeller

Navigation



to out-swim diffusion:

$$l \geq D/v \quad l \geq 30 \mu$$



$$S \approx 10^{-2}$$

local stirring accomplishes nothing

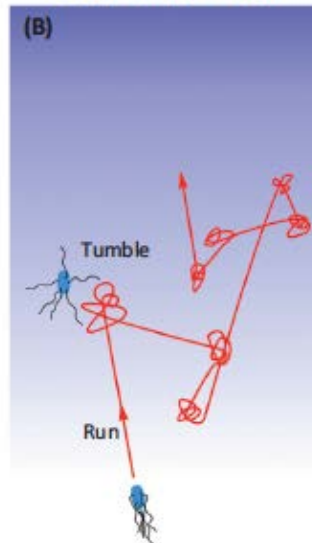
Spatial comparison



Slime mold *Dictyostelium*

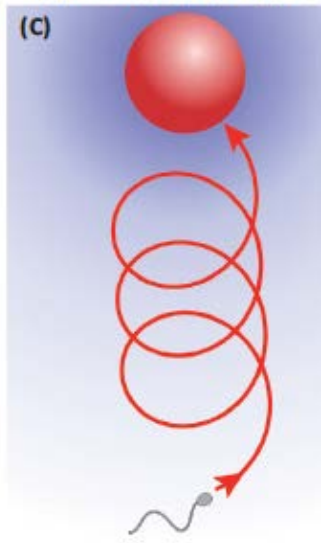
Temporal comparison

Biased random walk



Bacterium *E. coli*

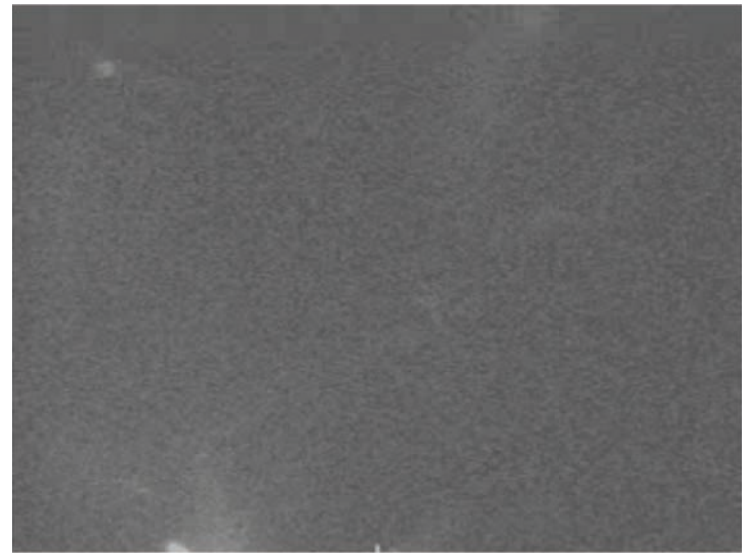
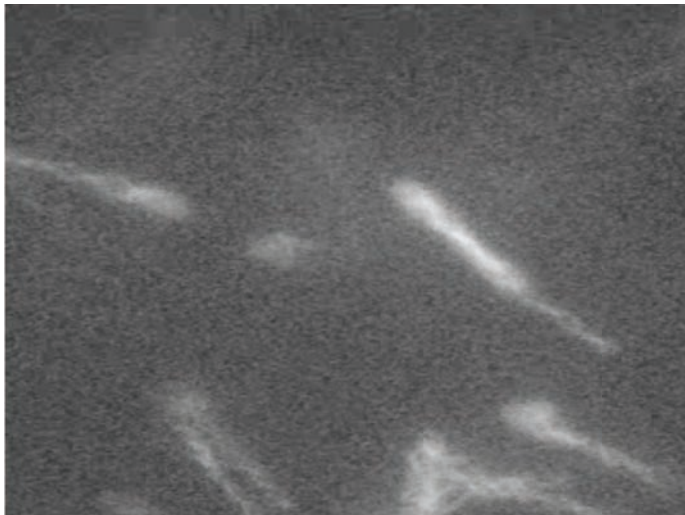
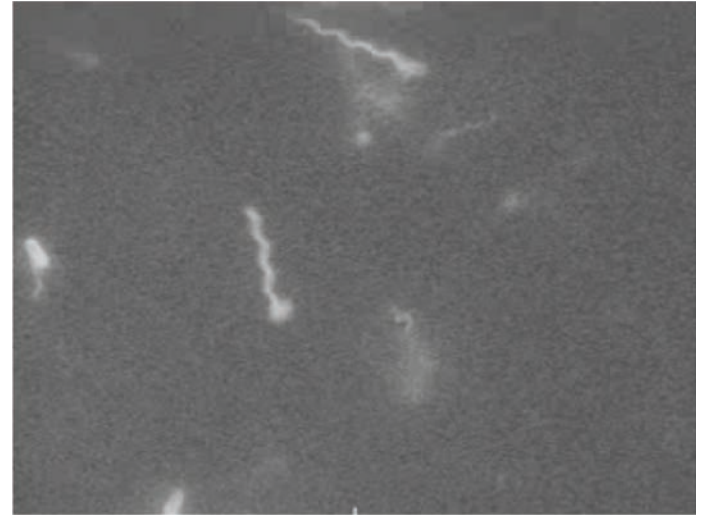
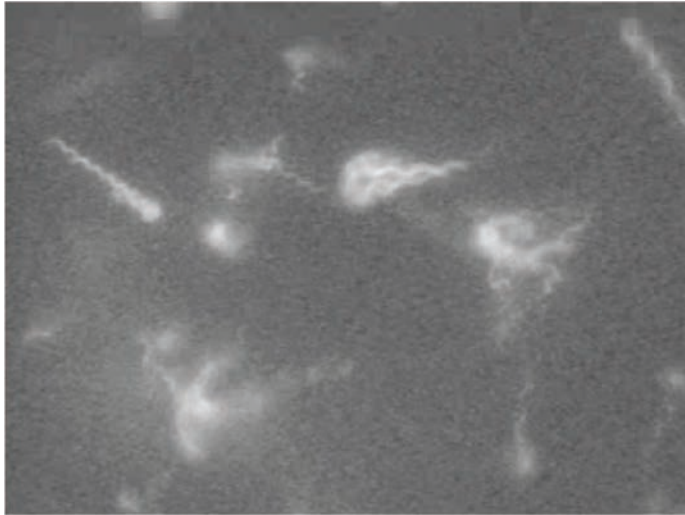
Deterministic chemotaxis



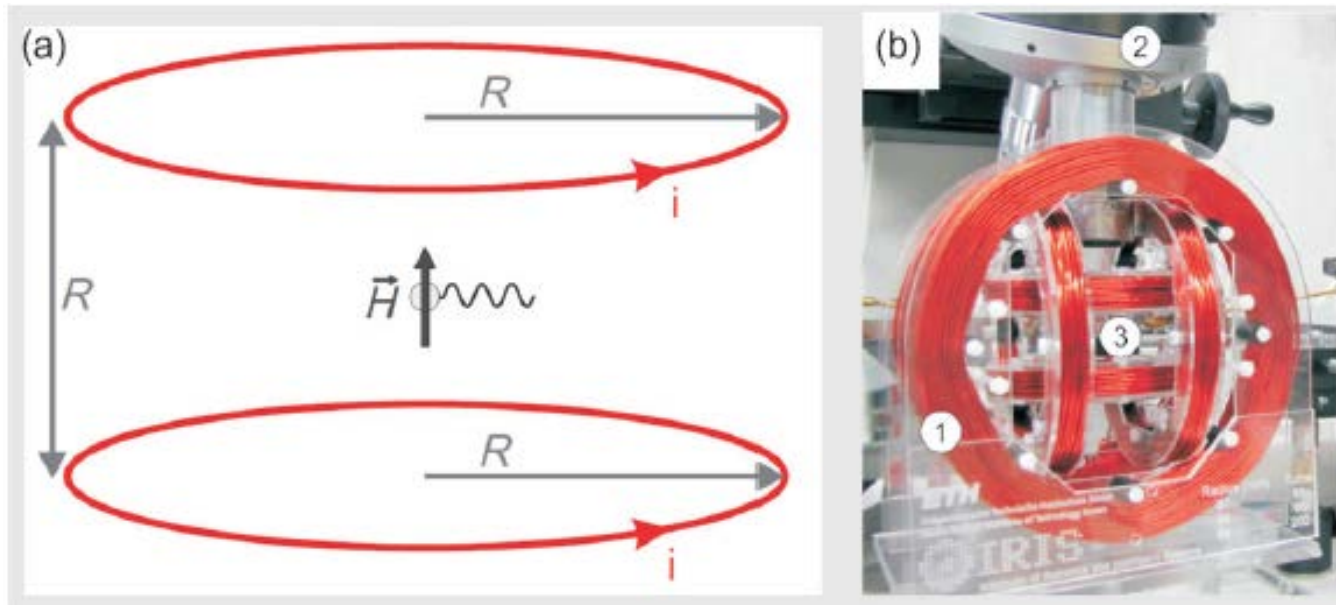
Sea urchin sperm

1977

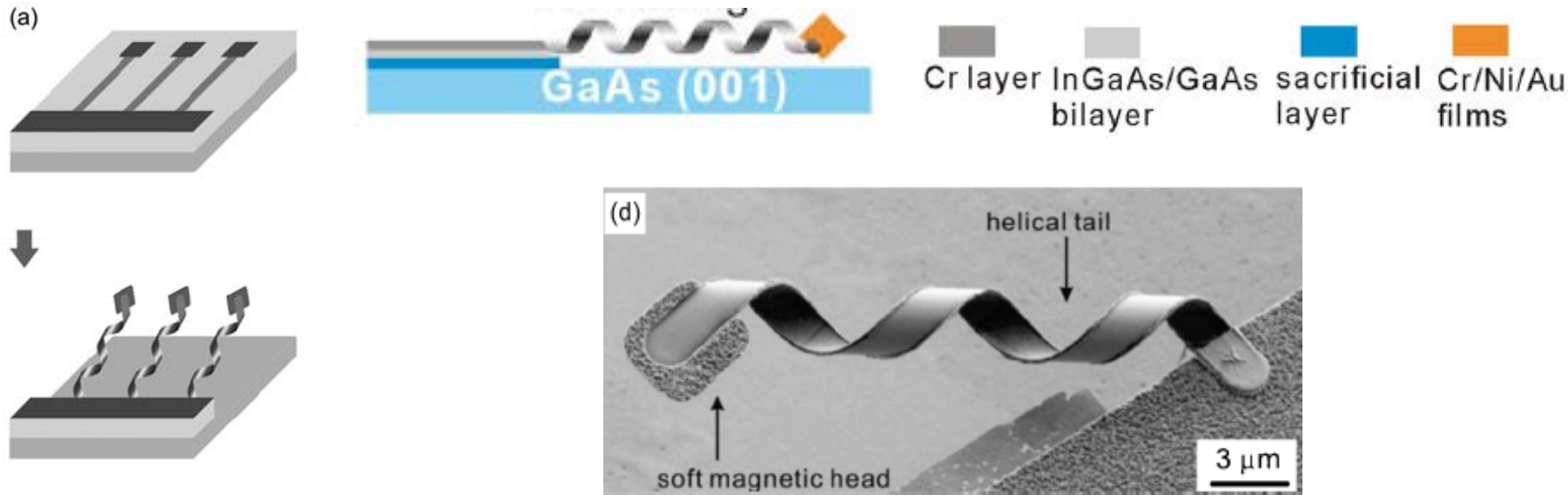
Navigation



Corkscrew Motion with Artificial Microswimmers



Self-scrolling



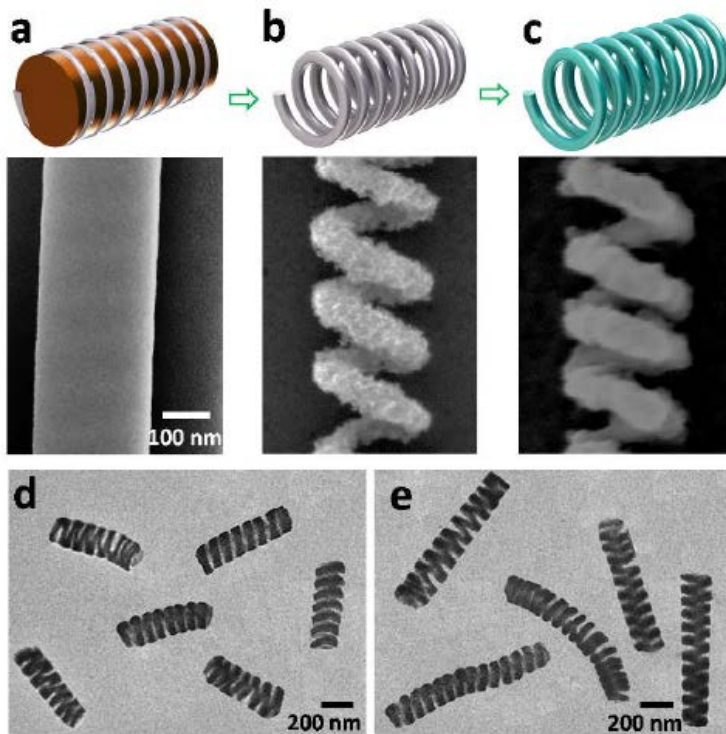
$$R = \frac{(h_1 + h_2) \left(8(1+m)^2 + (1+mn) \left(m^2 + \frac{1}{mn} \right) \right)}{6\varepsilon(1+m)^2}$$

$$n = E_1/E_2$$

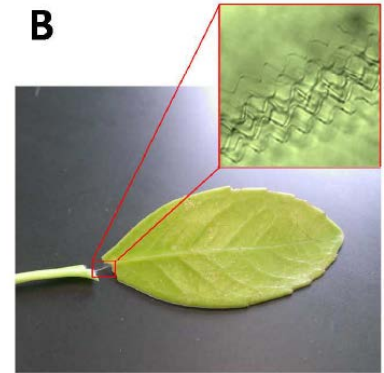
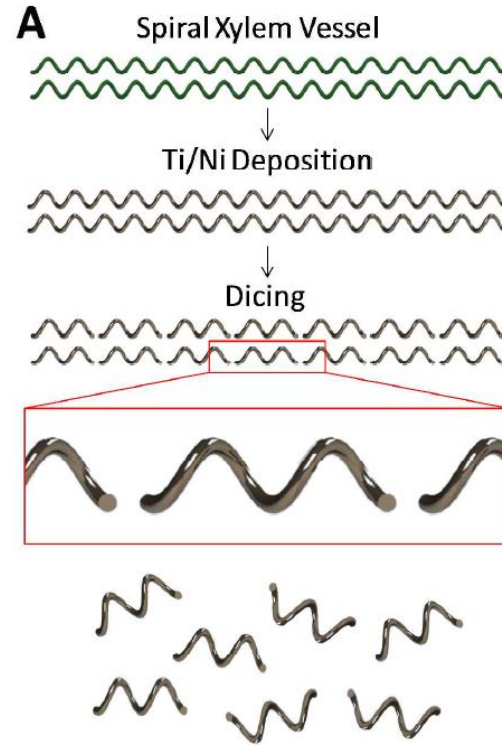
$$m = h_1/h_2$$

Zhang et al, *APL*, 2009

Growing on Seed Material

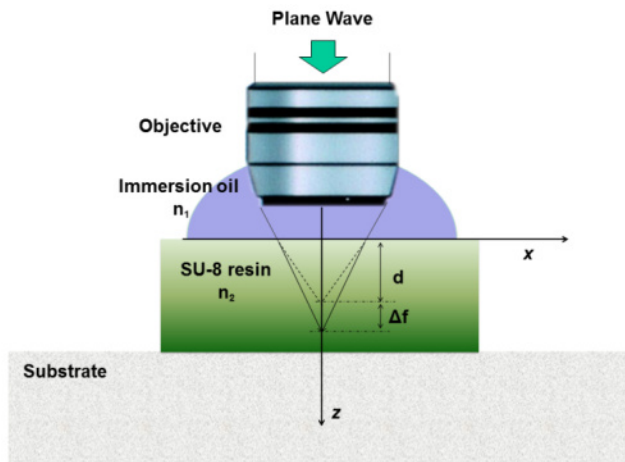
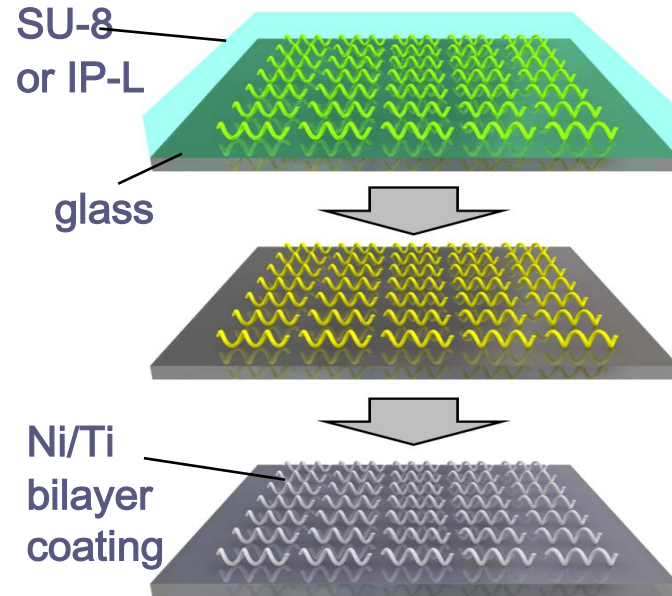
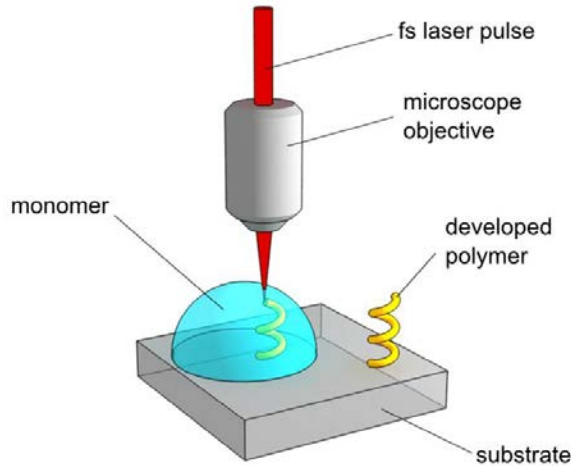


Pd/Cu rods
Cu etching
Ni coating on Pd nanospring



Wang et al, *Nanoscale*, 2014
Wang et al, *Nano Letters*, 2013

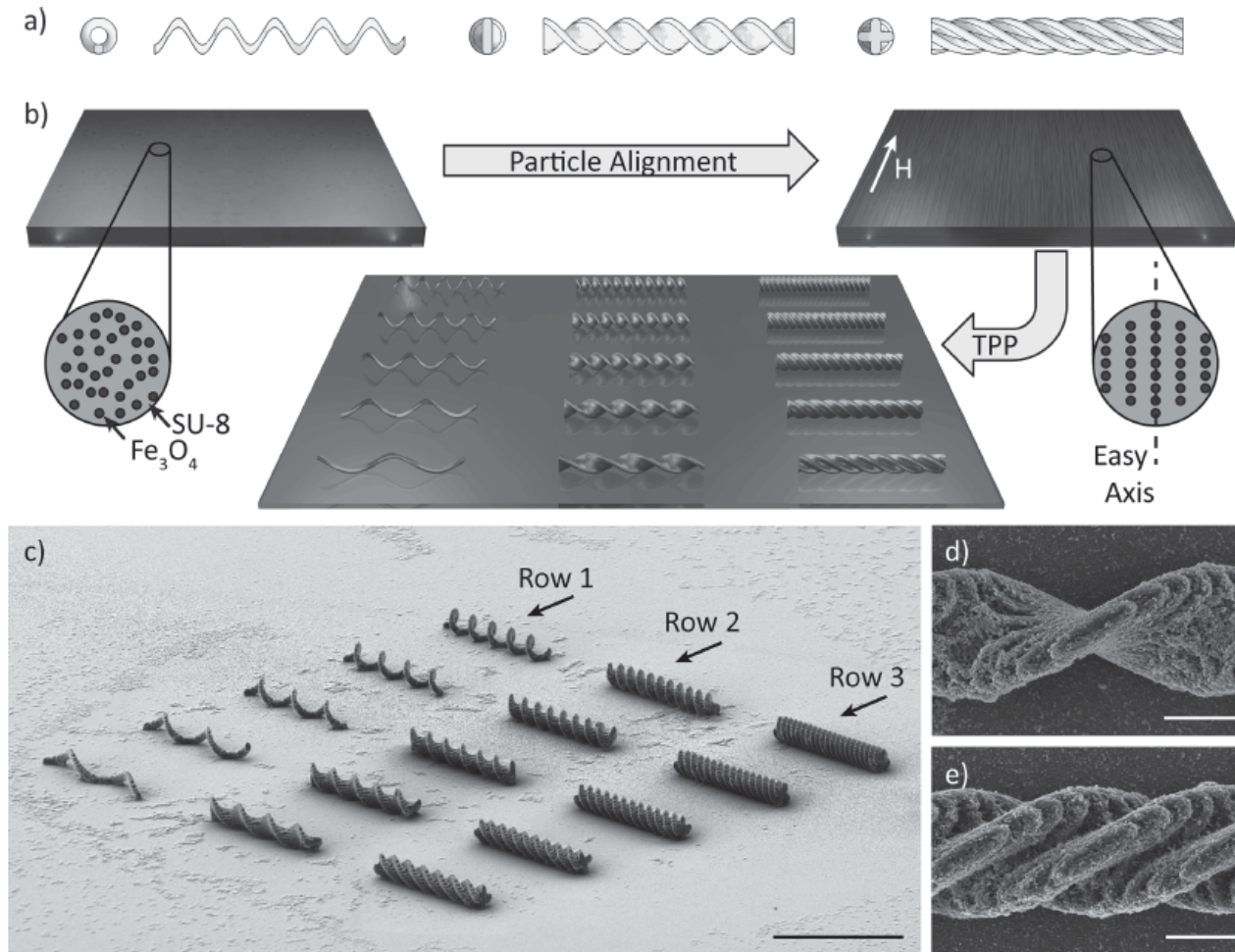
Direct Laser Writing



Nanometer scale resolution
Nickel evaporation for magnetization
Titanium evaporation for functionalization

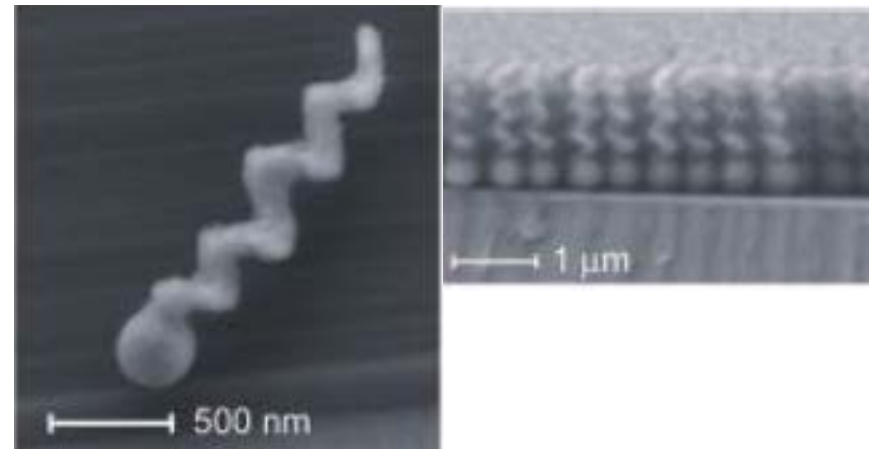
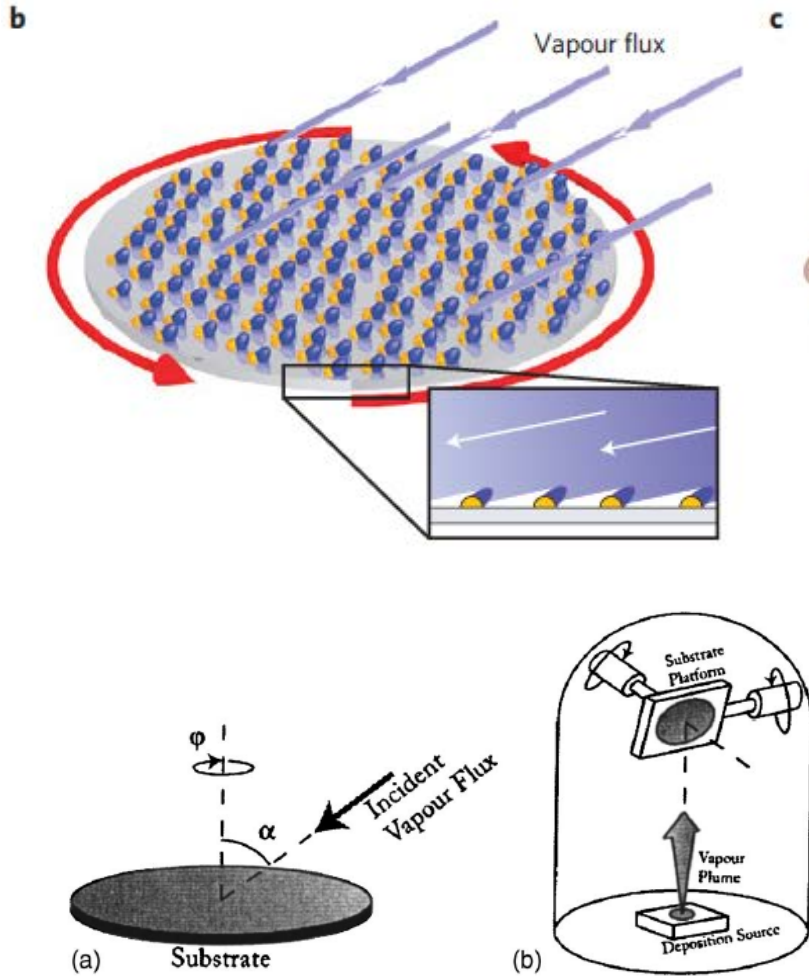
Tottori et al, Adv Mat, 2013

3D Printing of Nanocomposites



Peters et al, *Adv Mater*, 2015

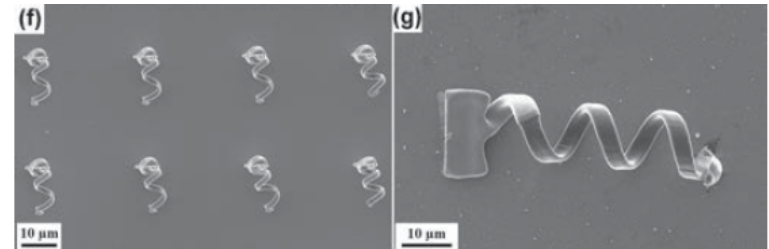
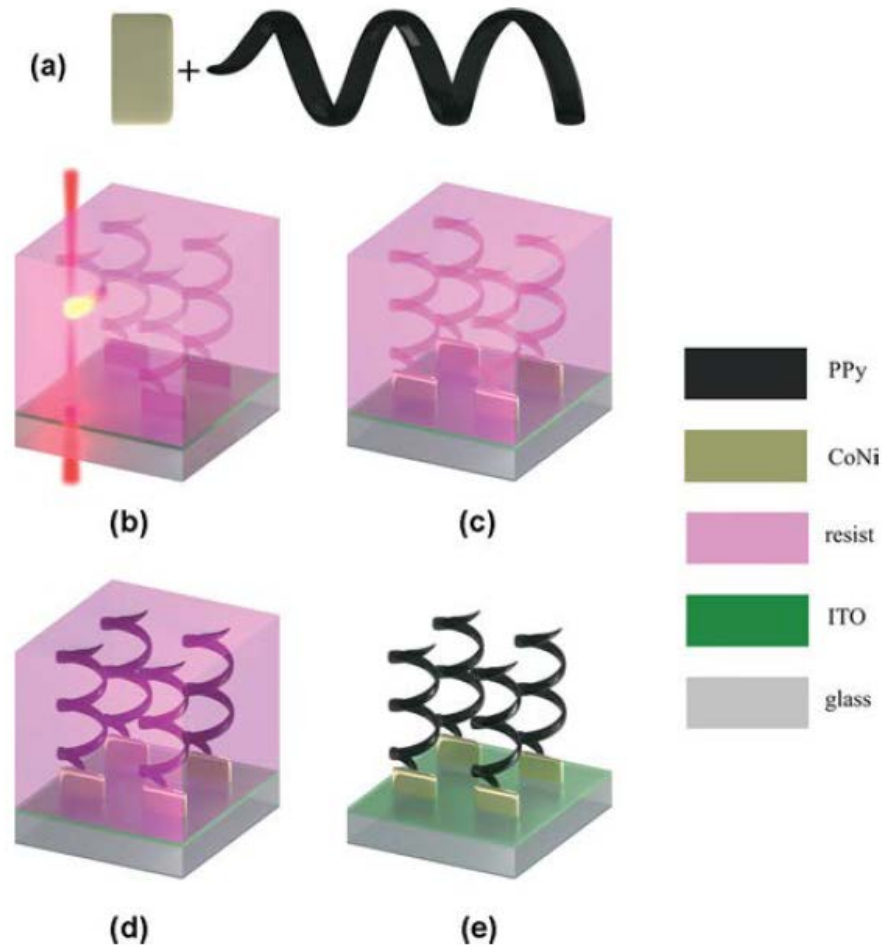
Glancing Angle Deposition



Hawkeye et al, *J Vac Sci*, 2007

Fischer et al, *Nano Letters*, 2009

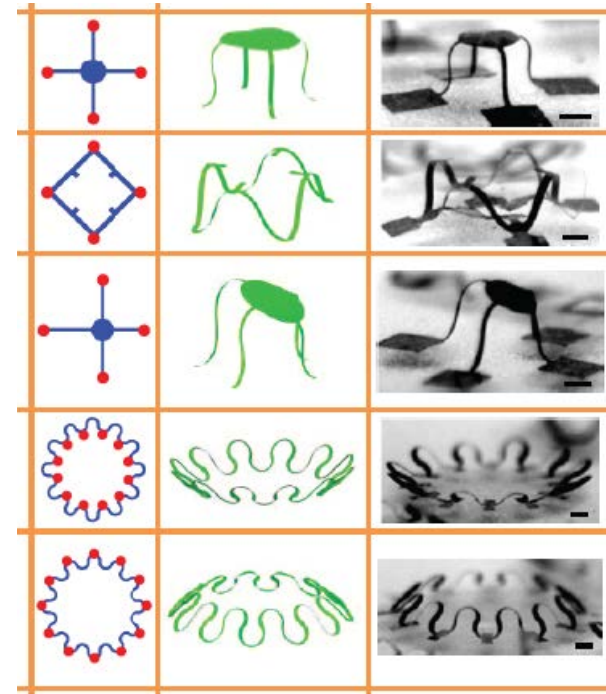
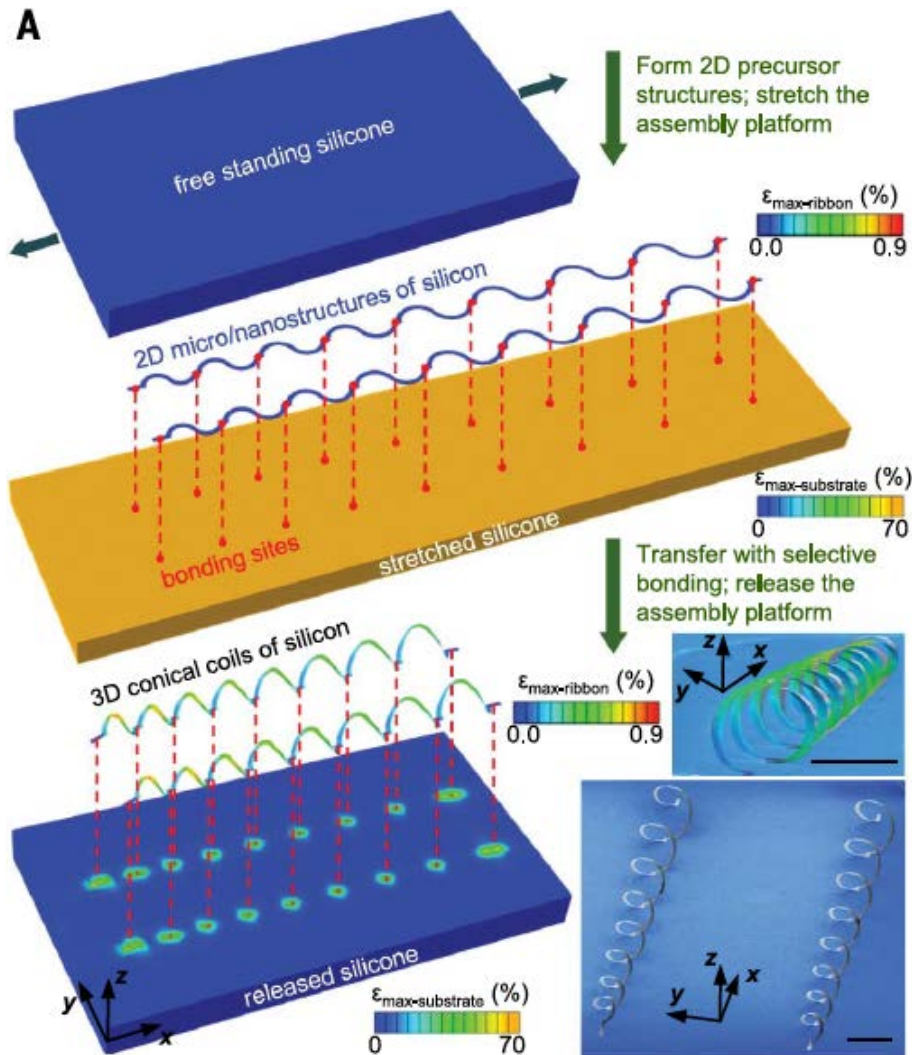
3D Printing and Electrodeposition



3D photoresist template
Fill with electrodeposition
Magnetic head
Polypyrrole Tail

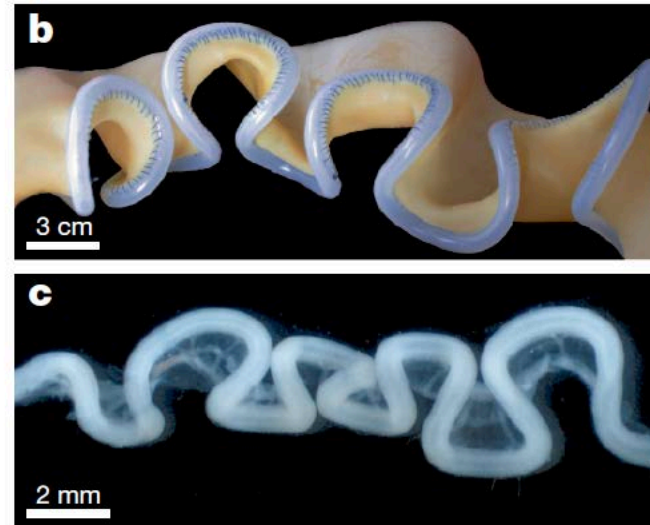
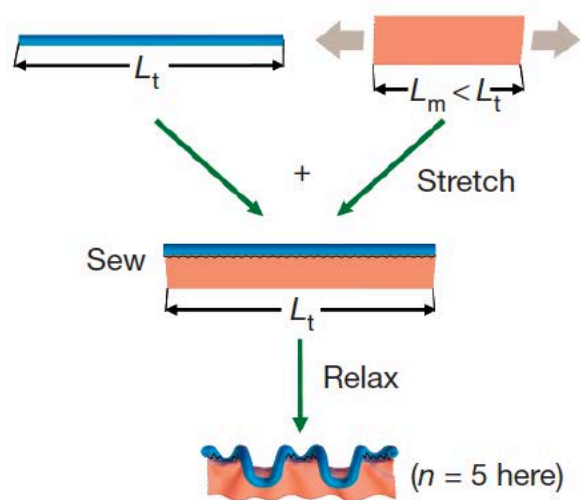
Zeeshan et al, *Small*, 2014

Compressive Buckling of Silicon

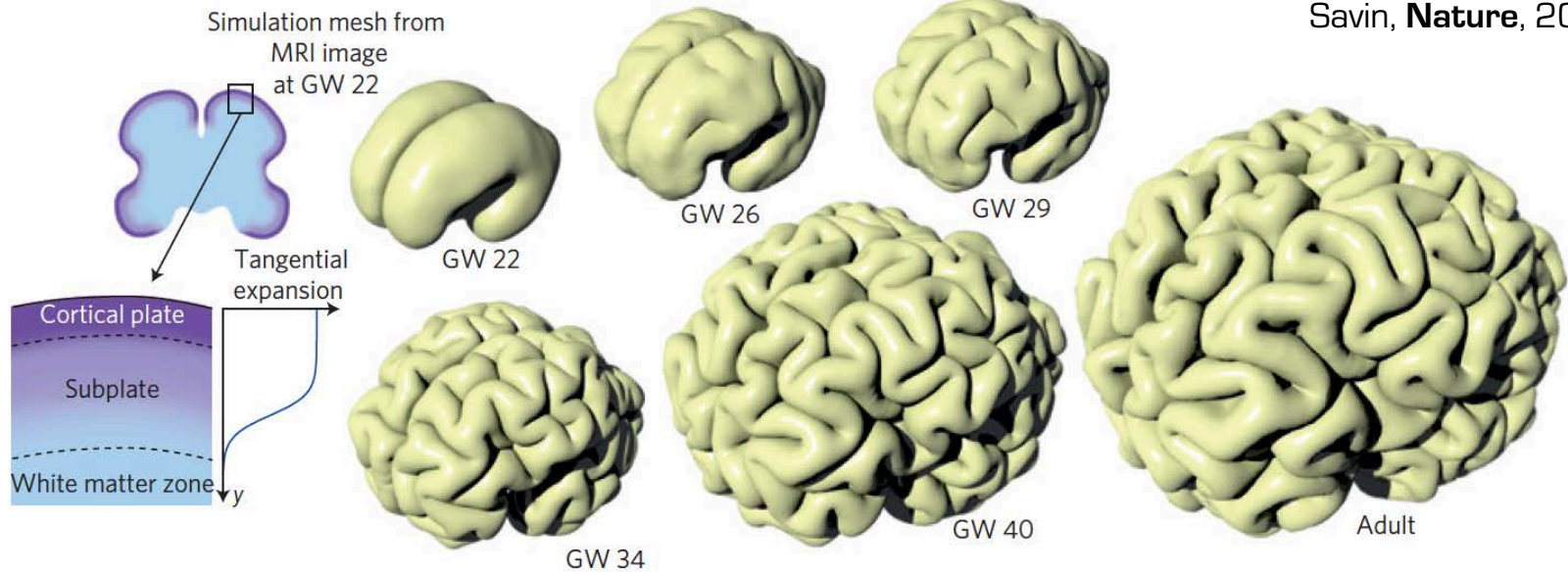


Xu et al, Science, 2015

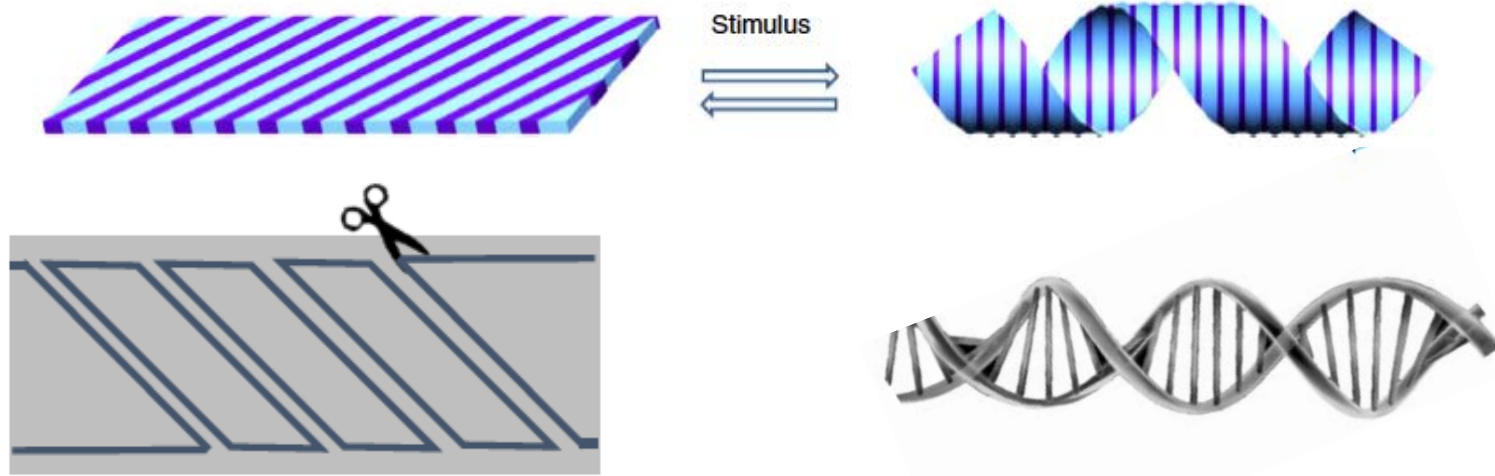
Biological Manufacturing: Differential Growth



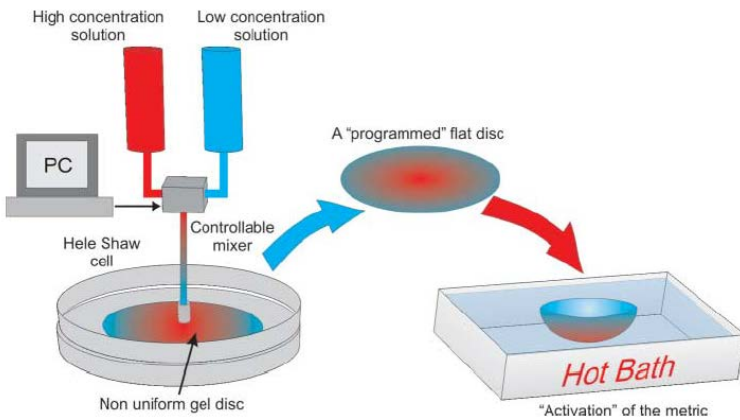
Savin, *Nature*, 2011



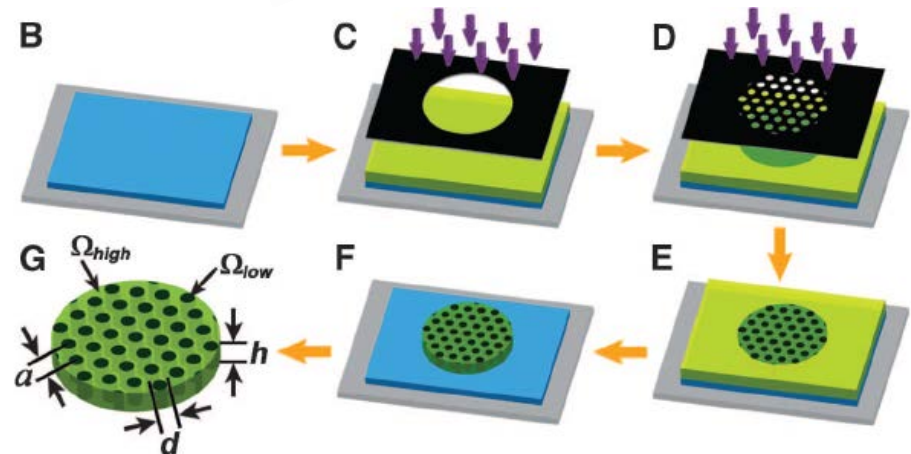
Origami and Kirigami with Hydrogels



Klein et al, *Science*, 2007

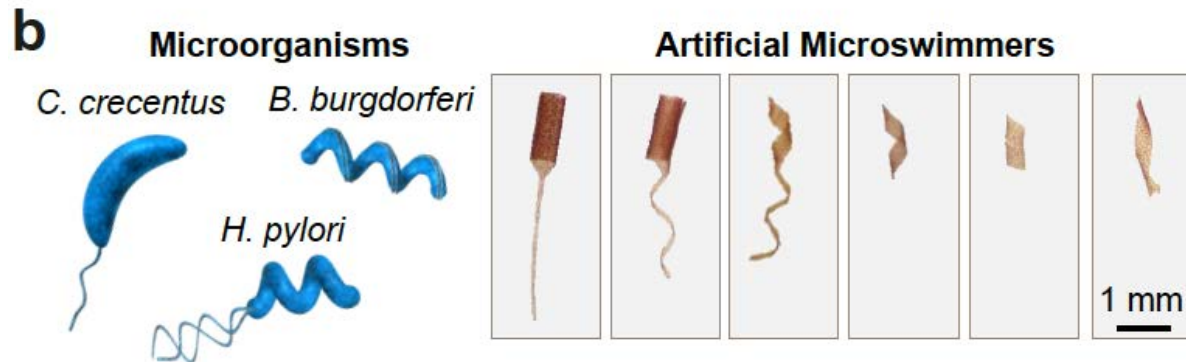
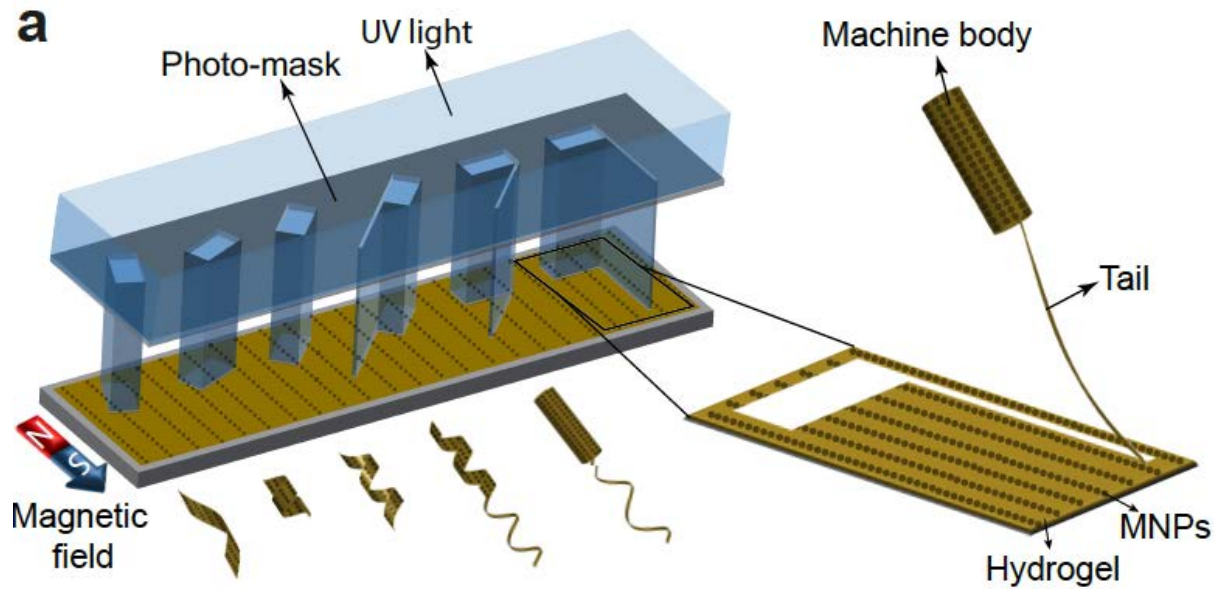


Kim et al, *Science*, 2012

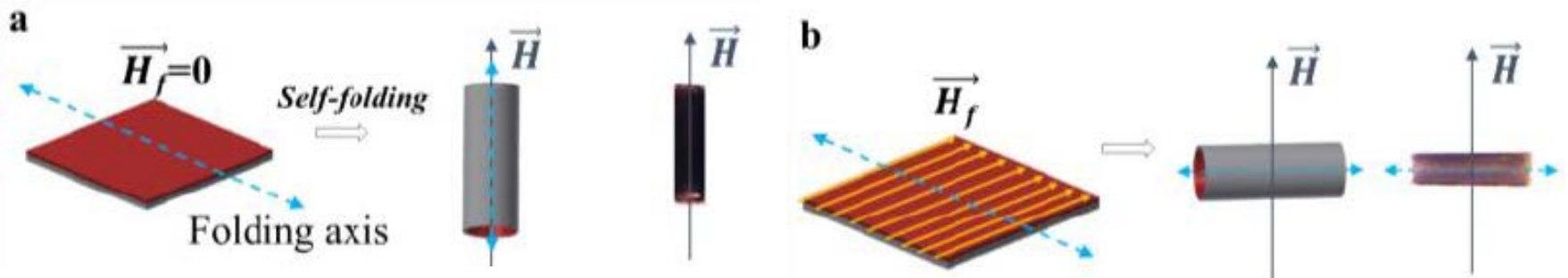
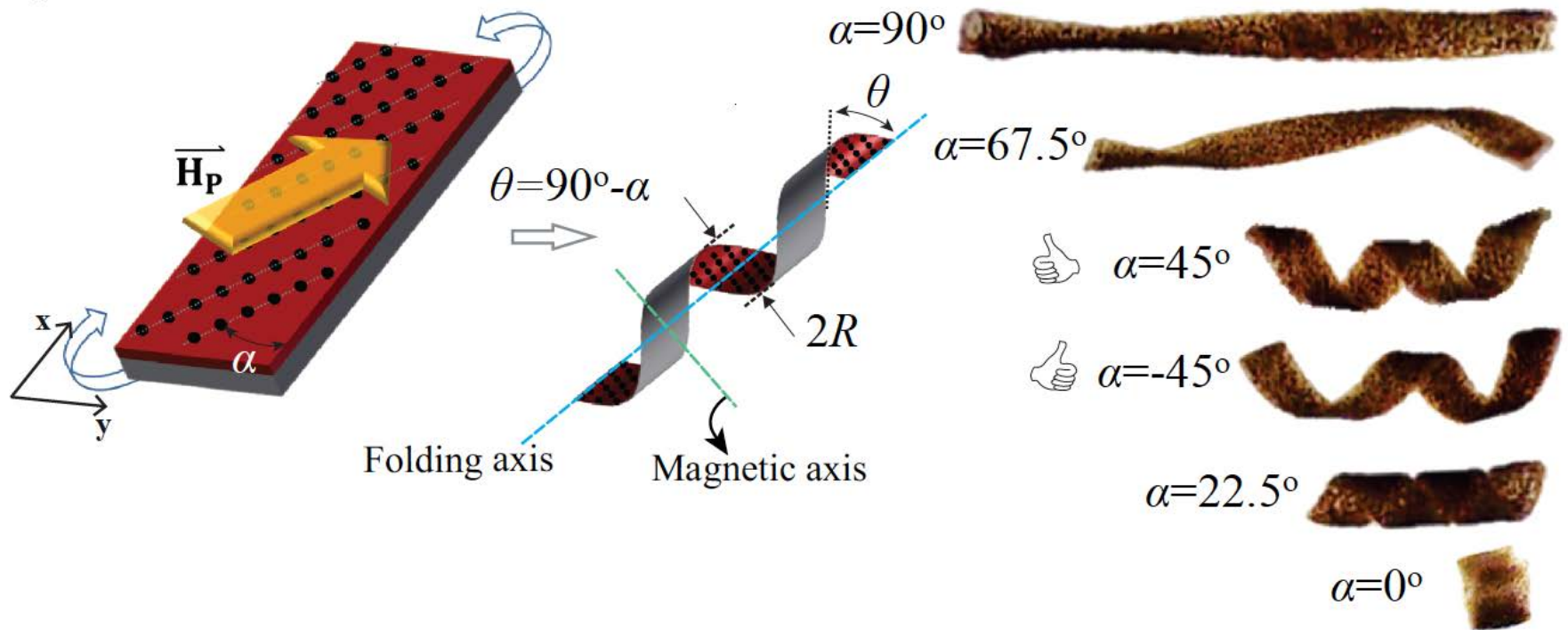


Programmable self-folding

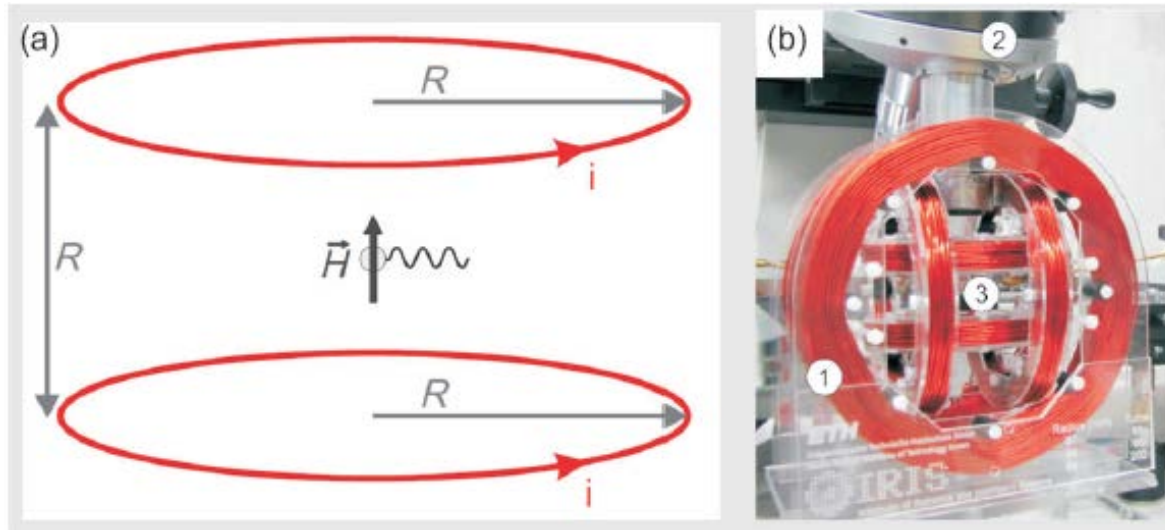
- Differential Swelling via Particle Gradients



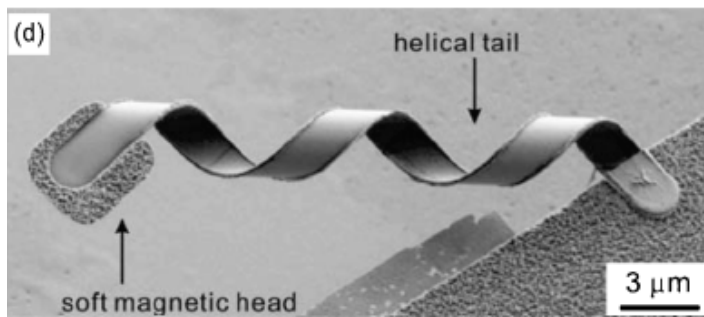
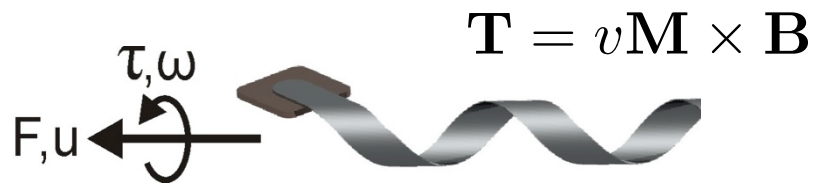
Programming Shape and Magnetic Anisotropy



Artificial Microswimmers



Zhang, **APL**, 2010



Propulsion Matrix

- Linear relationship between force F , torque τ , velocity u and rotational speed ω

$$\begin{pmatrix} F \\ \tau \end{pmatrix} = \begin{pmatrix} a & b \\ b & c \end{pmatrix} \cdot \begin{pmatrix} u \\ \omega \end{pmatrix}$$



- Measuring the parameter of the propulsion matrix
 - Gravity compensation
 - Free-fall
 - Horizontal swimming

$$\begin{pmatrix} a & b \\ b & c \end{pmatrix} = \begin{pmatrix} 1.5 \cdot 10^{-7} & 1.6 \cdot 10^{-14} \\ 1.6 \cdot 10^{-14} & 1.5 \cdot 10^{-19} \end{pmatrix}$$

Propulsion Matrix

- **Experiment 1:** Vertical balancing ($u = 0$)
 - ABF in vertical position
 - Propulsive force equalizes the external forces (gravity & buoyancy)

$$F_{ext} = -F_{grav} + F_{buoy}$$



$$F = a \cdot u + b \cdot \omega \quad \text{(i)} \quad b = \frac{F_{ext}}{\omega}$$
$$\tau = b \cdot u + c \cdot \omega \quad \text{(ii)}$$

- Experiment: tune ω until ABF does not move out of focus anymore
 - $F_{ext} = -5.1 \cdot 10^{-13}$ N, $\omega = 31$ rad/s

$$b = -1.6 \cdot 10^{-13} \text{ N}\cdot\text{s}$$

Propulsion Matrix

- **Experiment 2:** Vertical free-fall ($\tau = 0$)
 - ABF in vertical position
 - Free-fall velocity

$$F = a \cdot u + b \cdot \omega \quad (\text{i})$$

$$\tau = b \cdot u + c \cdot \omega \quad (\text{ii})$$

$$u = \frac{F_{\text{ext}} - b\omega}{a}$$

$$c = -\frac{b \cdot u}{\omega}$$



- Experiment: switch off actuation and record rotational speed
 - $\omega = -0.28$ rad/s

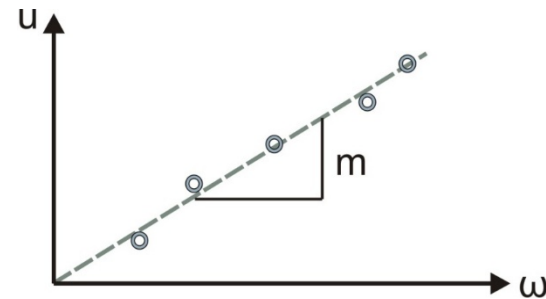
$$\mathbf{c = 2.3 \cdot 10^{-19} \text{ N} \cdot \text{s} \cdot \text{m}}$$

Propulsion Matrix

- **Experiment 3:** Horizontal swimming ($F = 0$)
 - ABF in horizontal position



$$F = a \cdot u + b \cdot \omega \quad \text{(i)} \quad u = -\frac{b}{a} \omega$$
$$\tau = b \cdot u + c \cdot \omega \quad \text{(ii)} \quad \underbrace{\quad}_{=: m}$$

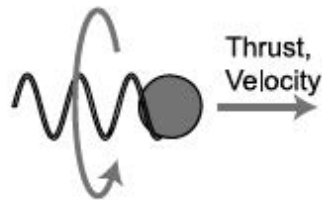


- Experiment: drive ABF at different frequencies and record velocities
 - Extract slope m of the linear ω - u relationship
 - $m = 1.1 \cdot 10^{-7} \text{ m/rad}$

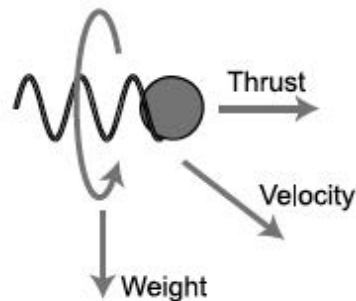
$$\mathbf{a = 1.5 \cdot 10^{-7} \text{ N}\cdot\text{s/m}}$$

Gravity Compensation

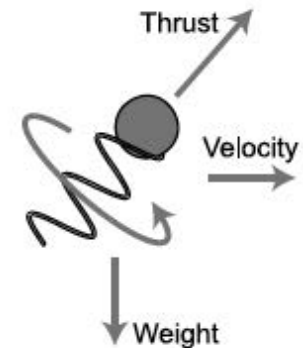
- Density depends on material choice
- Moving up against gravity



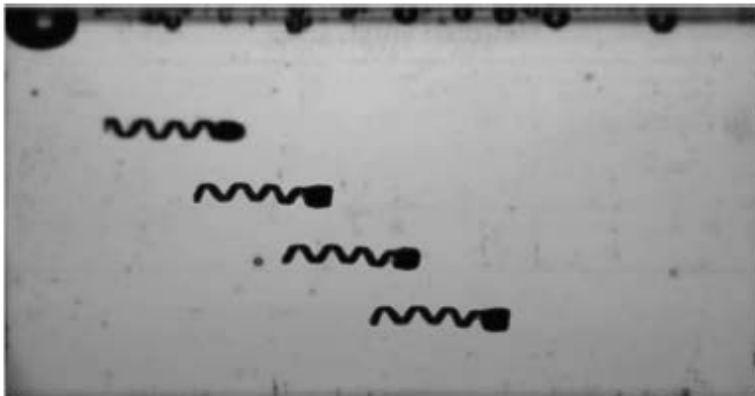
(a) Neutrally buoyant swimmer



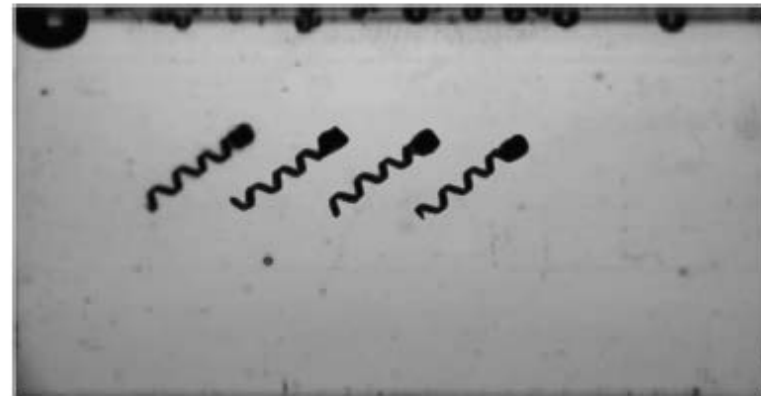
(b) Heavy swimmer



(c) Gravity compensation

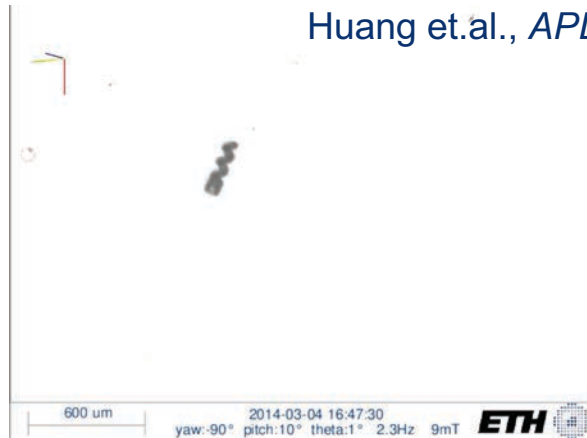
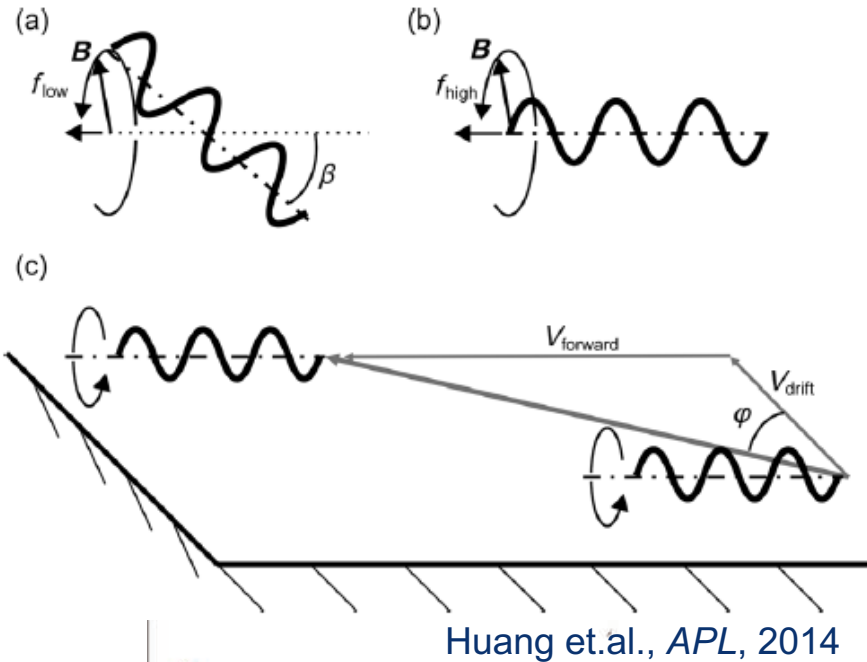


(d) Experiment without gravity compensation

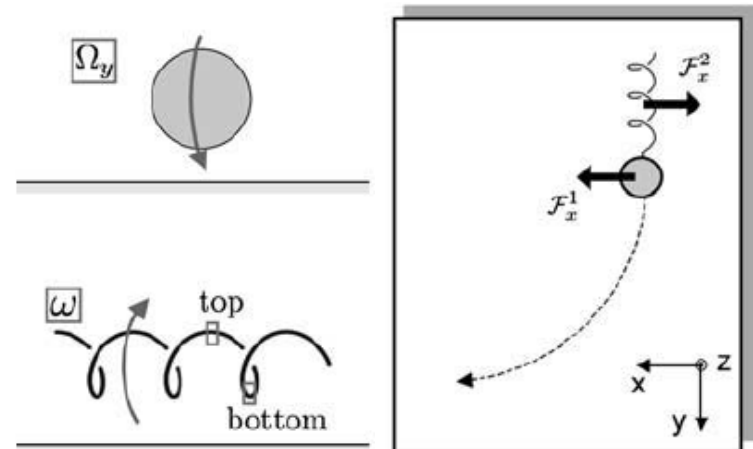
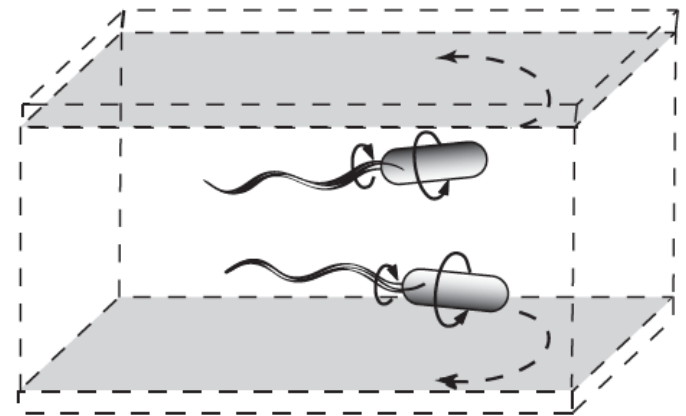


(e) Experiment with gravity compensation

Wobbling Motion and Drift



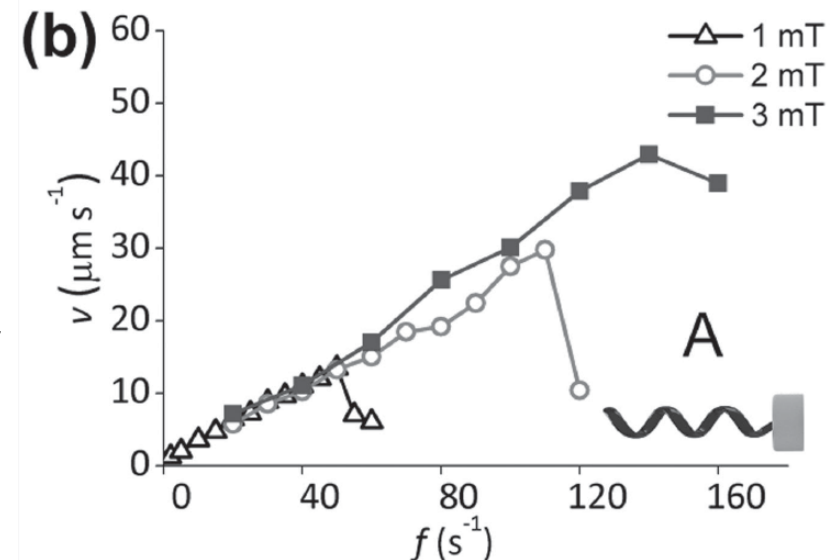
Bacteria swim in circles near planar surfaces



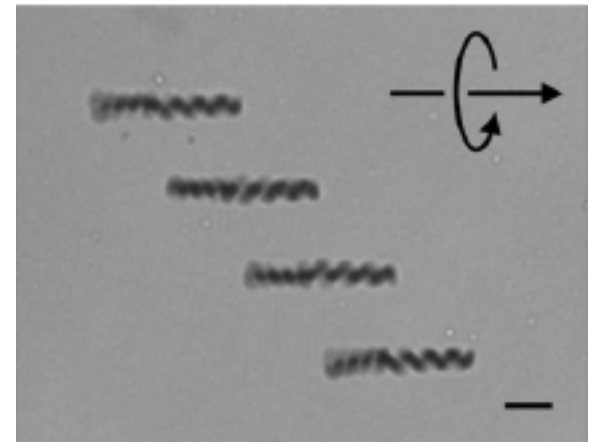
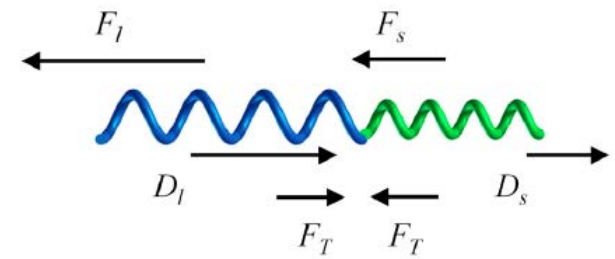
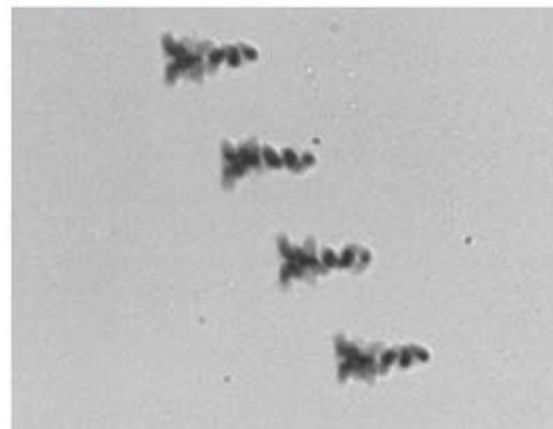
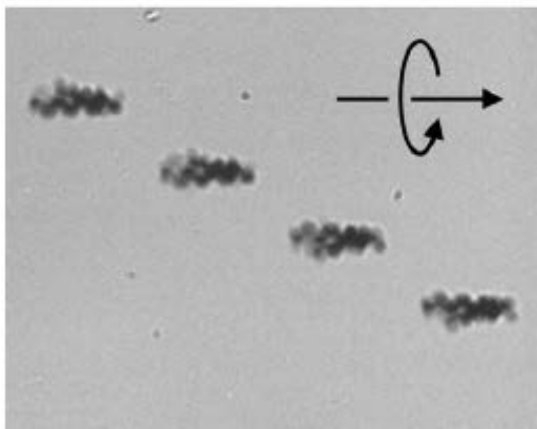
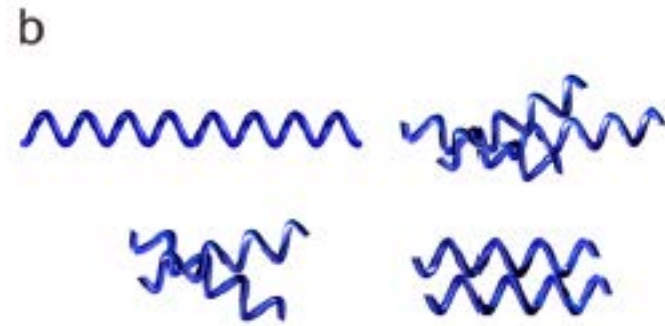
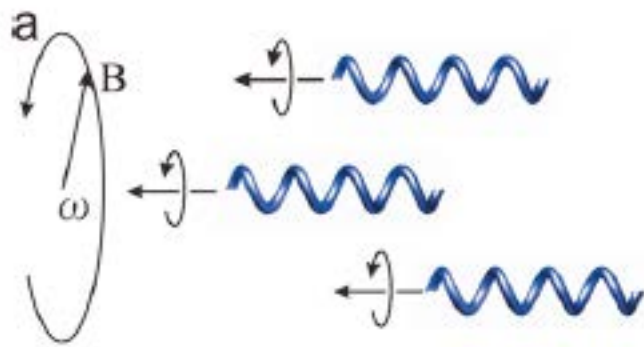
DiLuzio et.al., *Nature*, 2005

Step-out Frequency

- When the applied magnetic field rotates sufficiently slowly, the robots synchronously rotate with the field
- There exists a rotation frequency above which the applied magnetic torque is not strong enough to keep the robot synchronized with the field
 - Step-out frequency
- Step-out frequency depends on
 - Robot magnetization
 - Friction
 - Field strength
- Robot's velocity rapidly declines when operated above step out frequency

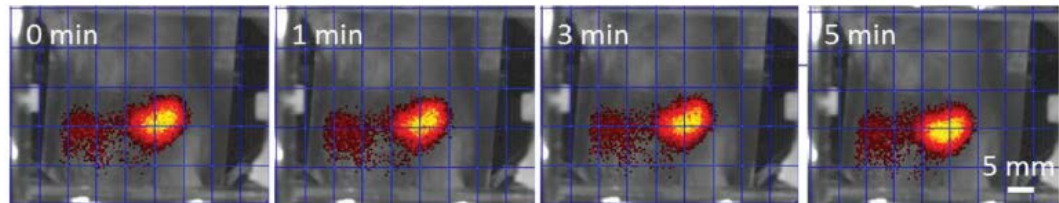
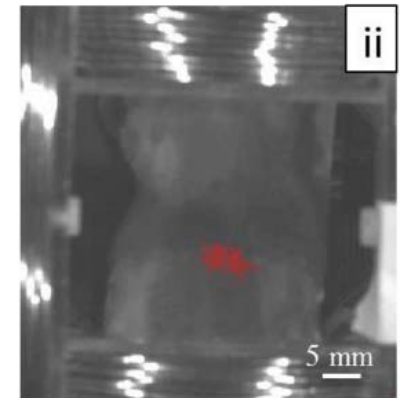
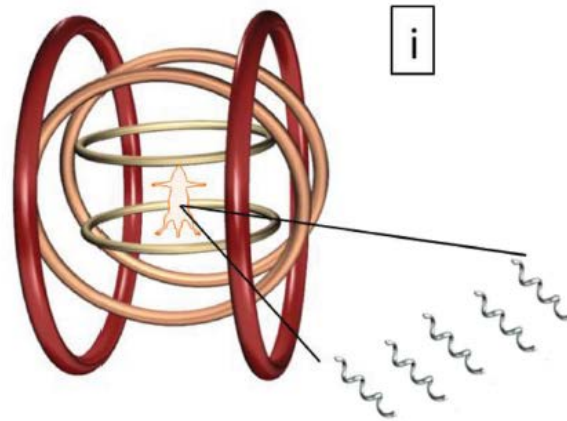
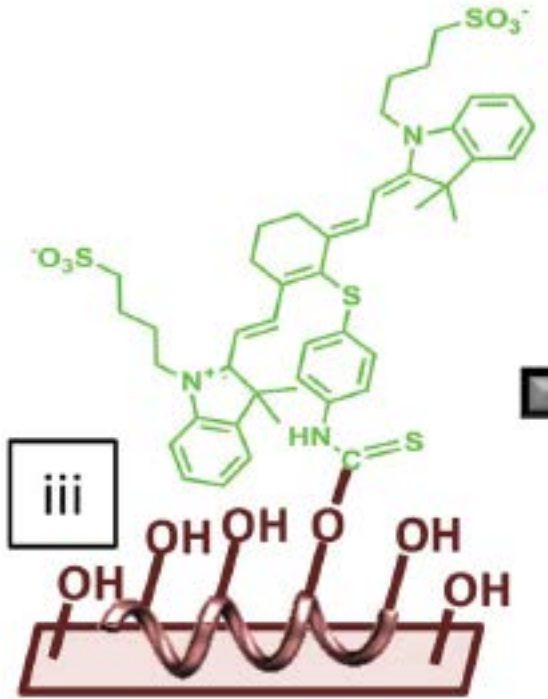


Assembly in Active Micromachine Suspensions



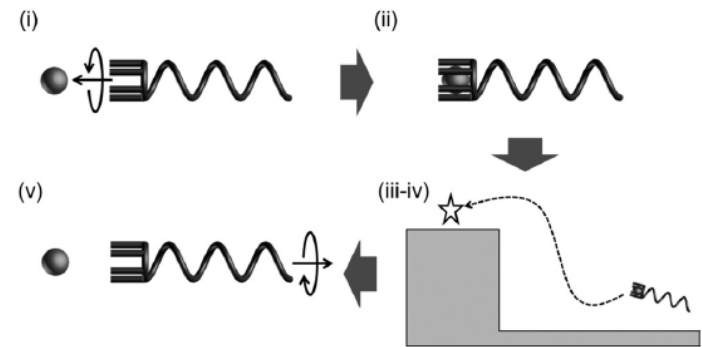
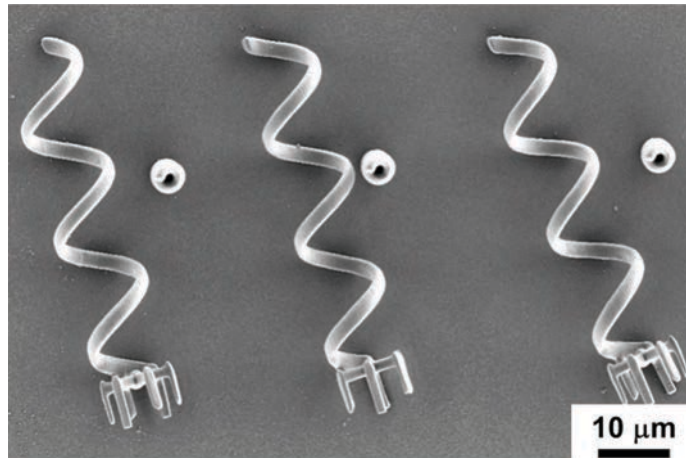
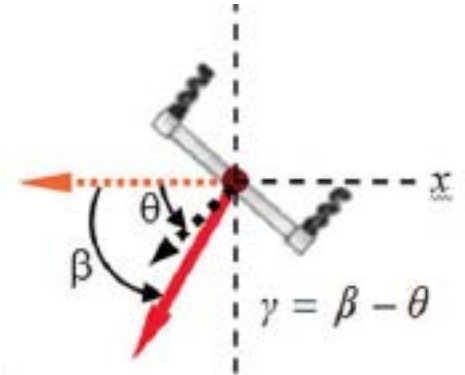
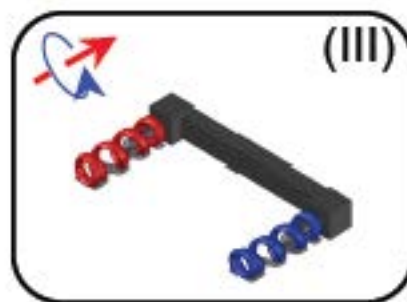
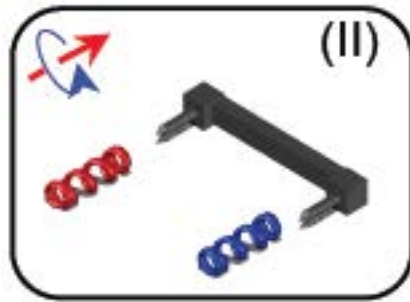
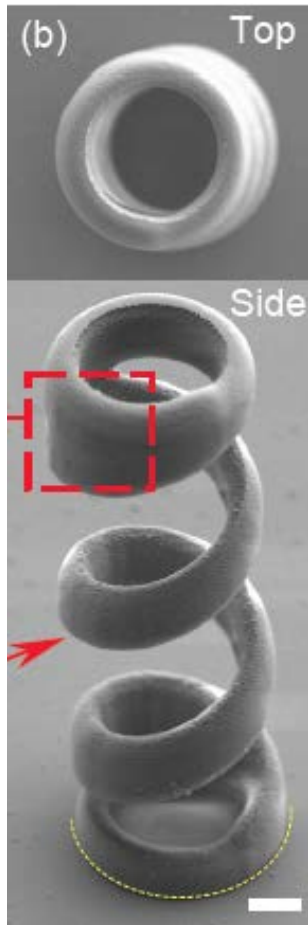
Microswimmers in the Mouse Peritoneal Cavity

Near Infrared Fluorophore: NIR-797
Swarms of microrobots



Servant, *Adv Mater*, 2015

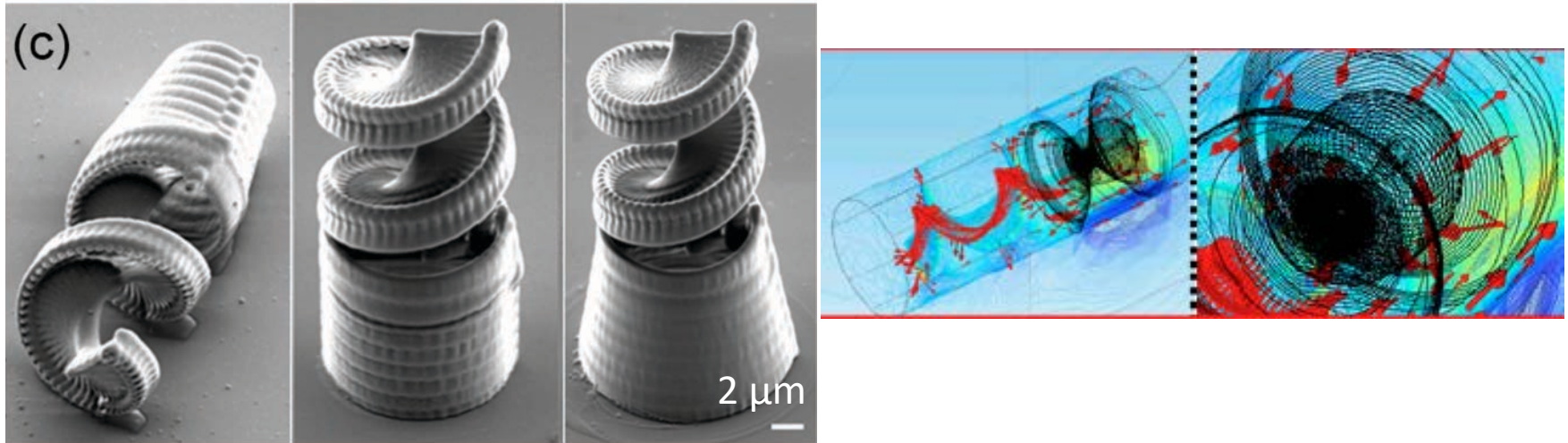
Microtransporter (contact mode)



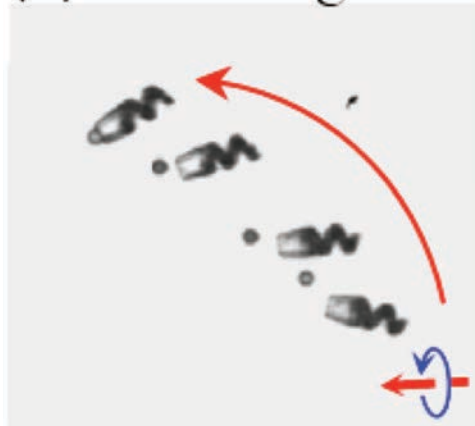
S. Tottori et.al., Advanced Materials, 2012

T Huang et.al., RSC Adv, 2014

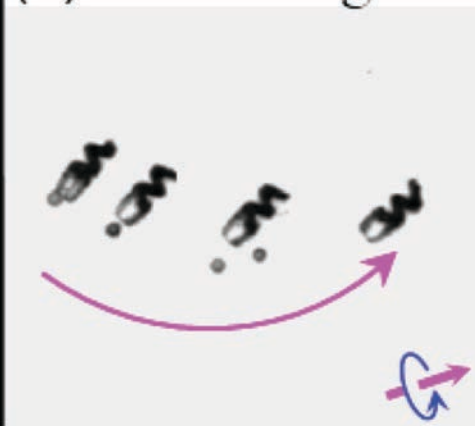
Mobile Fluidic Traps in 3D



(a) Loading



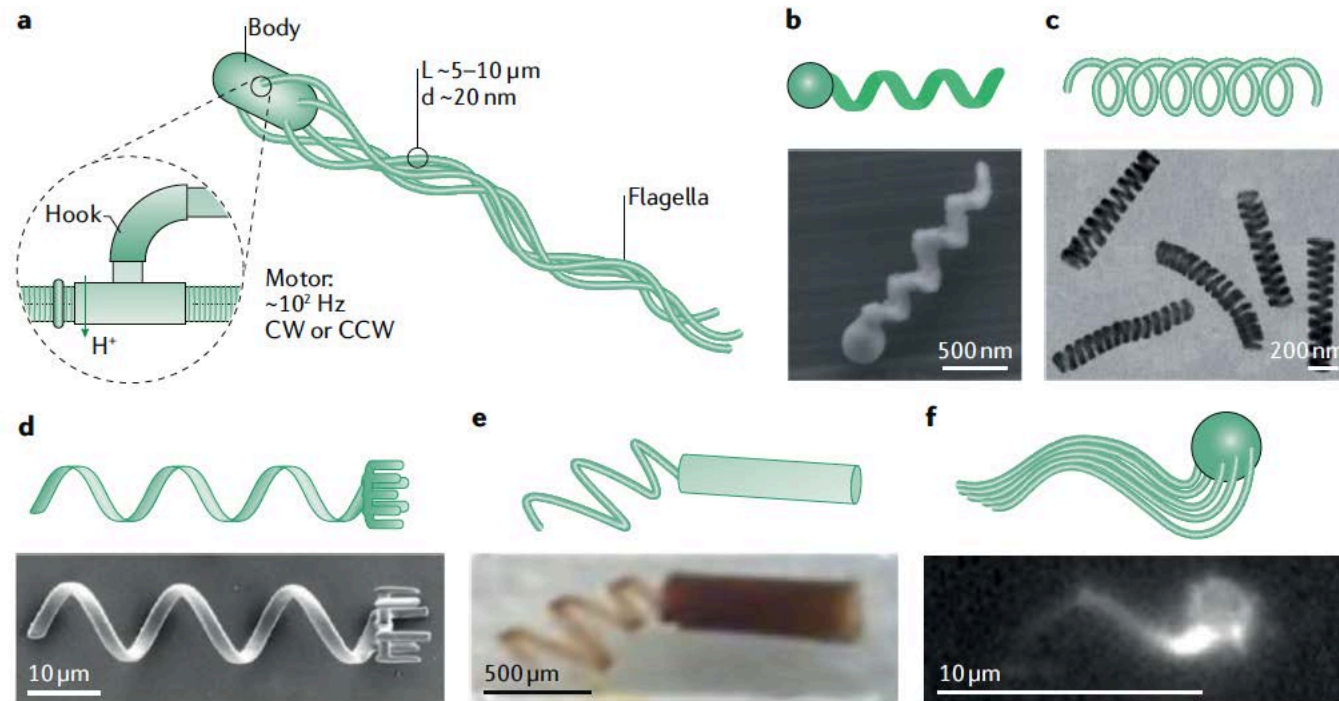
(b) Releasing



T Huang et al, APL, 2014

Swimming at Low Reynolds Number

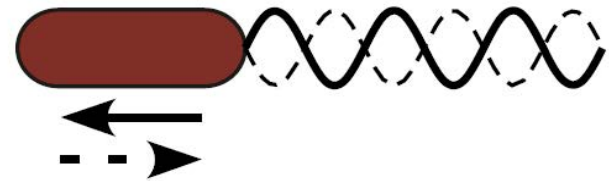
- How to elude the scallop theorem (Aristotelian fluid regime)
 - Rotate a chiral arm
 - Wave an elastic arm



Eukaryotic Flagella and Cilia

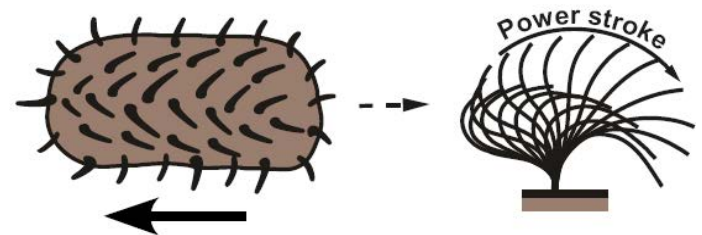
- **Eukaryotic flagella**

- Active organelles which create traveling waves
- Swimming direction can be reversed by reversing the direction of the wave
 - Head-to-tail: moving forward
 - Tail-to-head: moving backwards



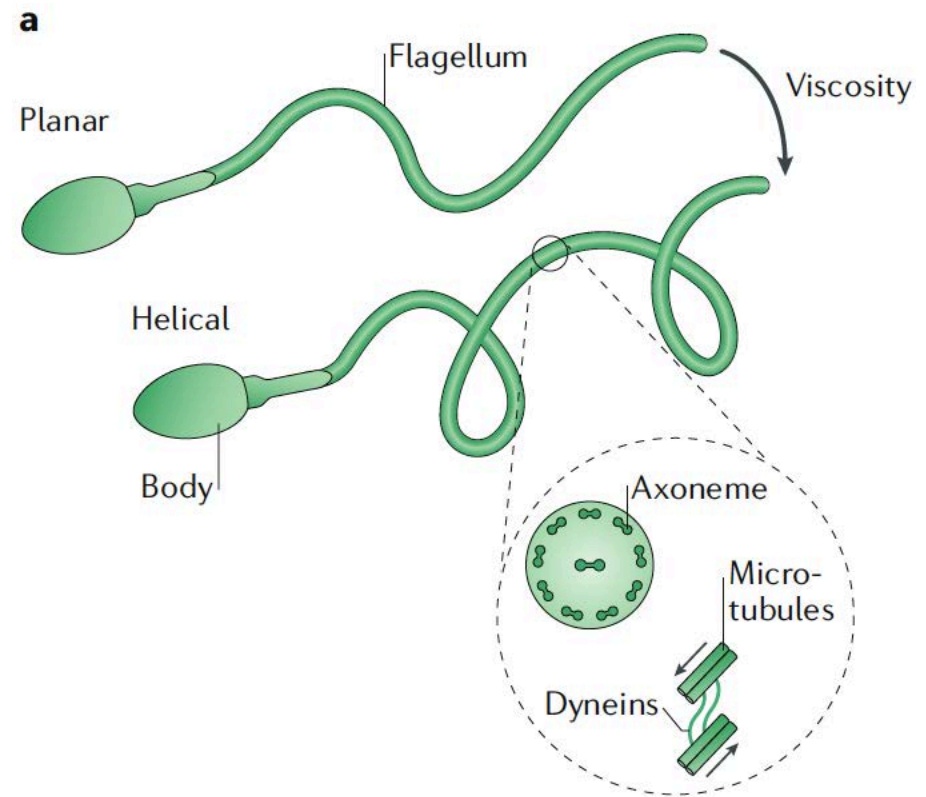
- **Cilia**

- Active organelles
- Held perpendicular during the power stroke
- Parallel during recovery stroke



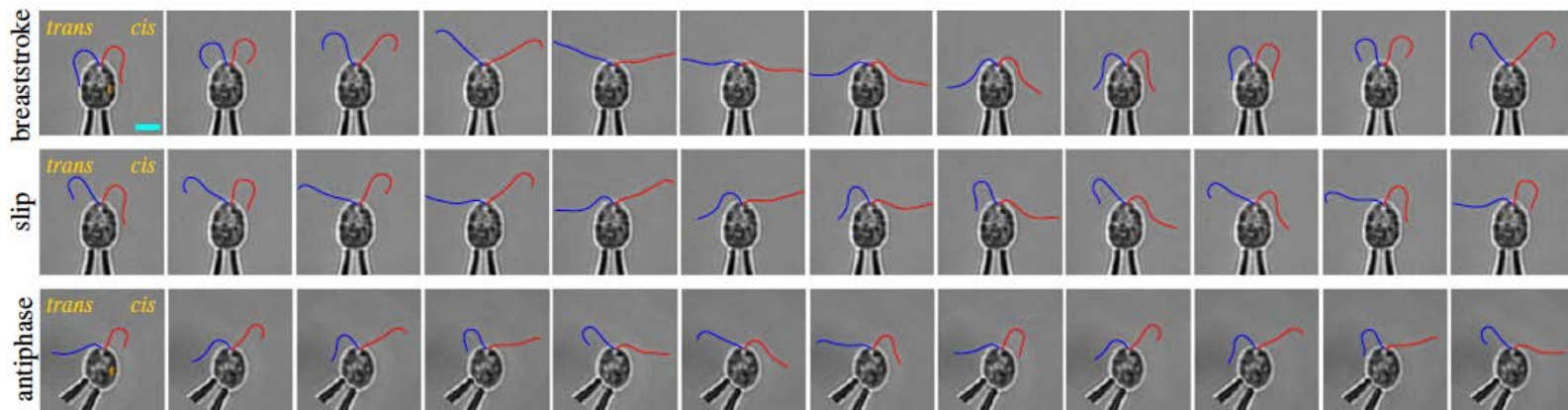
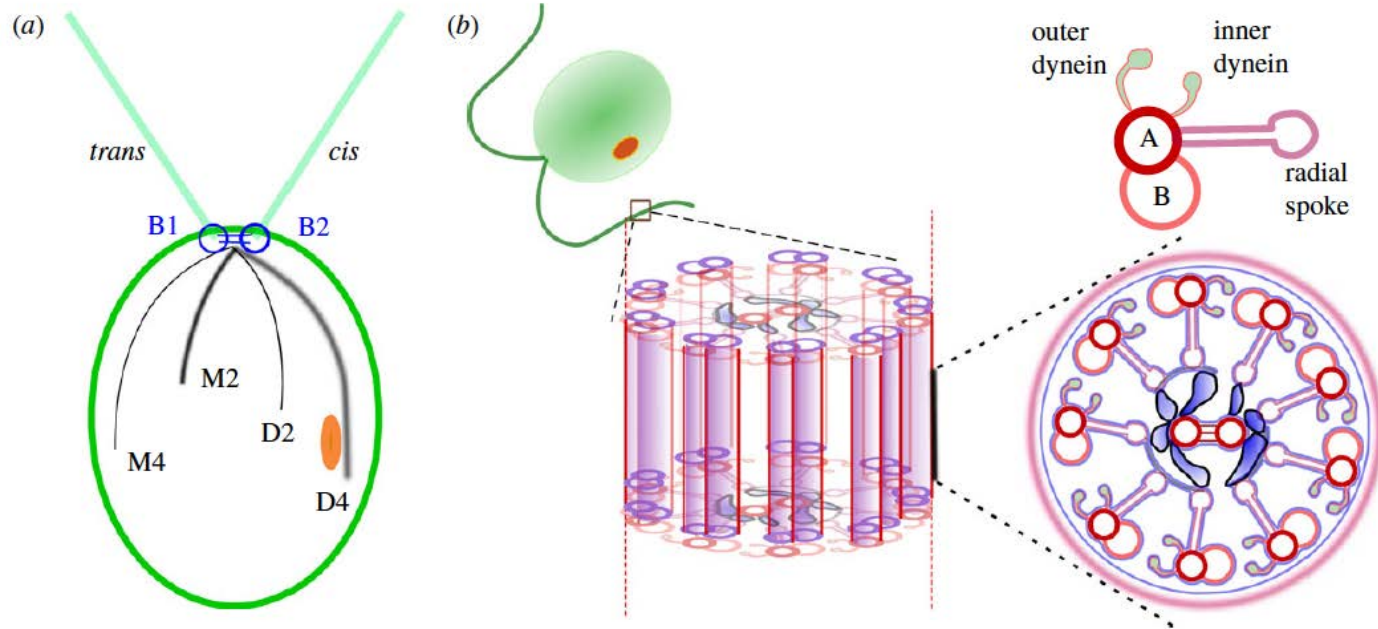
Eukaryotic Flagellum

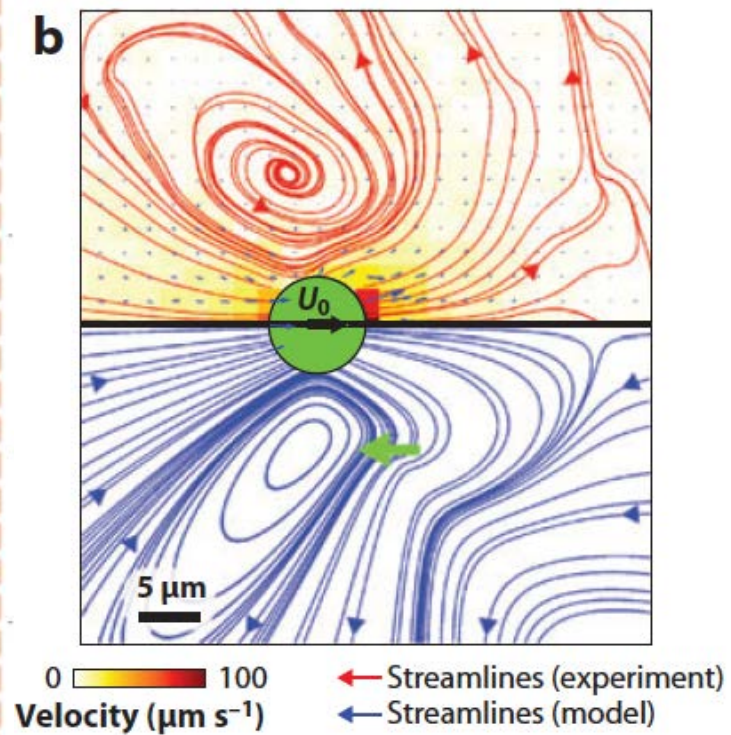
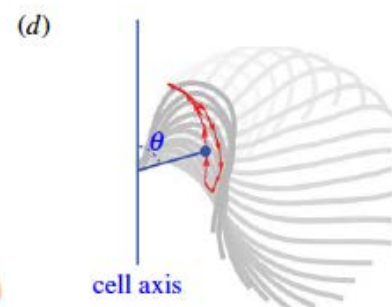
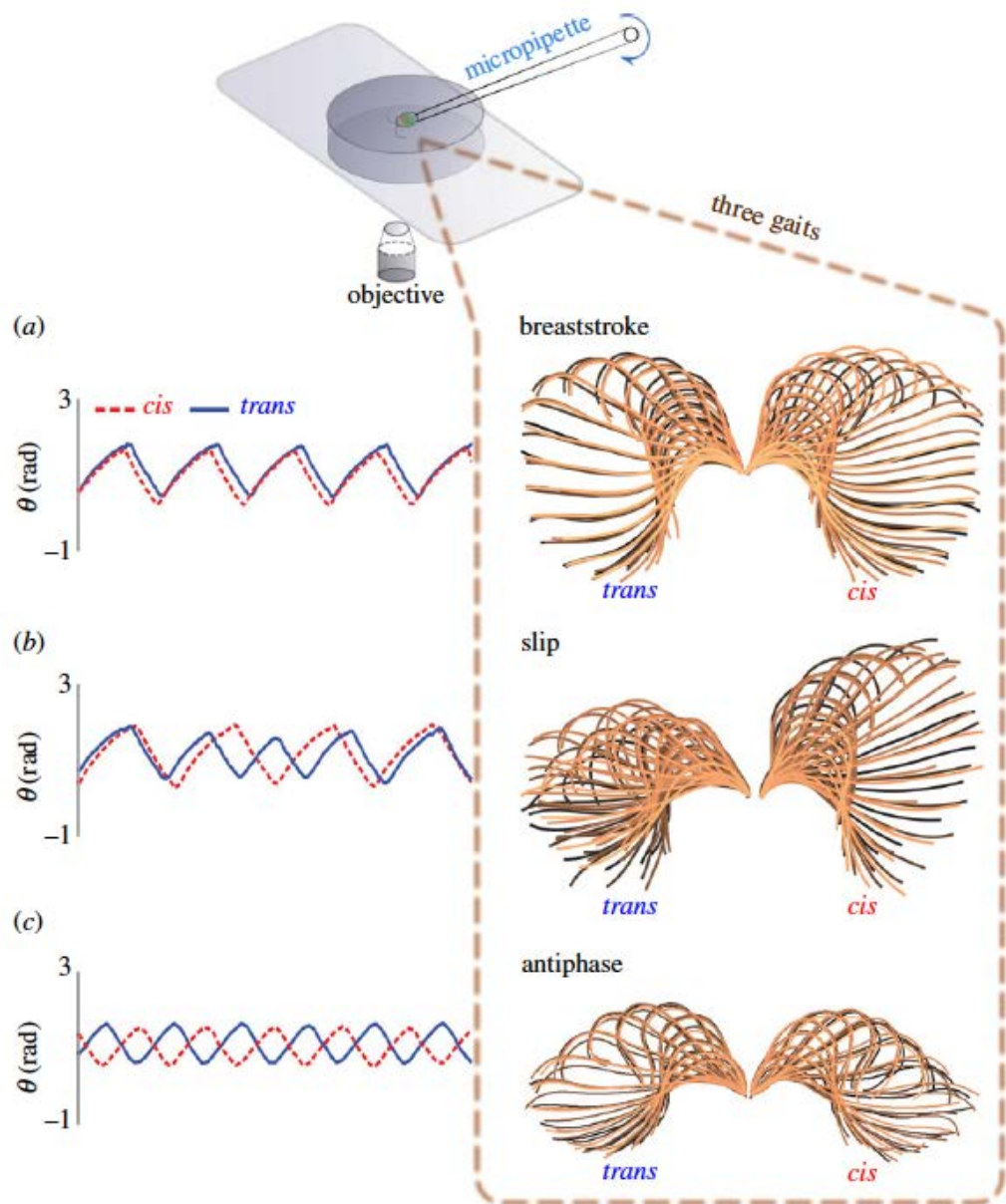
- Sperm cells swim owing to bending waves that propagate along their long, flexible flagellum
- The whole tail is actuated
 - Bending is powered by dynein motor proteins that cause sliding of microtubule doublets in the axoneme
- The waveform depends on the viscosity of the surrounding fluid: planar or helical
- Long and thin flagellum
 - Guarantees asymmetry in the resistance to forward and sideways motion



Biflagellate Alga *Chlamydomonas*

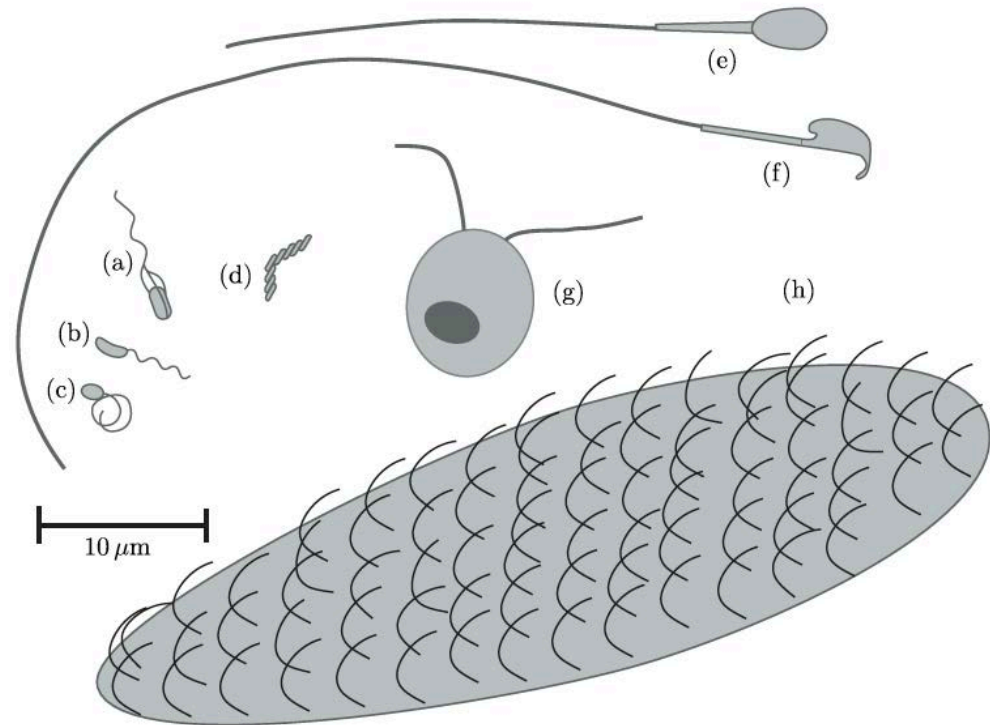
movie





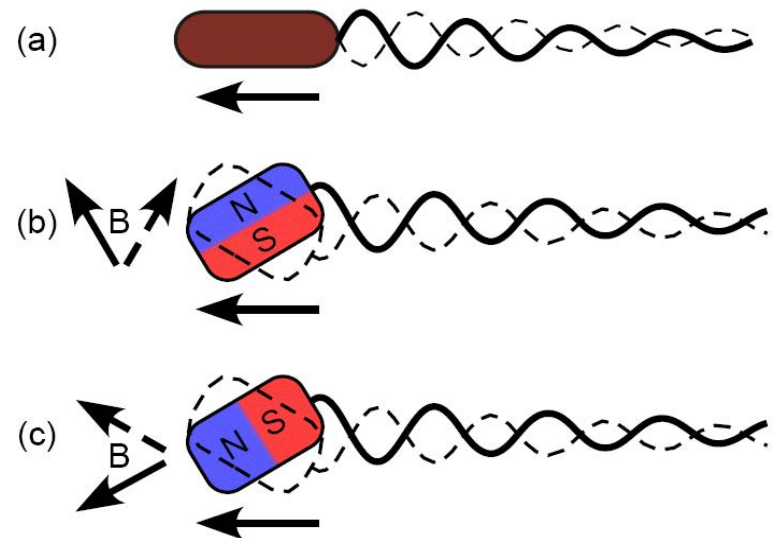
Scaling of Appendage Size

- Eukaryotic flagella are at least ten times larger (diameter and length) than bacterial flagella
 - Typical diameter: 20nm vs 200nm
- Cilia: thousands of small appendages that beat in coordinated manner
 - Propelling the cell at speeds of 500 $\mu\text{m}/\text{s}$
- With increasing size, we see a transition from flagellum to cilia



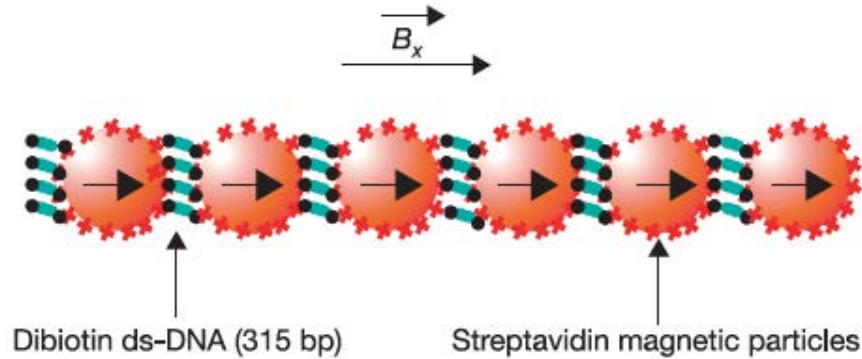
Bioinspired Swimming: Elastic Oar

- One-sided actuation
 - There exists an optimum in tail elasticity and length
 - Too short & rigid
 - “Scallop theorem”
 - Too long & elastic
 - Increased drag
- Use of varying magnetic fields
 - Magnetic field creates a torque on a magnet
 - By varying the field, the torque is a function of time
 - Induces a waving motion to the following tail



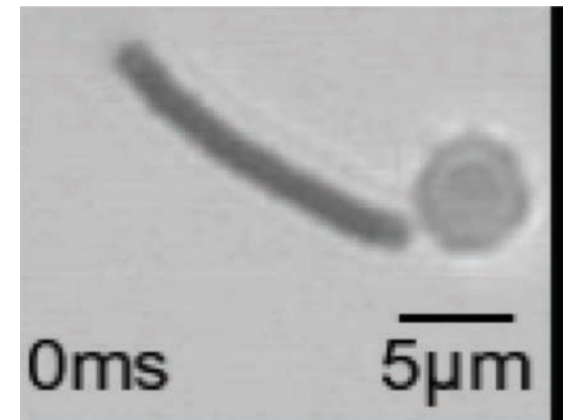
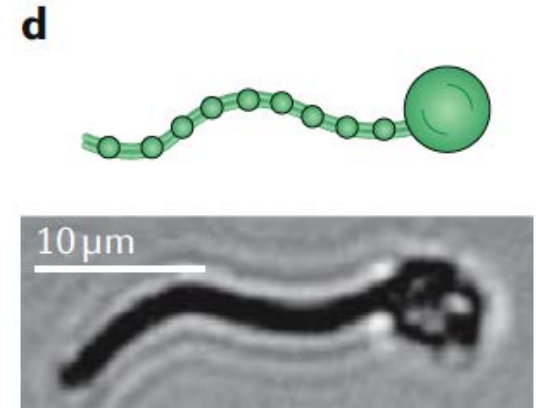
Artificial Eukaryotic Flagellum

Dreyfus et al,



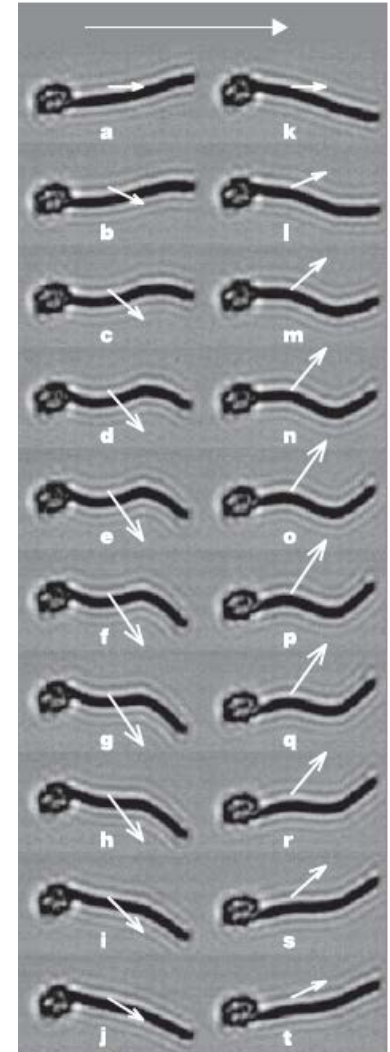
$$\mathbf{B}_x = B_x$$
$$\mathbf{B}_y = B_y \sin(2\pi ft)$$

- Magnetic microbeads
 - Each bead has an easy axis
 - They are linked with DNA
 - The beads tend to align with an oscillating external magnetic field



Artificial Eukaryotic Flagellum

- An undulation that propagates toward the attachment point from the tip of the tail
- Remember that in sperm cells bending wave propagates from head to tail



Sperm Number

- A dimensionless number that represents the relative importance of viscous to elastic stresses on a filament

$$S_p = \frac{L}{\sqrt[4]{\left(\frac{\kappa}{\xi_{\perp} \omega}\right)}}$$

L: length of the filament

κ : bending rigidity

ω : angular driving frequency

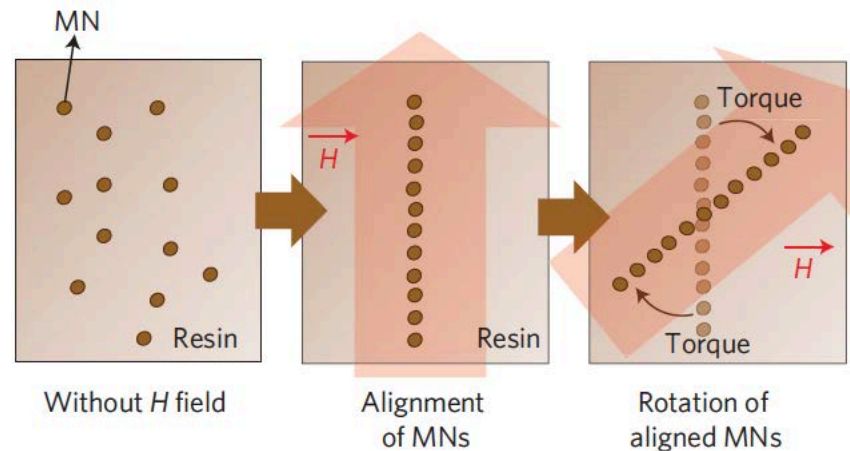
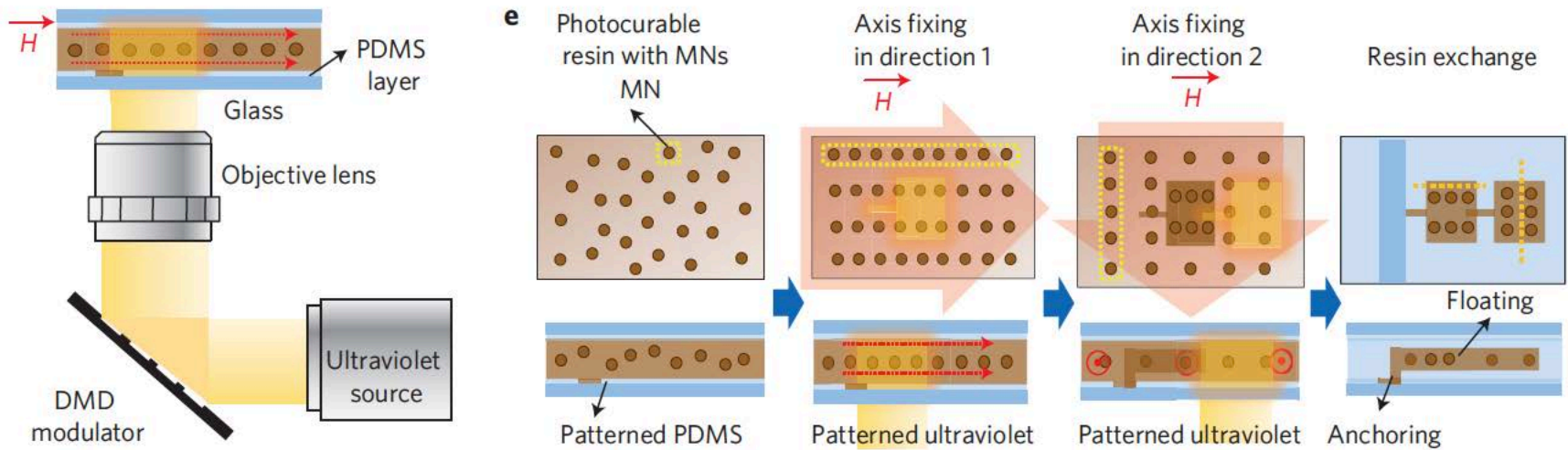
ξ_{\perp} : perpendicular viscous coefficient

- For a one-armed swimmer, two extreme regimes emerge
 - At low S_p , internal elasticity dominates
 - At high S_p , viscous friction dominates
- Maximum normalized swimming speed ($V/L\omega$) is attained for S_p of the order unity (for sperm cells $S_p = 7$)

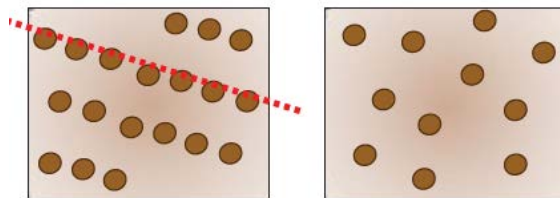
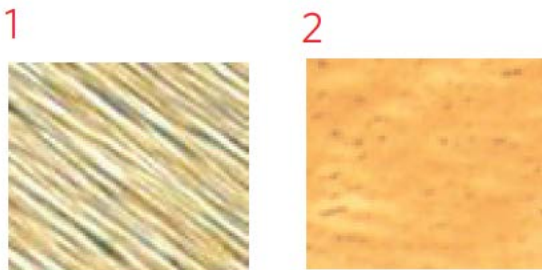
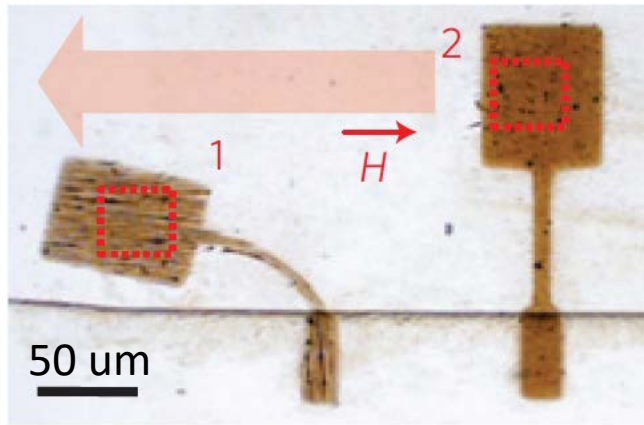
Soft Magnetic Composites

- Embedding particles of low-coercivity ferromagnetic materials in hydrogels
 - Soft magnetic materials
 - Iron and iron oxides
- Soft magnetic materials develop strong magnetization along the applied magnetic field
- They do not retain the strong magnetism once the external field is removed
- Deformation is limited to elongation or compression under magnetic field gradients

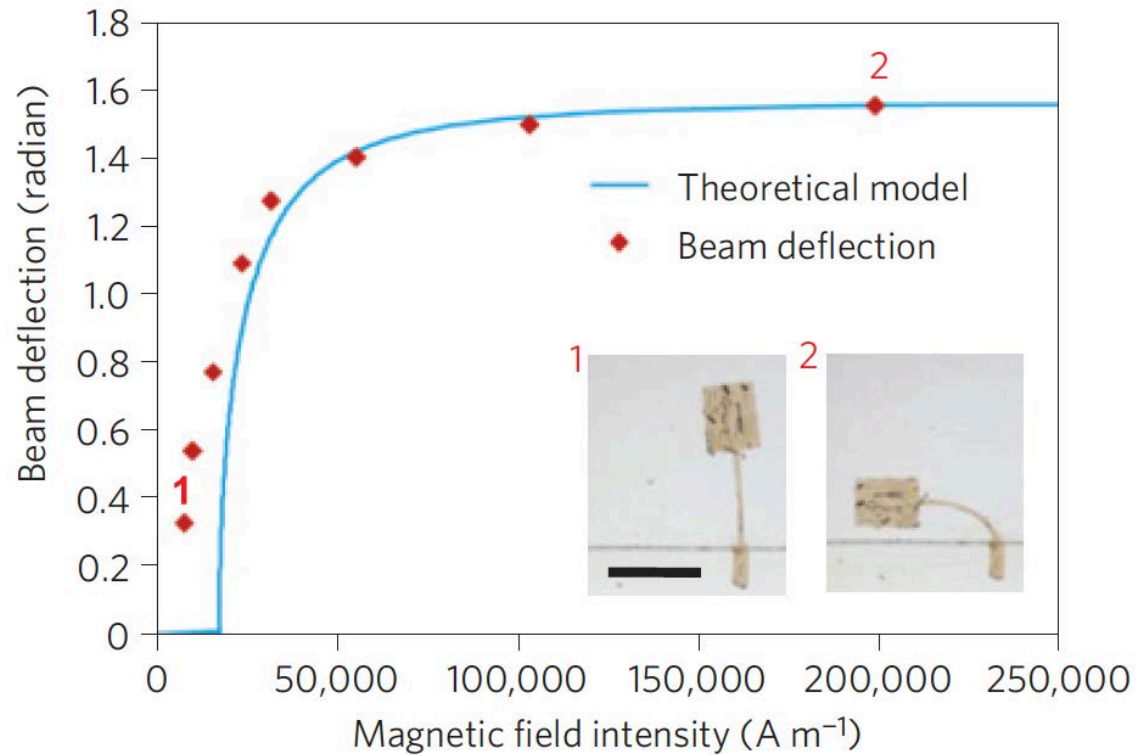
Programming magnetic anisotropy



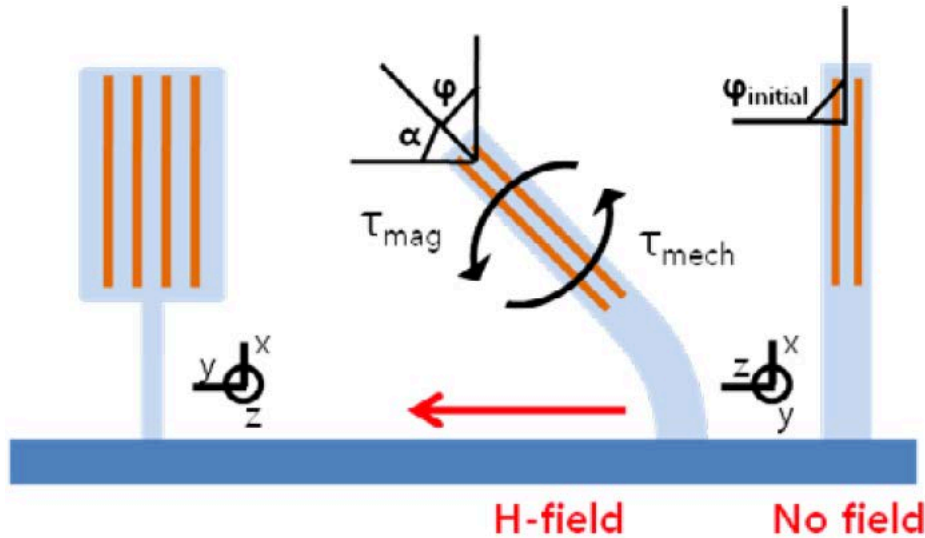
Programming magnetic anisotropy



Magnetic axis



Programming magnetic anisotropy

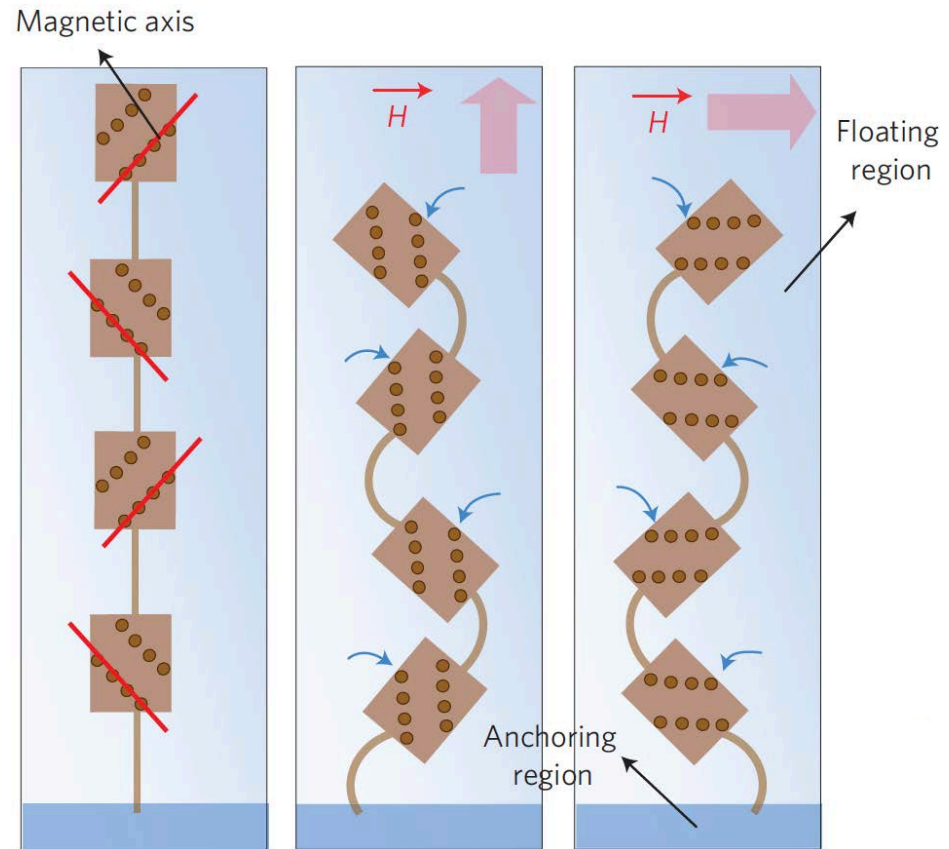
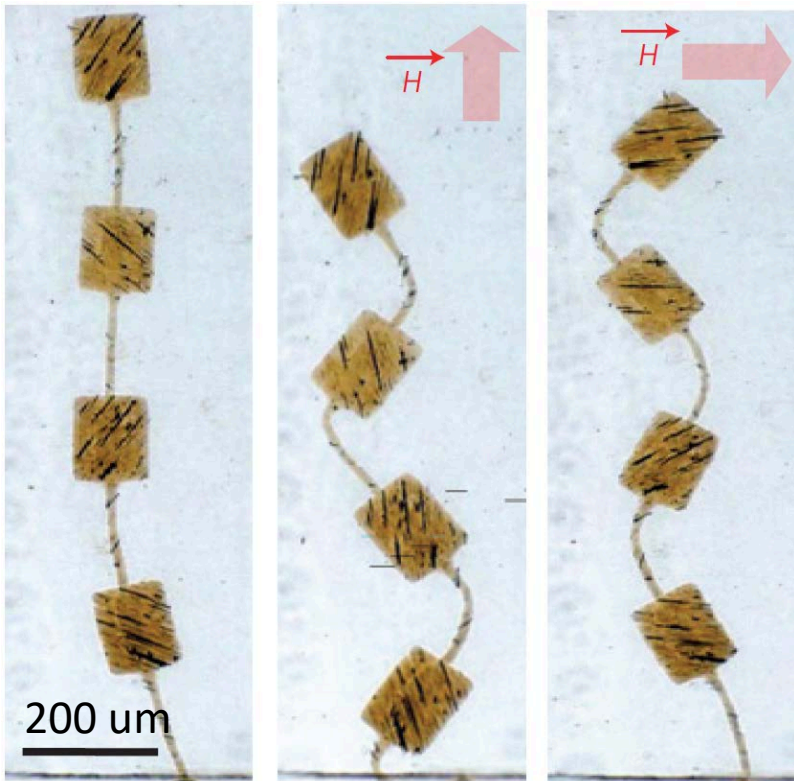
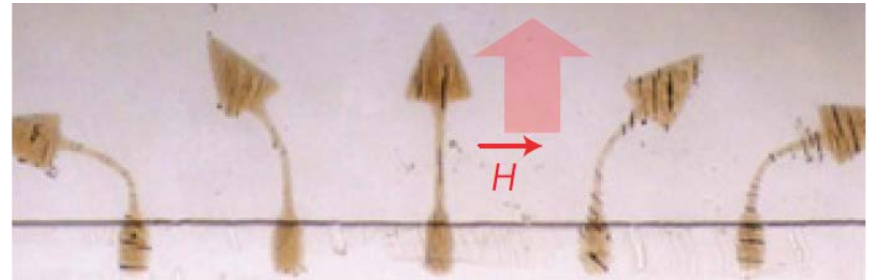
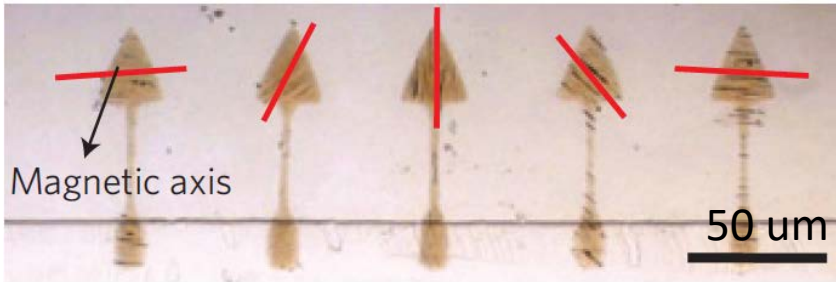


$$\tau_{\text{mechanical}} = -k_{\varphi}\varphi$$

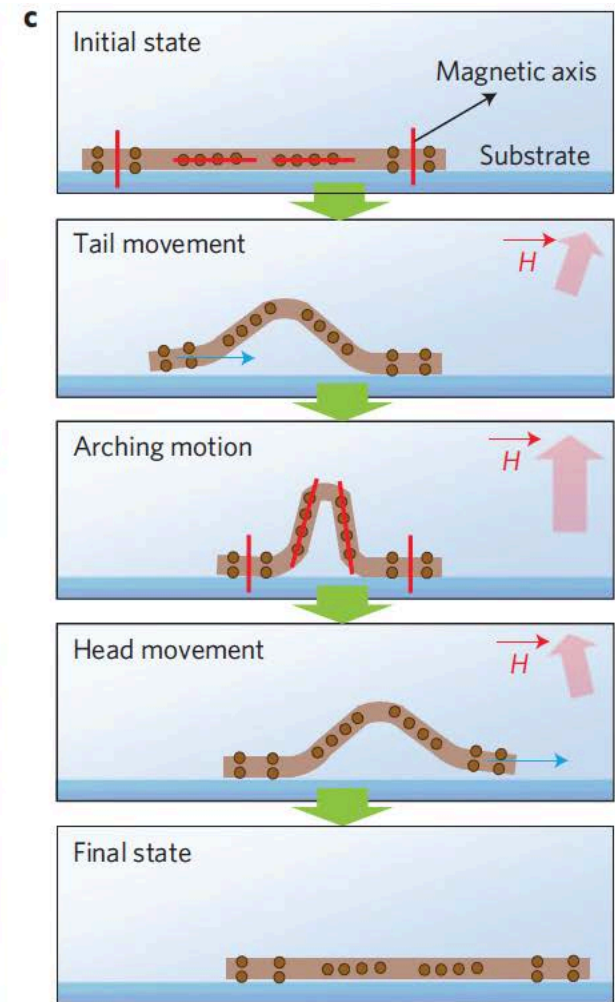
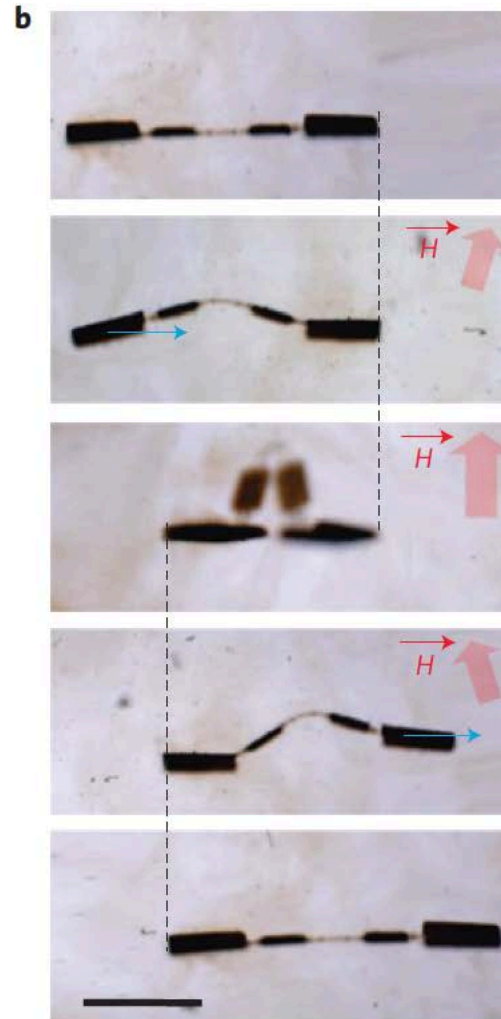
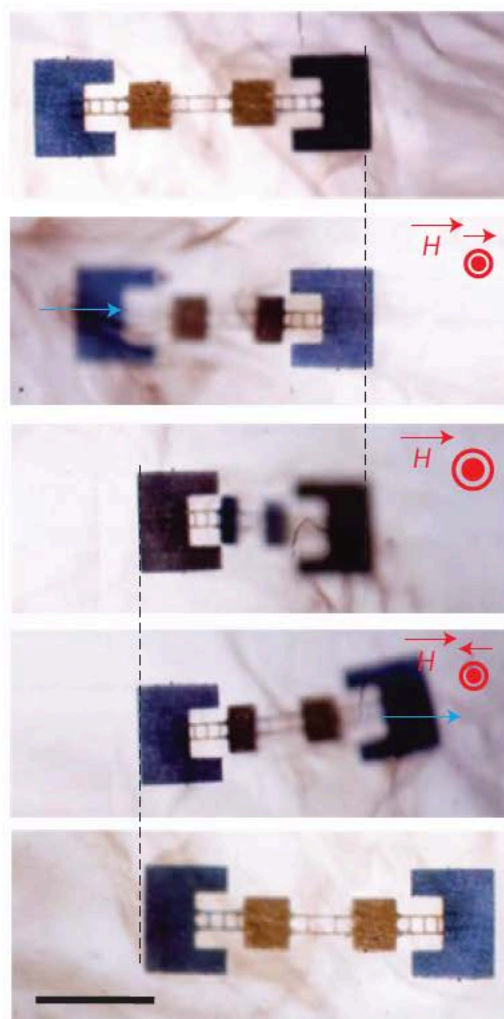
$$k_{\varphi} = \frac{E_y w D^3}{I 12}$$

$$\tau_{\text{magnetic}} = N \frac{3\mu_0 m^2}{4\pi} \sin(2\alpha) \frac{n^2}{d^3} = N \frac{3\mu_0 n^2 \chi^2 R^6 \pi}{4\pi} H^2 \sin(2\alpha)$$

Programming magnetic anisotropy

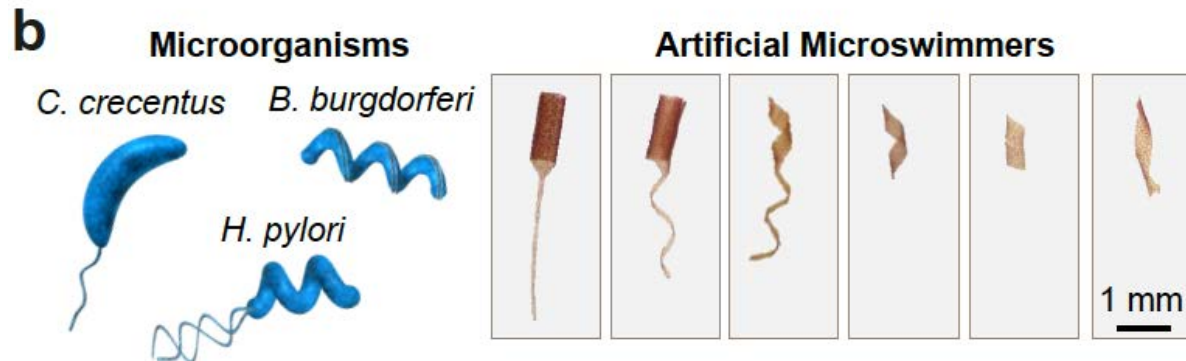
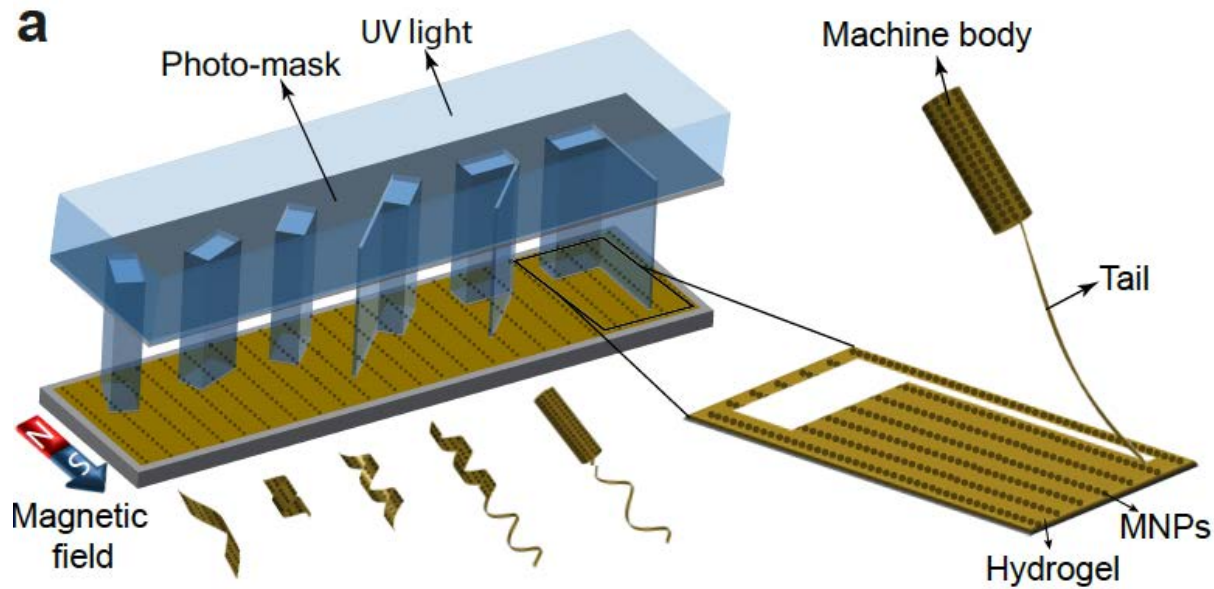


Programming magnetic anisotropy

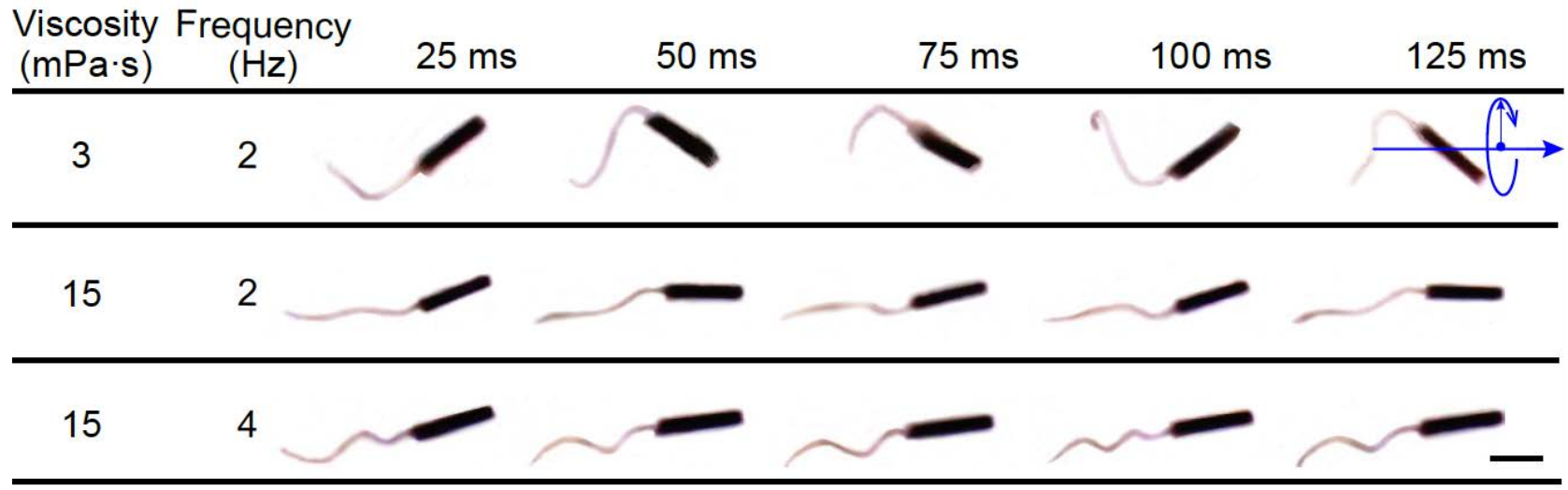


Programmable self-folding

- Differential Swelling via Particle Gradients



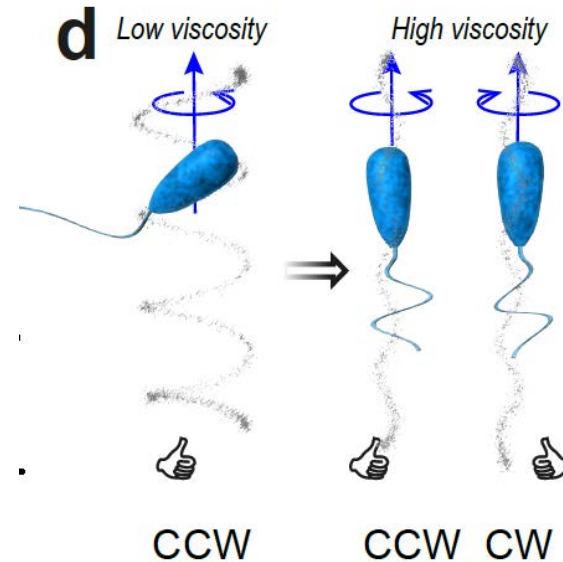
Elastohydrodynamic Coupling



Sperm Number

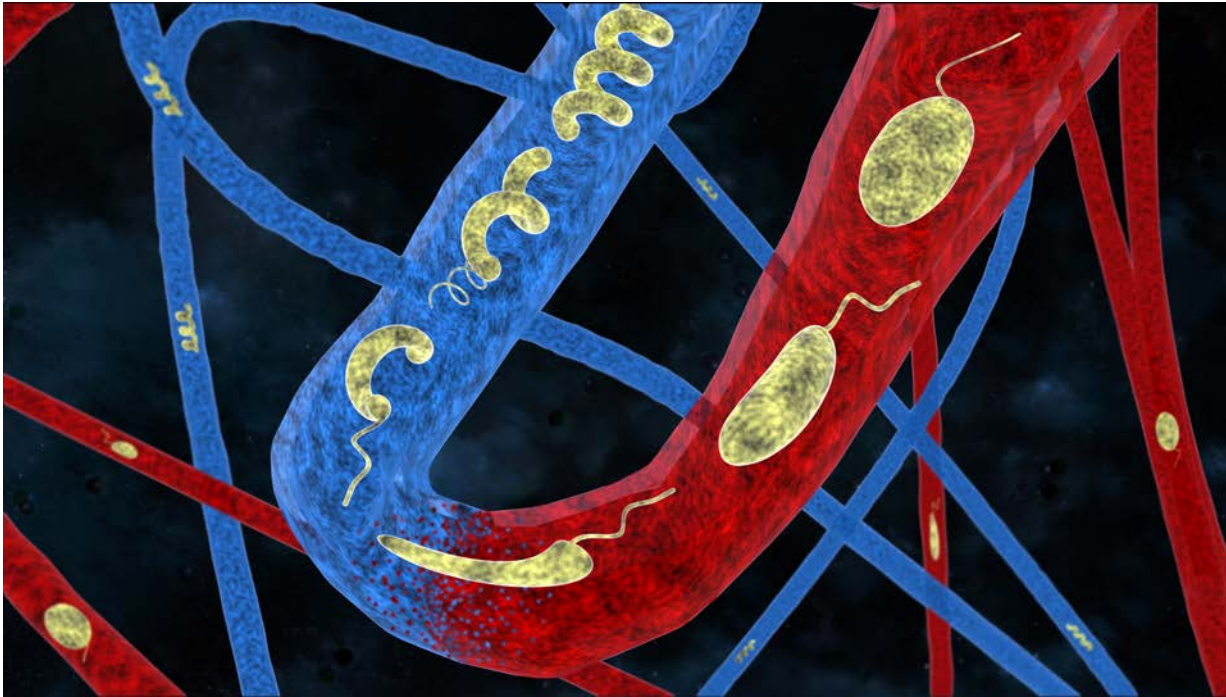
$$S_p = L / \left(\frac{\kappa}{\zeta_{\perp} \omega} \right)^{1/4}$$

Bending rigidity vs viscous drag



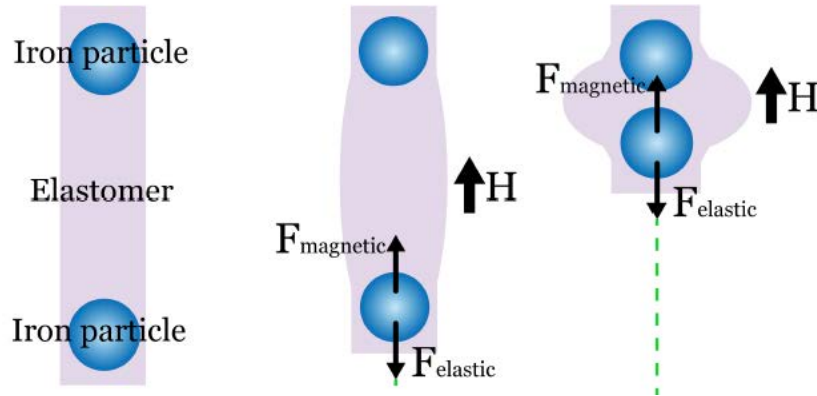
Adaptive Microswimmers

- Shape change induced by viscous drag or osmotic pressure
- Shape shifting as a strategy to tune motility and maneuverability
- Stimuli responsive gels and elastic structures



Magnetoelastic Effect

- Magnetic pull-in instability



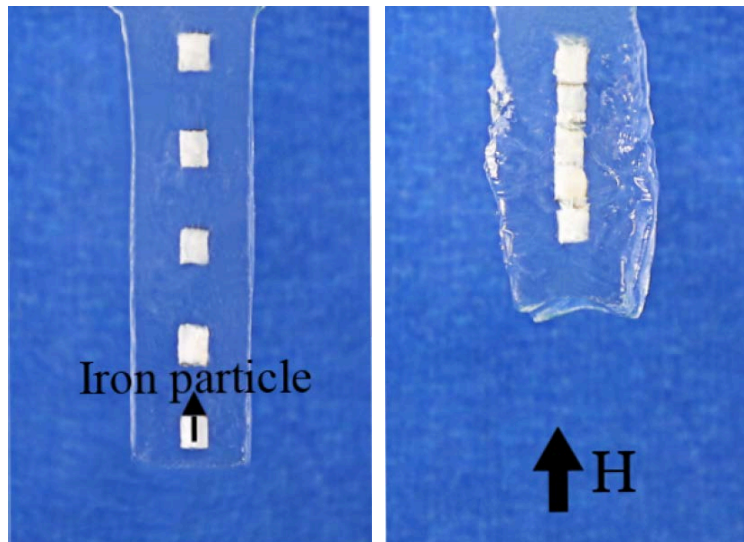
Magnetic Force

$$F_m \approx 3\mu_0 m^2 / (2\pi l^4)$$

$$m = V\chi_m H$$

Elastic Force (neo-Hookean)

$$F_e = A\gamma[l/l_0 - (l/l_0)^{-2}]$$



- Shear modulus of the matrix vs the magnetic Maxwell stress
- Placement of magnetic particles is the key

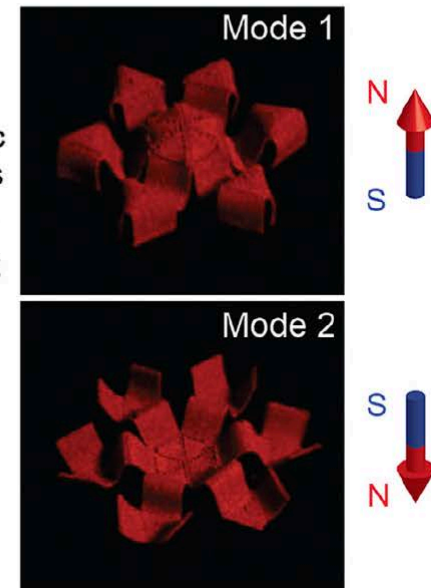
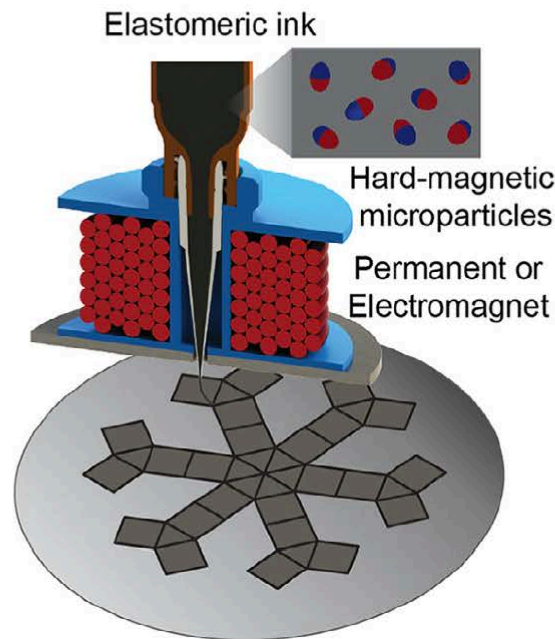
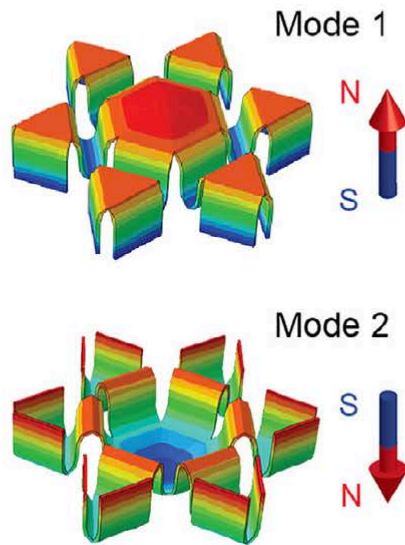
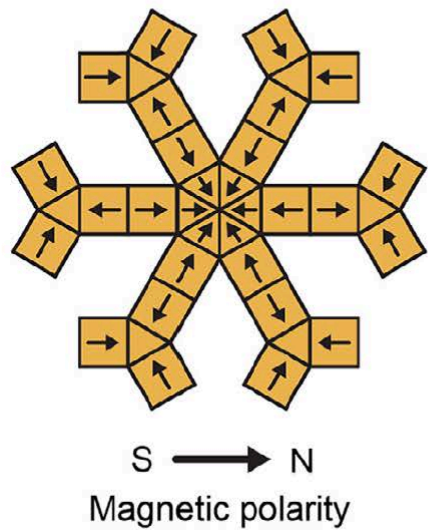
Hard Magnetic Composites

- Particles of high-coercivity ferromagnetic materials
 - Hard magnetic materials
 - such as NdFeB
- High remnant characteristics allow them to retain high residual magnetic flux density even in the absence of magnetic fields after saturation (high magnetization at low field)
- High coercivity helps them sustain high residual magnetic flux density over a wide range of applied magnetic fields below the coercive field strength (hard to demagnetize or re-magnetize)

Hard Magnetic Composites

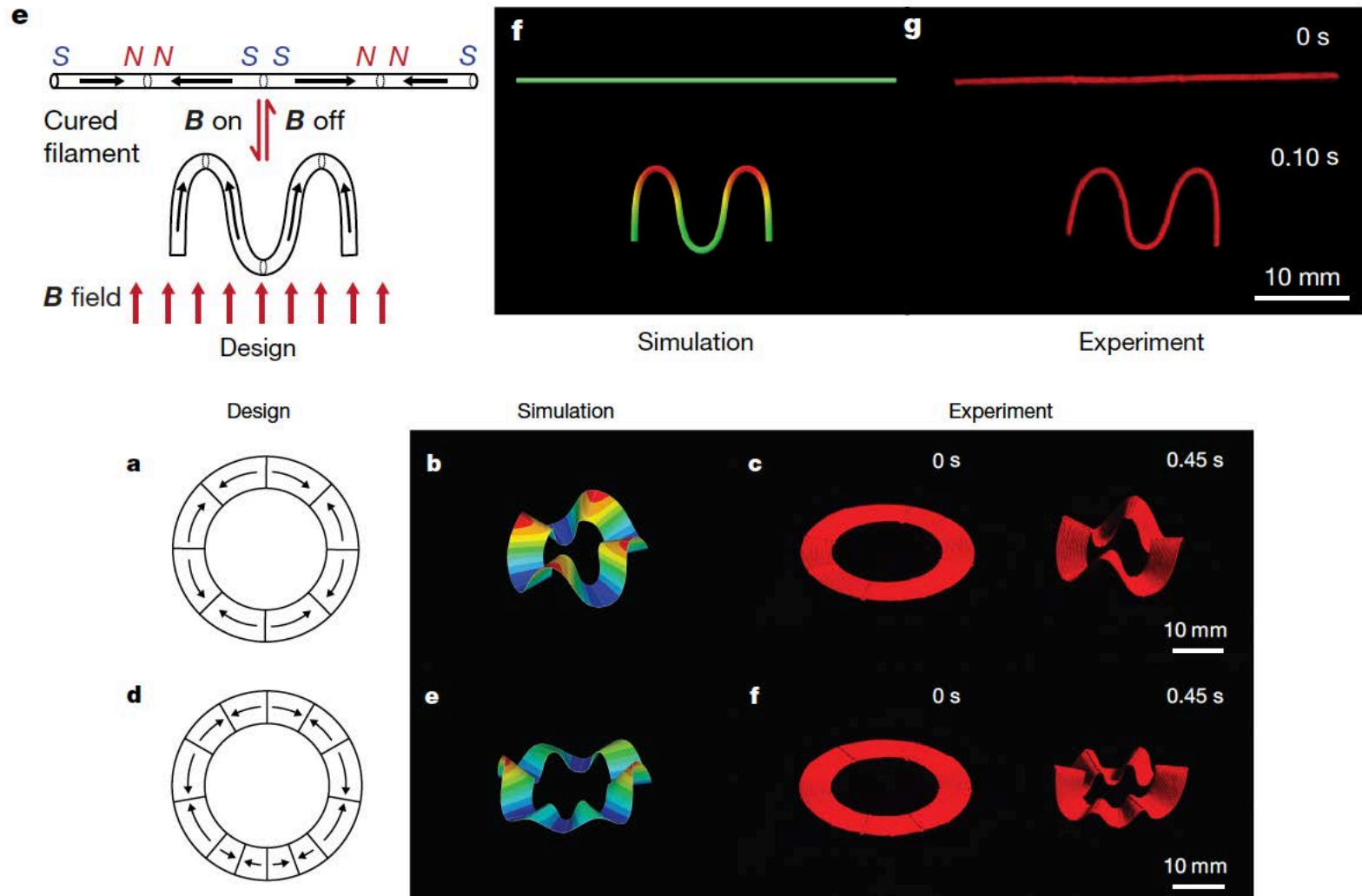
- Design of ferromagnetic domains in 3D printed soft materials

Design → Model-based Simulation → Fabrication (3D Printing) → Experiment

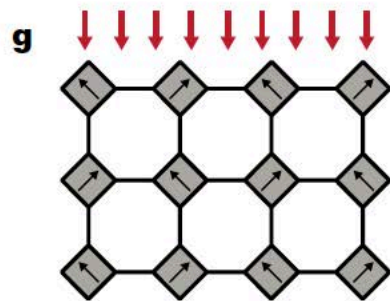
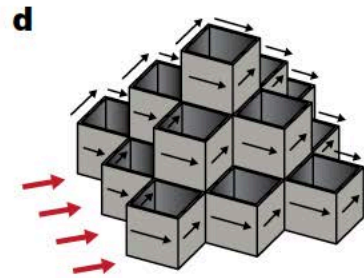
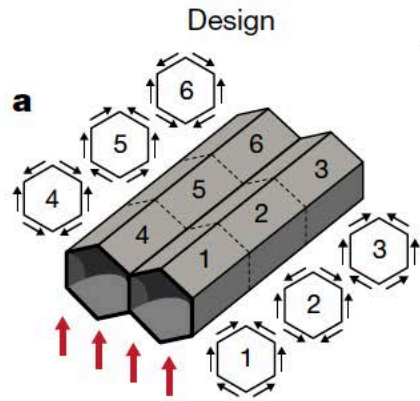


Hard Magnetic Composites

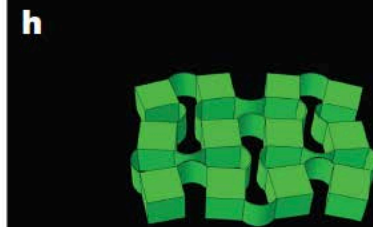
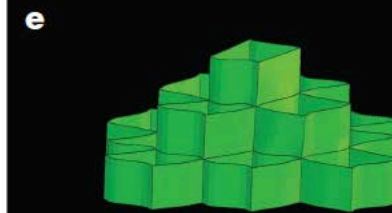
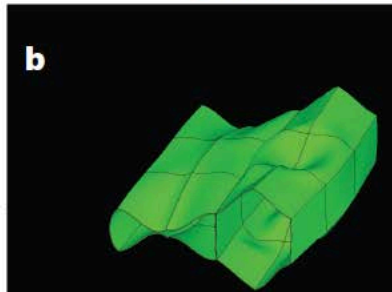
movie



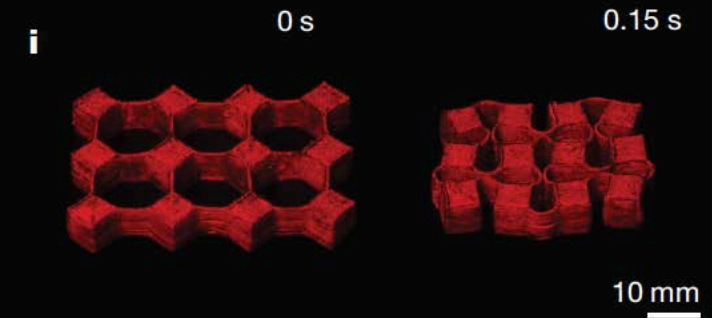
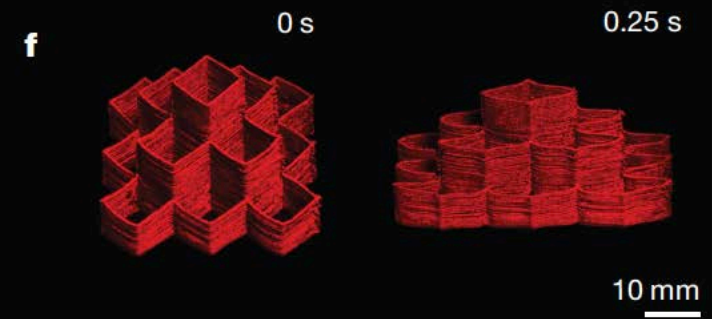
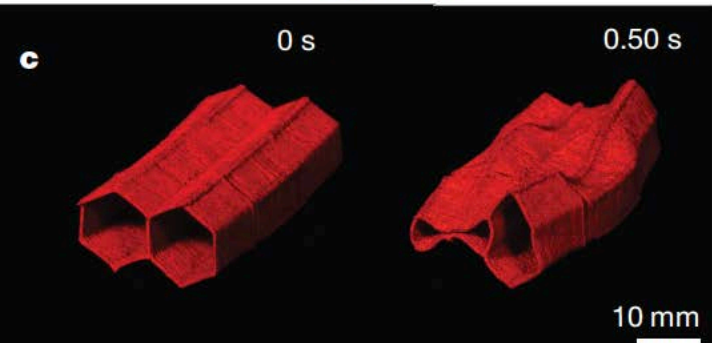
Hard Magnetic Composites



Simulation



Experiment



Printing ferromagnetic domains for untethered fast-transforming soft materials

Yoonho Kim^{1,2*}, Hyunwoo Yuk^{1*}, Ruike Zhao^{1*}, Shawn A. Chester³, Xuanhe Zhao^{1,4}

¹*Soft Active Materials Laboratory, Department of Mechanical Engineering, Massachusetts Institute of Technology*

²*Harvard-MIT Division of Health Sciences and Technology, Massachusetts Institute of Technology*

³*Department of Mechanical and Industrial Engineering, New Jersey Institute of Technology*

⁴*Department of Civil and Environmental Engineering, Massachusetts Institute of Technology*

*These authors contributed equally to the current work

Correspondence should be addressed to Xuanhe Zhao (zhaox@mit.edu)

Overall printing process and actuation of a shape-morphing structure with programmed ferromagnetic domains



Printing ferromagnetic domains for untethered fast-transforming soft materials

Yoonho Kim^{1,2*}, Hyunwoo Yuk^{1*}, Ruike Zhao^{1*}, Shawn A. Chester³, Xuanhe Zhao^{1,4}

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*These authors contributed equally to the current work

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Fast transformation of a set of 2D structures into complex 3D shapes under applied magnetic fields



Printing ferromagnetic domains for untethered fast-transforming soft materials

Yoonho Kim^{1,2*}, Hyunwoo Yuk^{1*}, Ruike Zhao^{1*}, Shawn A. Chester³, Xuanhe Zhao^{1,4}

¹*Soft Active Materials Laboratory, Department of Mechanical Engineering, Massachusetts Institute of Technology*

²*Harvard-MIT Division of Health Sciences and Technology, Massachusetts Institute of Technology*

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⁴*Department of Civil and Environmental Engineering, Massachusetts Institute of Technology*

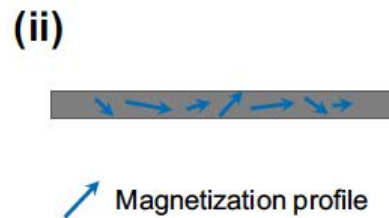
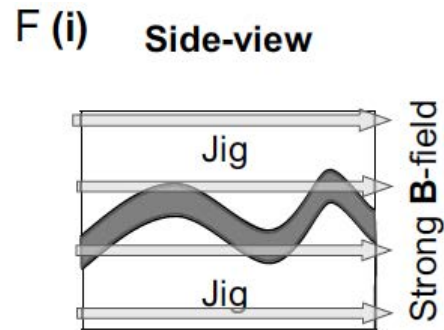
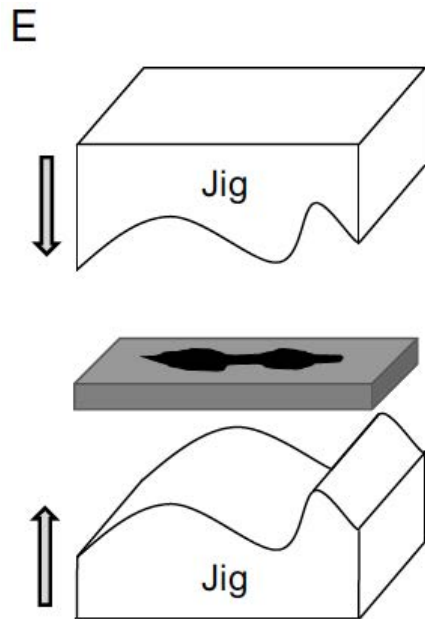
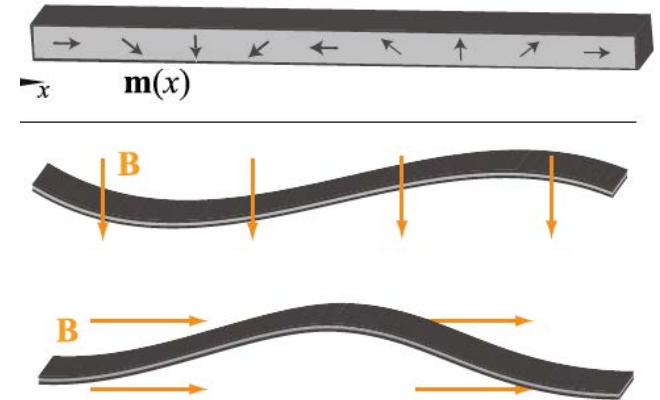
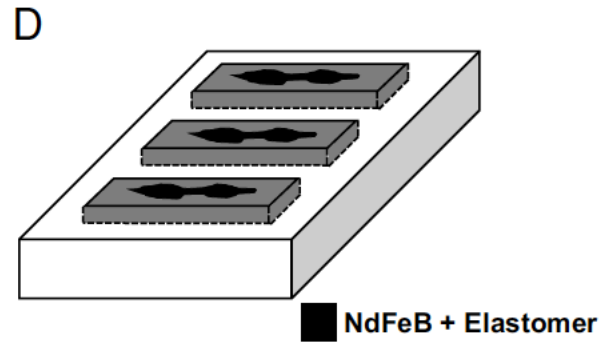
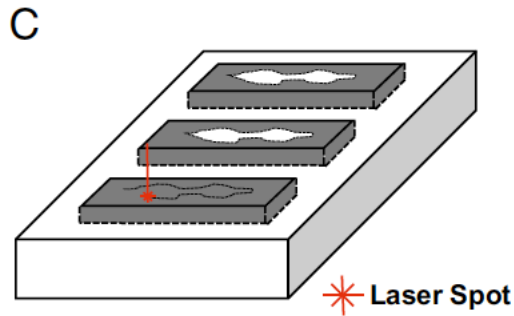
*These authors contributed equally to the current work

Correspondence should be addressed to Xuanhe Zhao (zhaox@mit.edu)

Rolling-based locomotion and delivery of a drug pill of the hexapedal structure under a rotating magnetic field



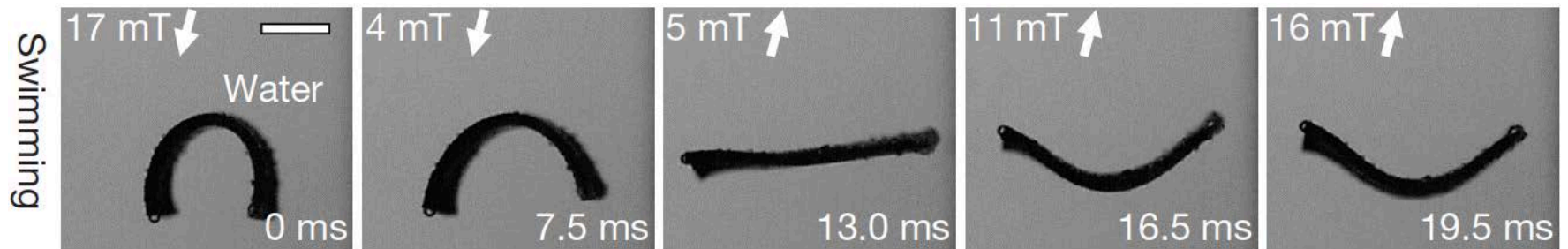
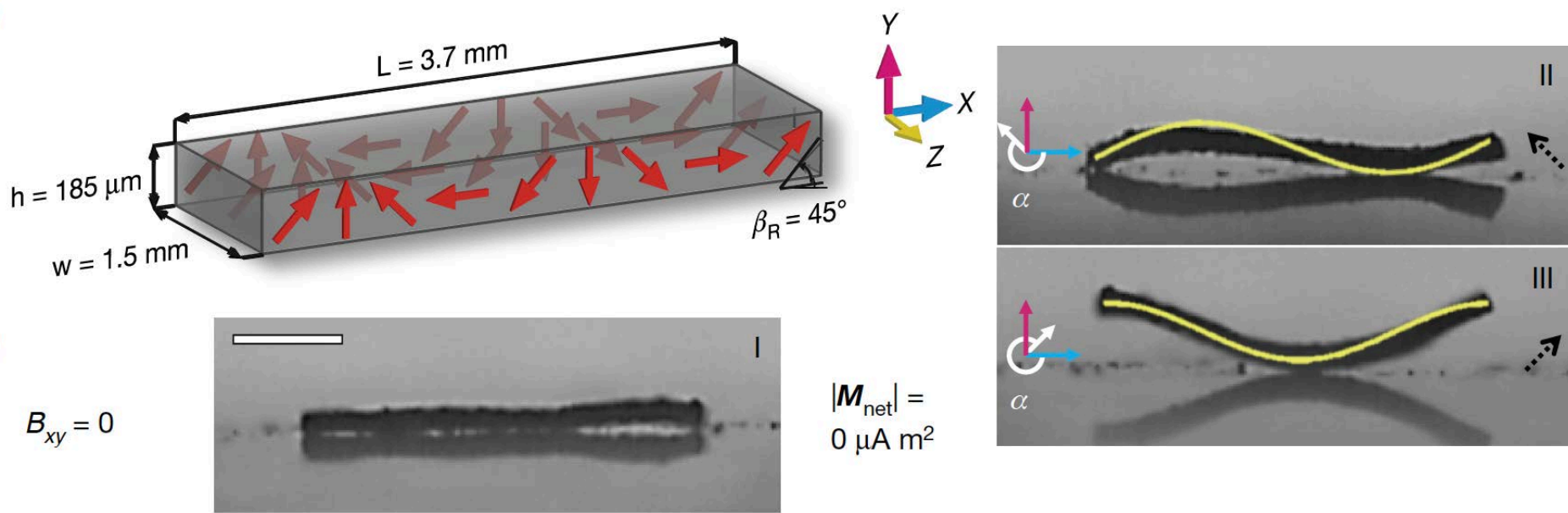
Shape-programmable magnetic soft matter



$$b = \frac{MA\lambda^3}{8\pi^3 EI} B$$

Shape-programmable magnetic soft matter

→ m \Rightarrow B $\cdots \Rightarrow$ M_{net} — Model-predicted deflection



- Intelligence on the external control signal

Small-scale soft-bodied robot with multimodal locomotion

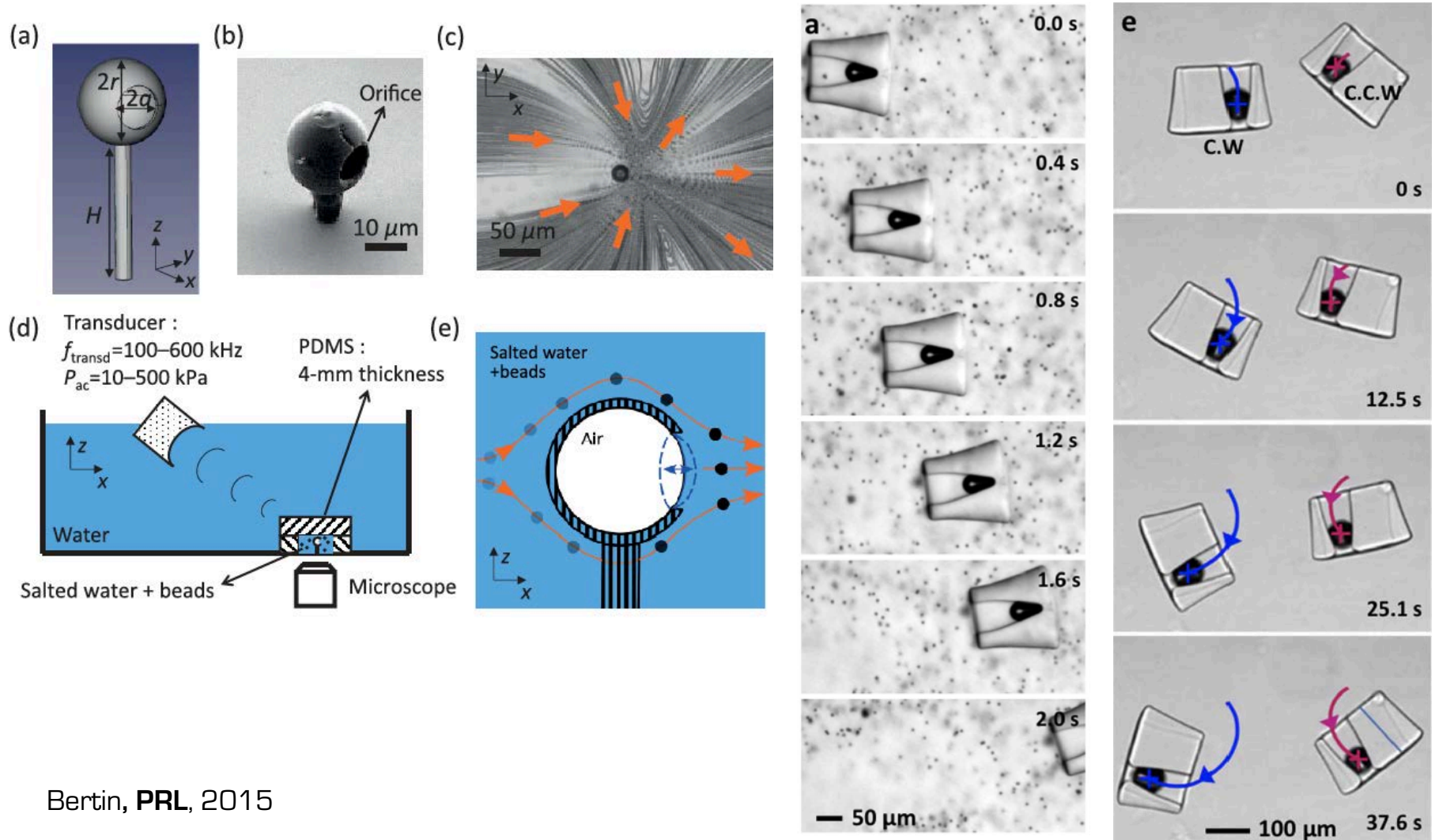
Wenqi Hu, Guo Zhan Lum, Massimo Mastrangeli, Metin Sitti

Multimodal locomotion

(Play speed is indexed to real time)

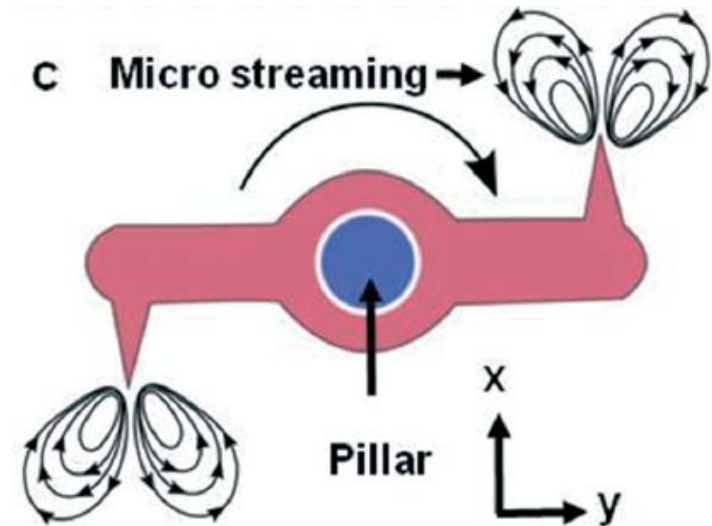
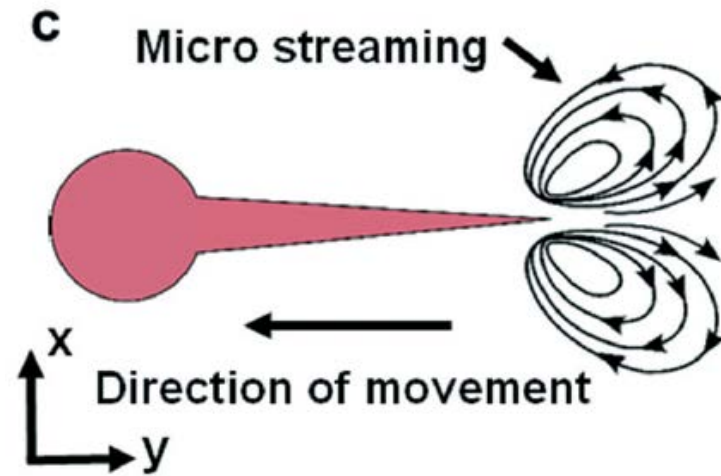
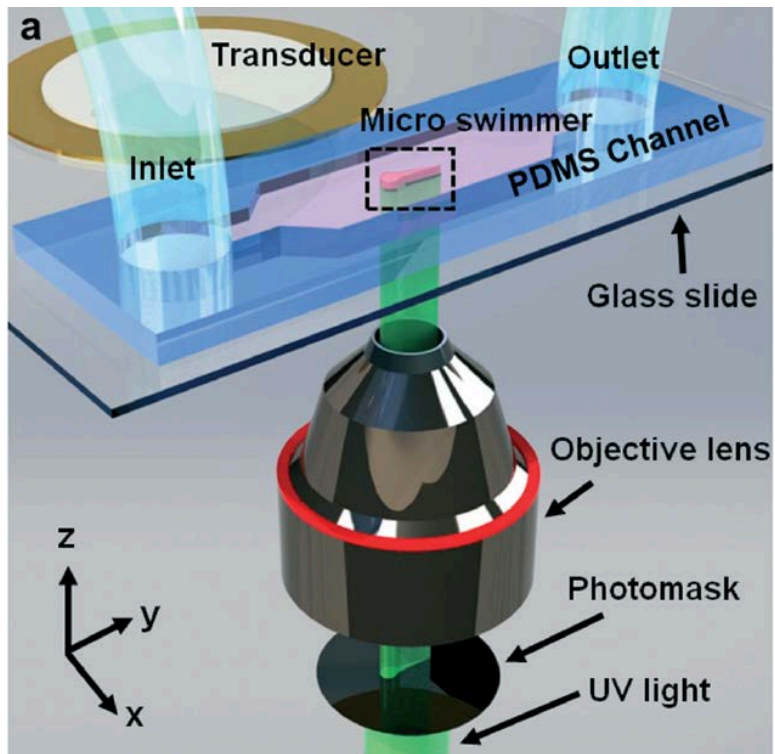


Acoustofluidic Actuation



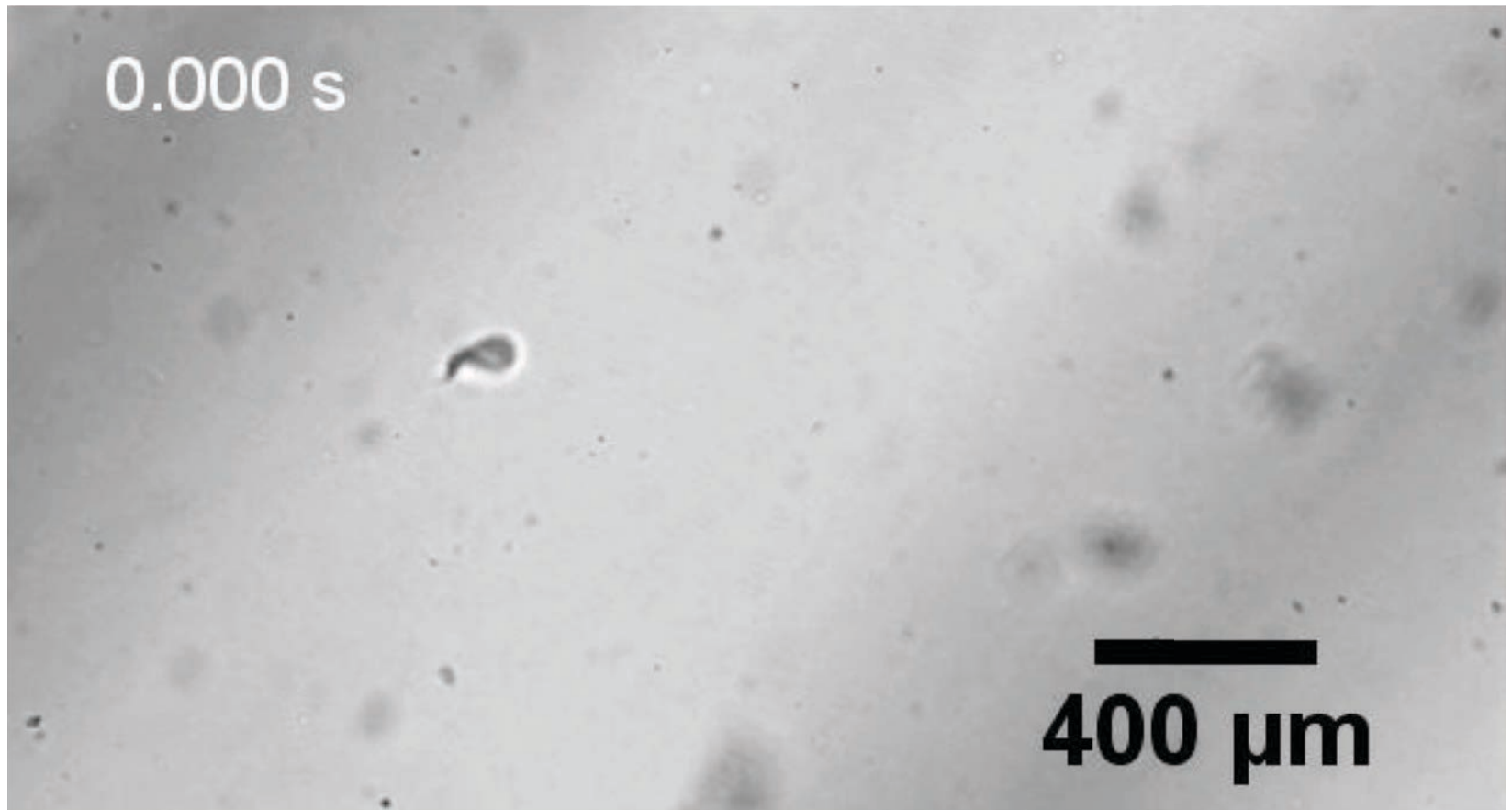
Bertin, **PRL**, 2015

Acoustofluidic Actuation

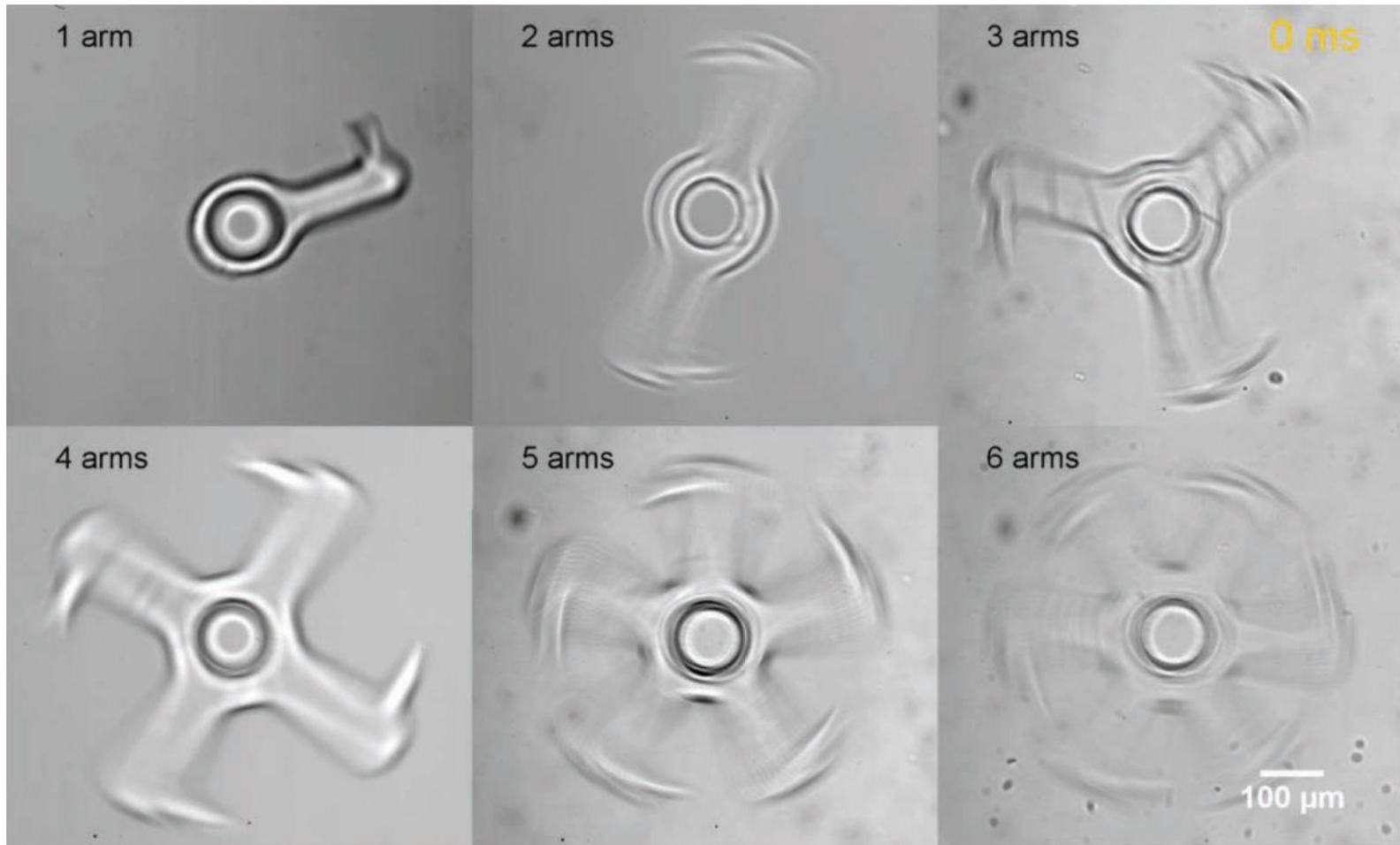


Kaynak, *Lab Chip*, 2016

Acoustofluidic Actuation



Acoustofluidic Actuation

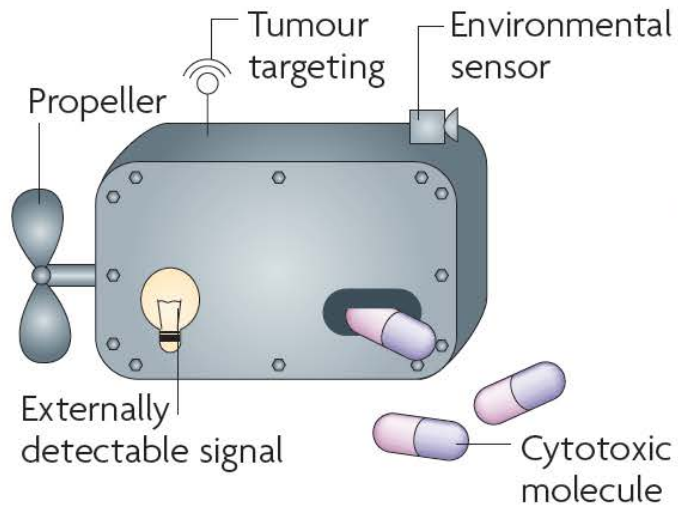


Biological Actuators

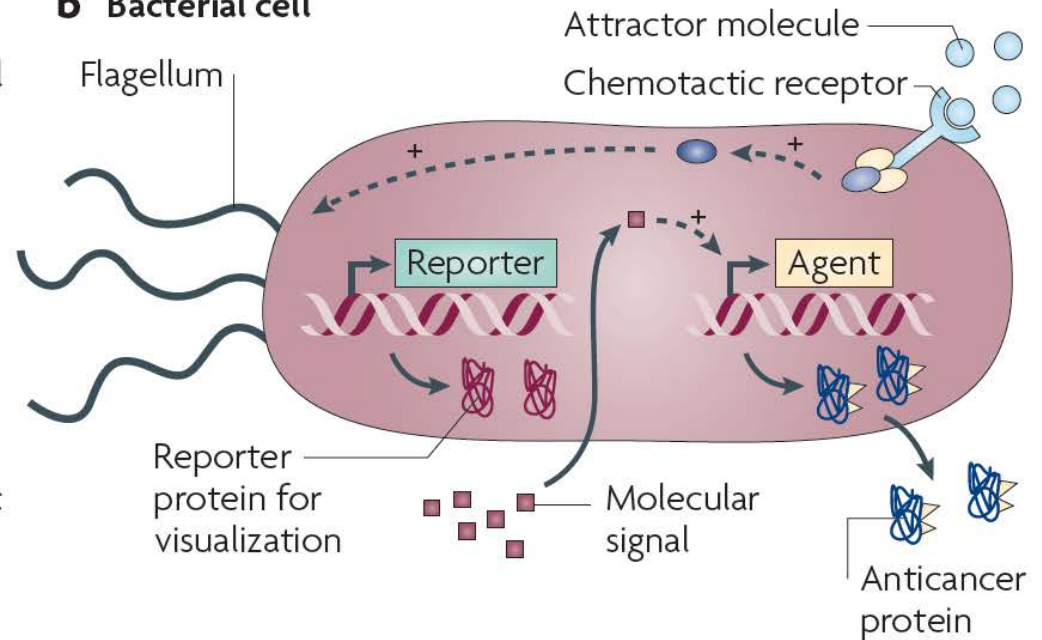
- Sensing-computation-actuation seems to be impossible to reach at microscale
- Microorganisms and immune cells already access everywhere in the body
- We can engineer cells thanks to genetic engineering
- We may even build minimal cells (designer cells) or artificial cells
- Engineering with life may teach us more about the anatomy and physiology

Ideal Prototype

a Robot factory



b Bacterial cell



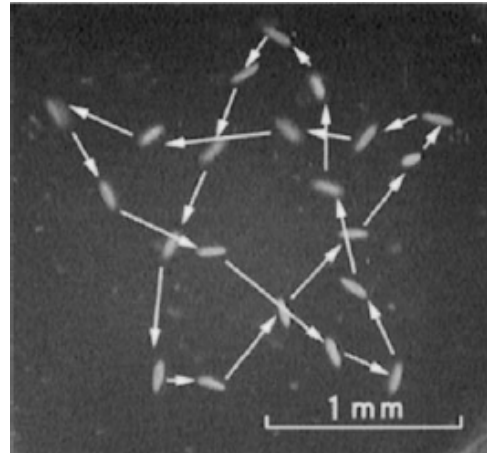
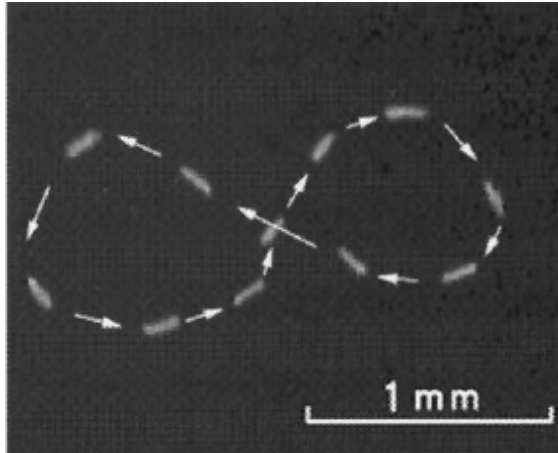
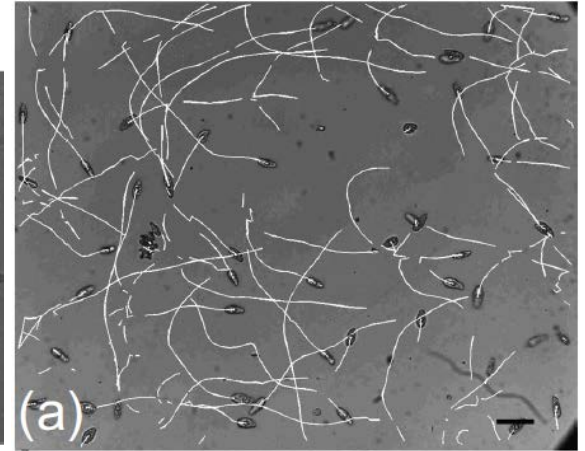
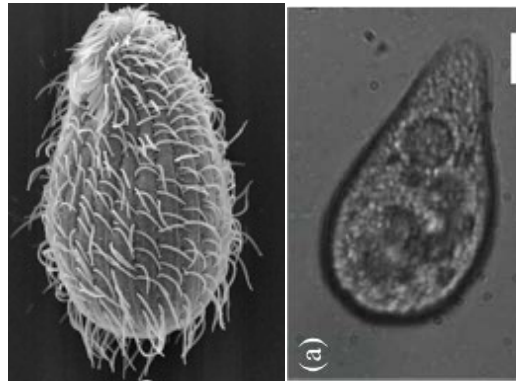
Forbes, *Nat Rev Cancer*, 2011

Galvanotactic Control of Ciliate Protozoa

Paramecium caudatum



Tetrahymena pyriformis

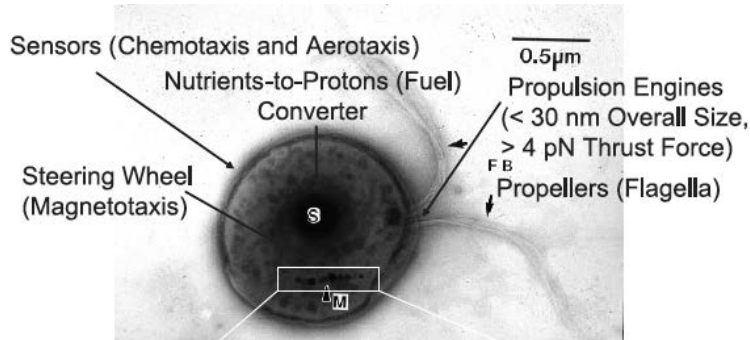


Itoh, *Trans Mech*, 2000

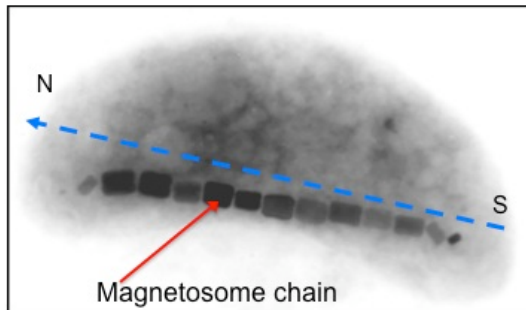
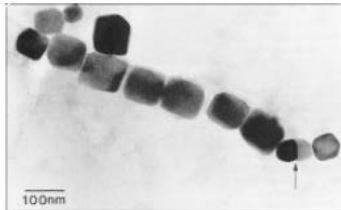
Kim, *APL*, 2009

Magnetotactic Bacteria

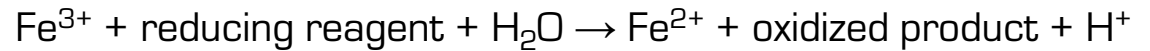
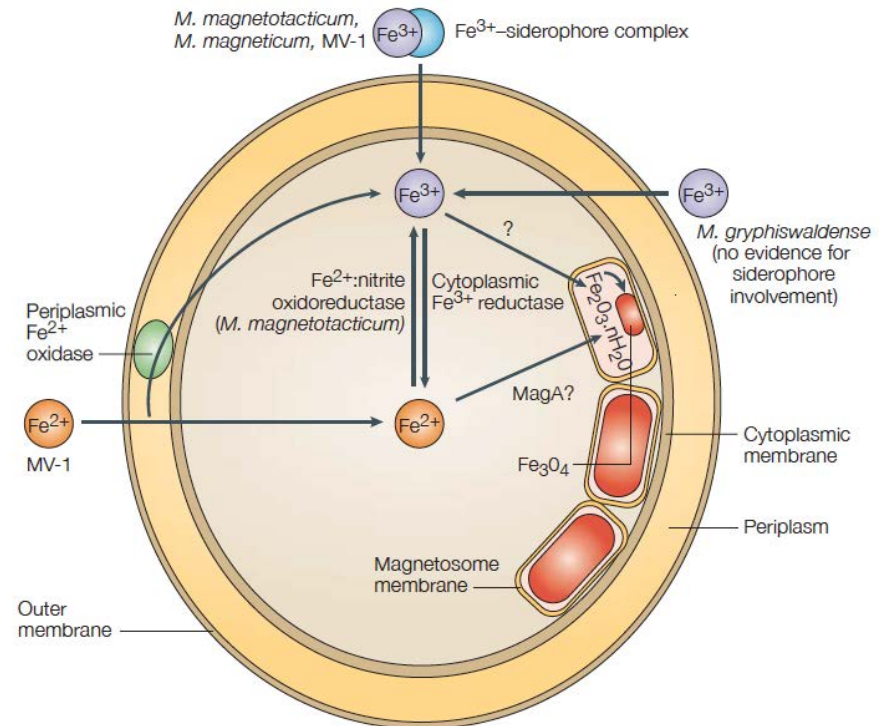
VIDEO



MC-1

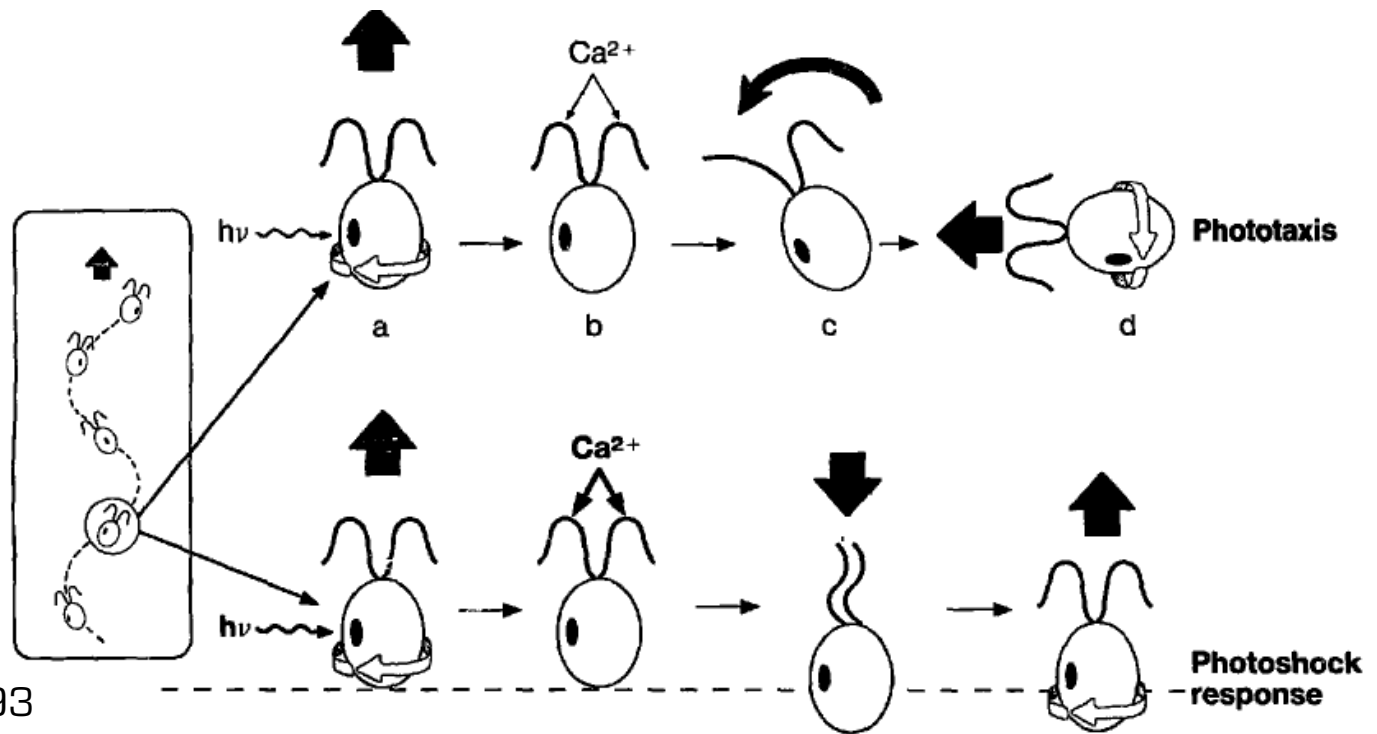
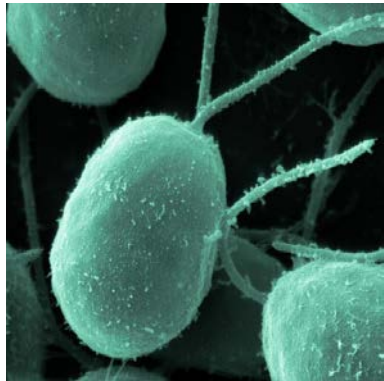
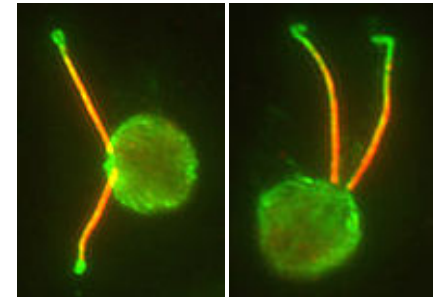
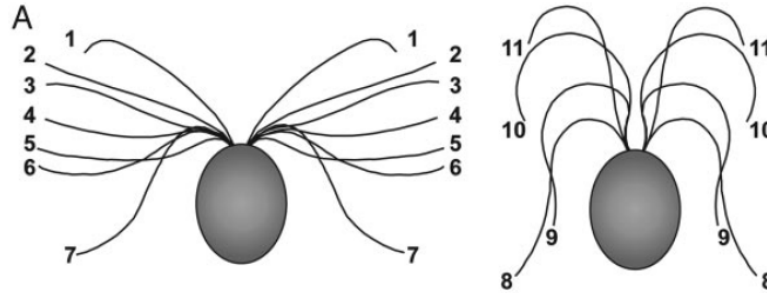
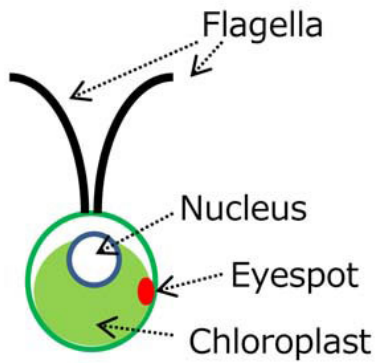


Synthesis in anaerobic conditions



Martel, *IJRR*, 2009 Frankel, *Nat Rev*, 2004

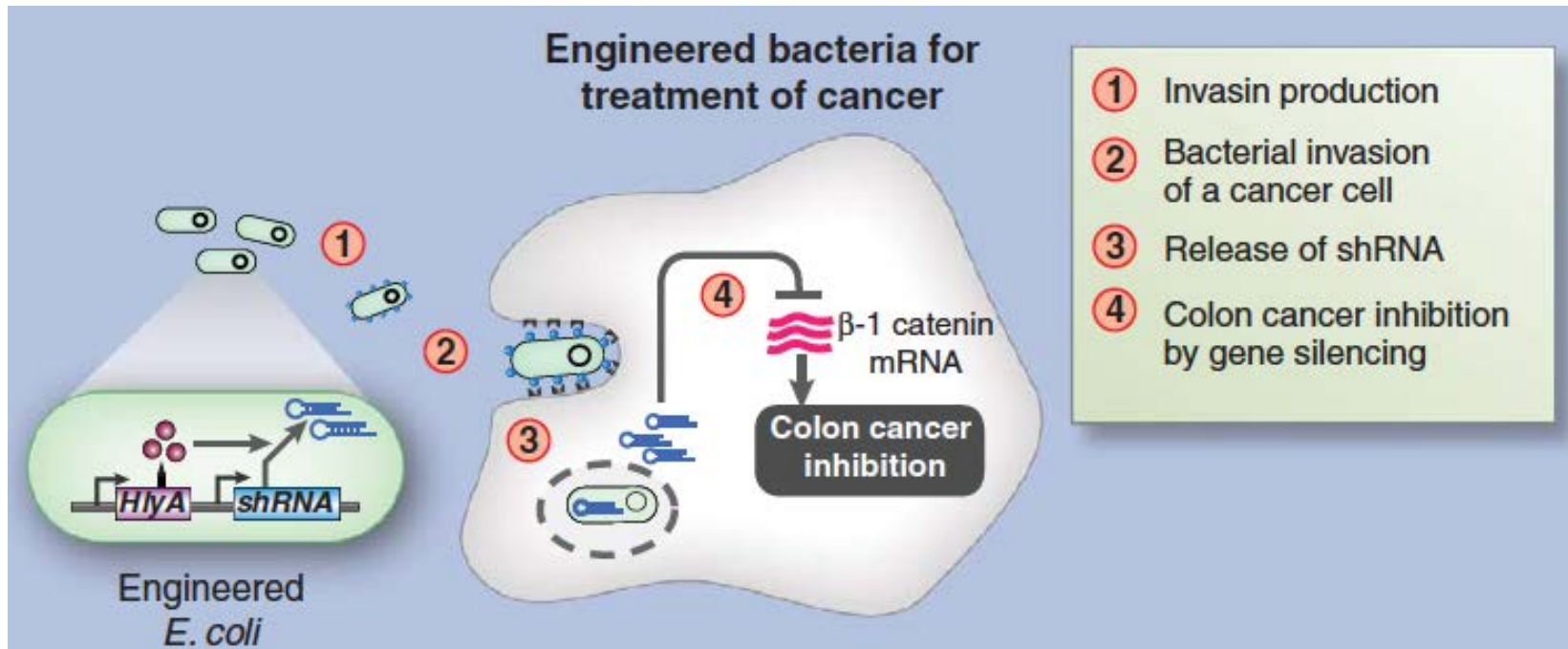
Phototaxis to Steer *Chlamydomonas reinhardtii*



Witman, T Cell Bio, 1993

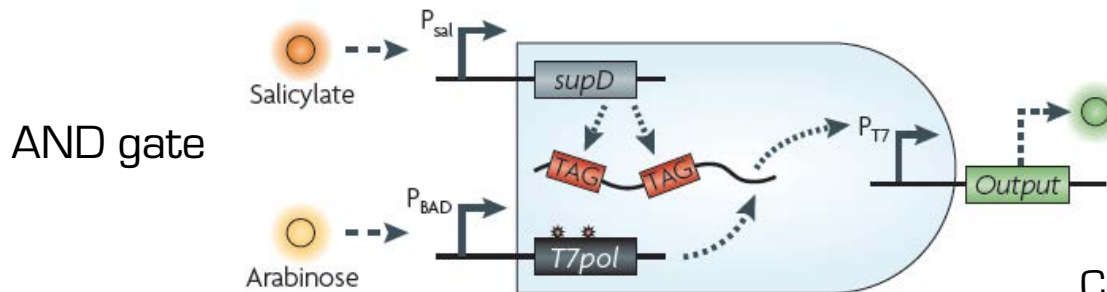
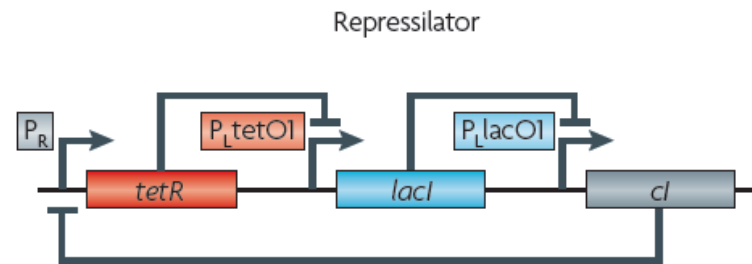
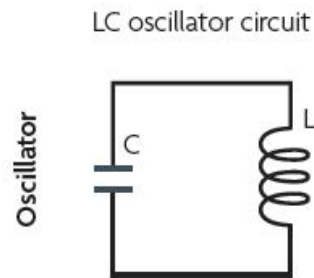
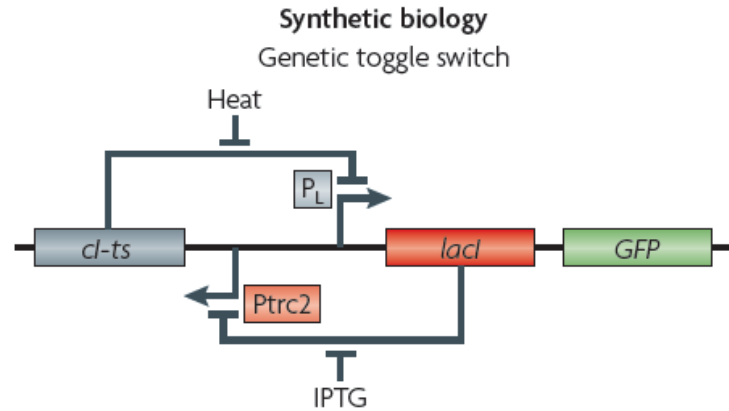
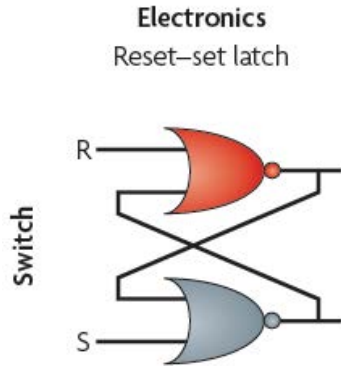
Release of Therapeutic Agents

- Detection of cancer cells and/or tumor microenvironment
- Triggered production and release of proteins and nucleic acids



Ruder, *Science*, 2011

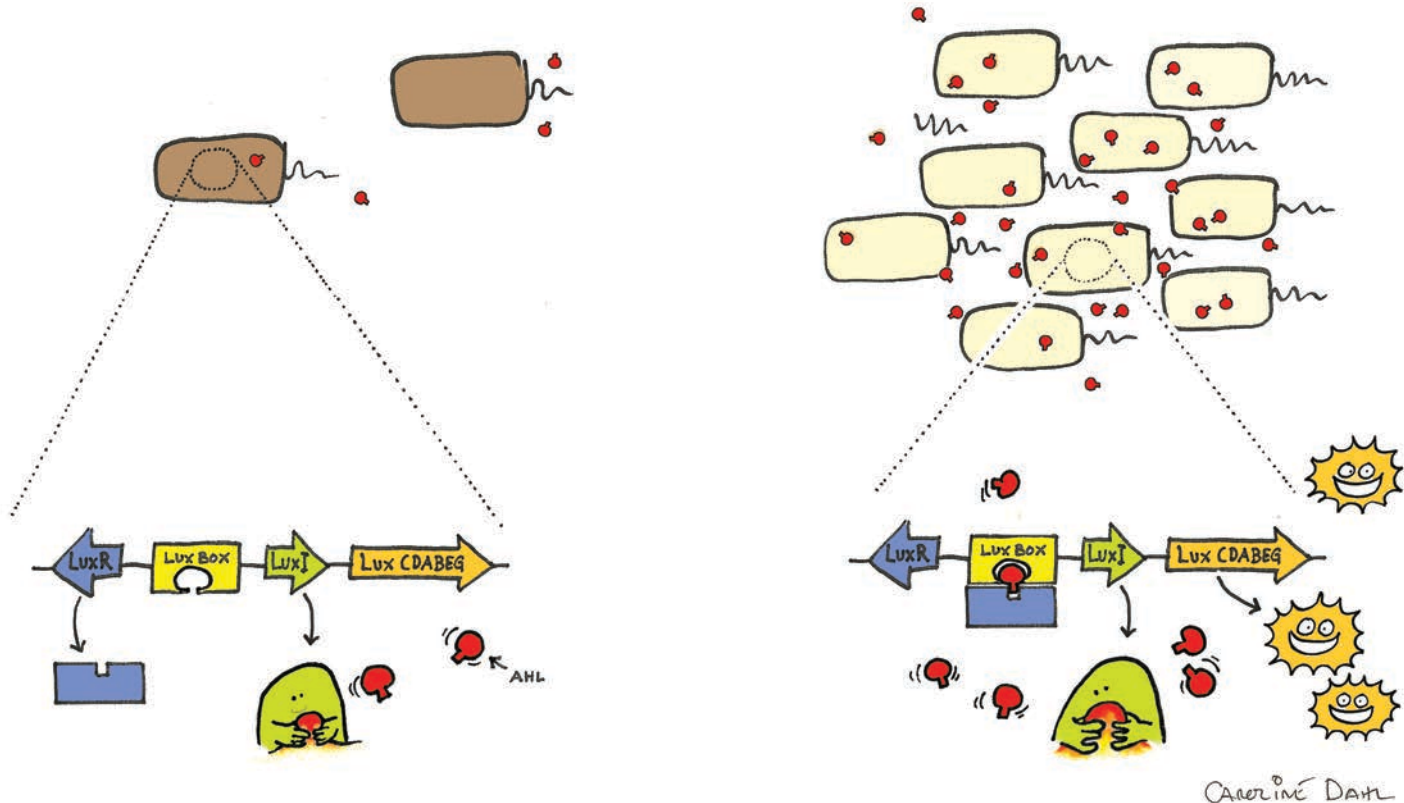
Logic Gates and Circuits



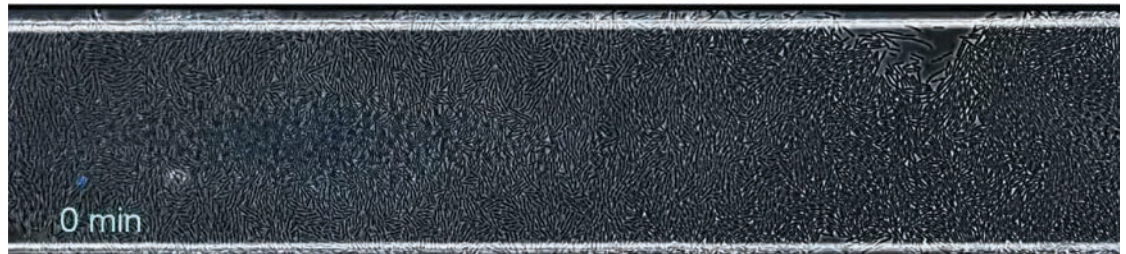
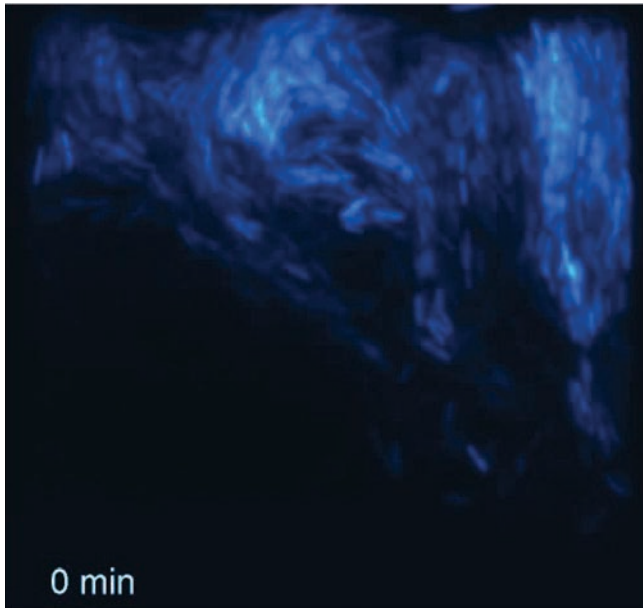
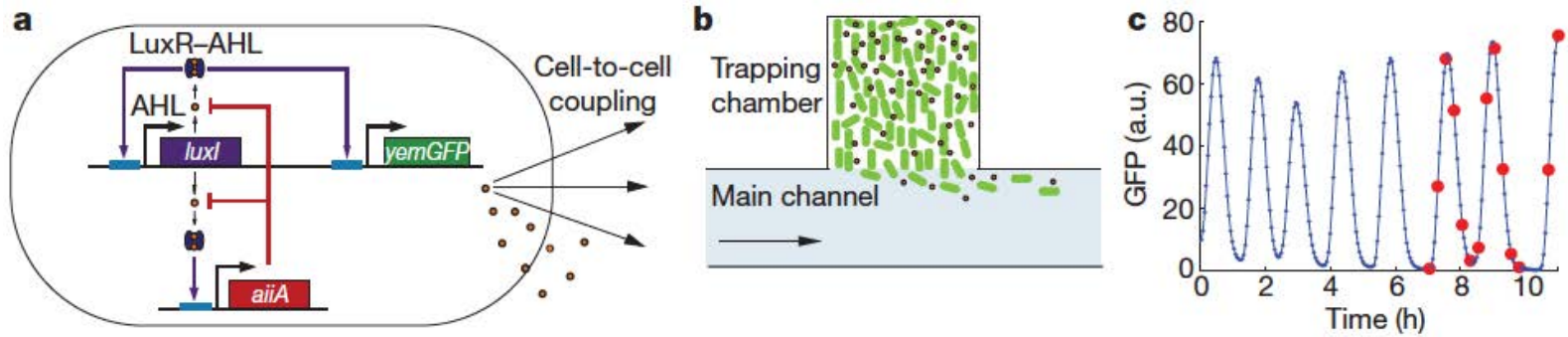
Collins, *Nat Rev Gen*, 2010

Quorum Sensing

- Produce and release an autoinducer (AHL)
- Bacteria regulate virulence, competence, antibiotic production, motility, biofilm formation etc. using quorum sensing



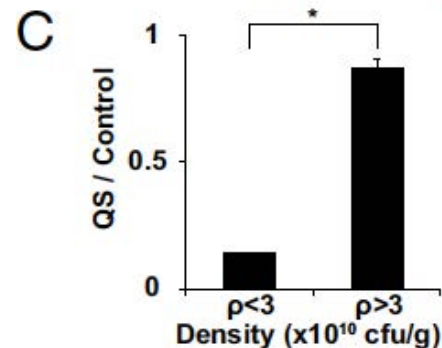
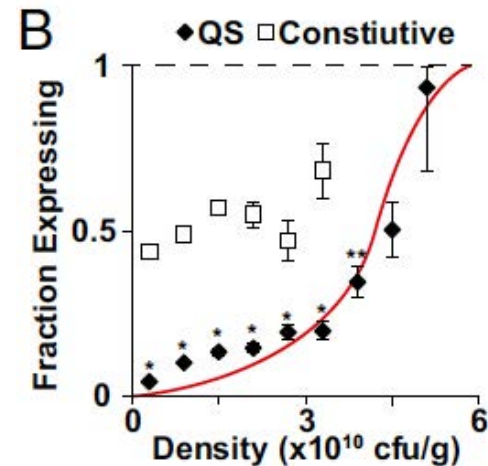
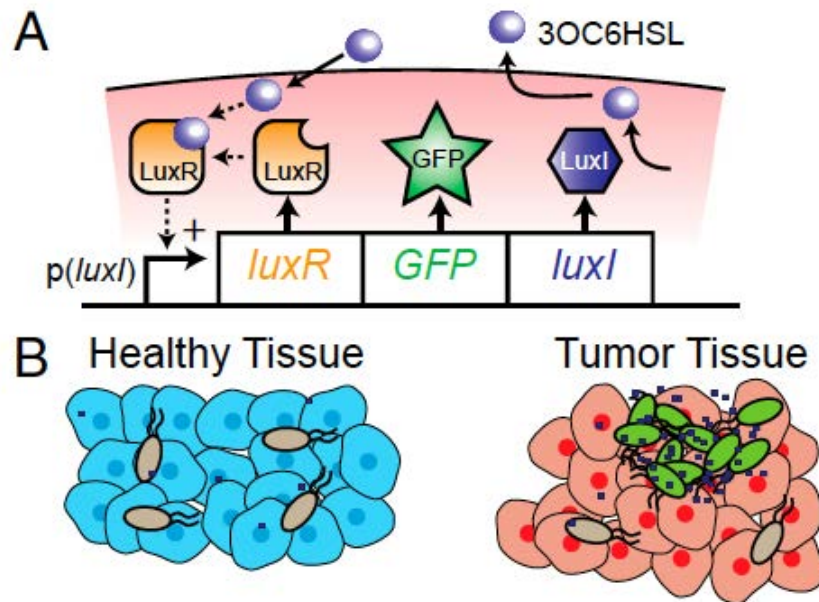
A synchronized quorum of genetic clocks



Danino, *Nature*, 2010

Selective protein expression within tumors

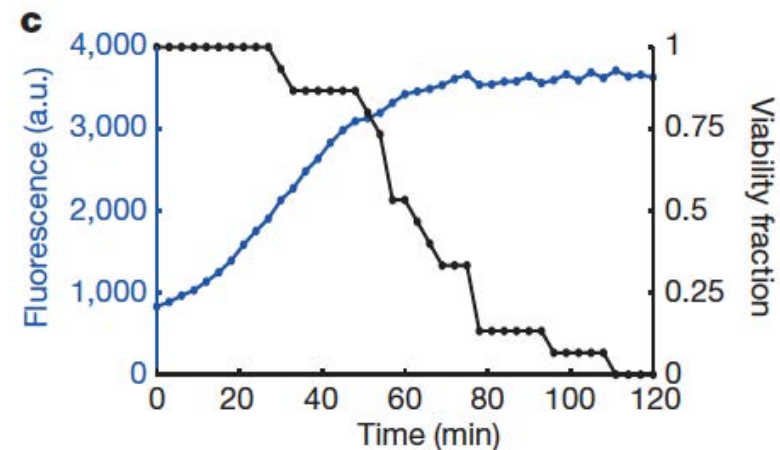
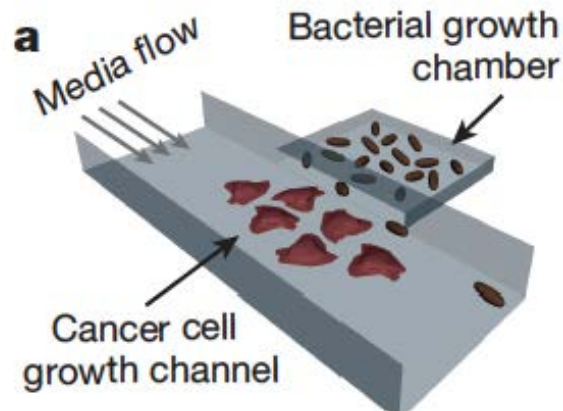
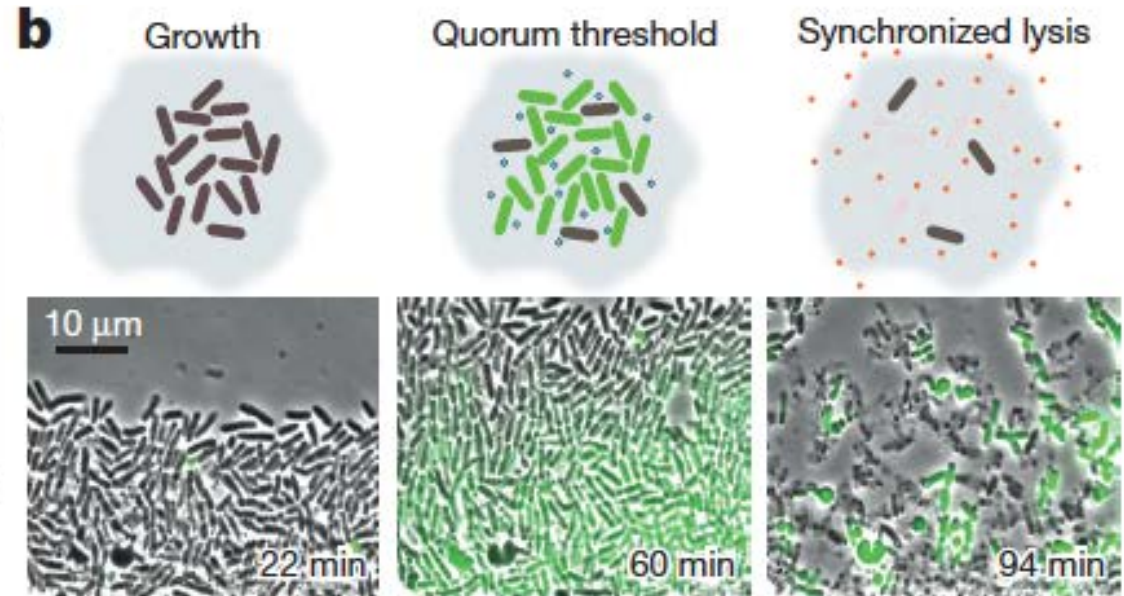
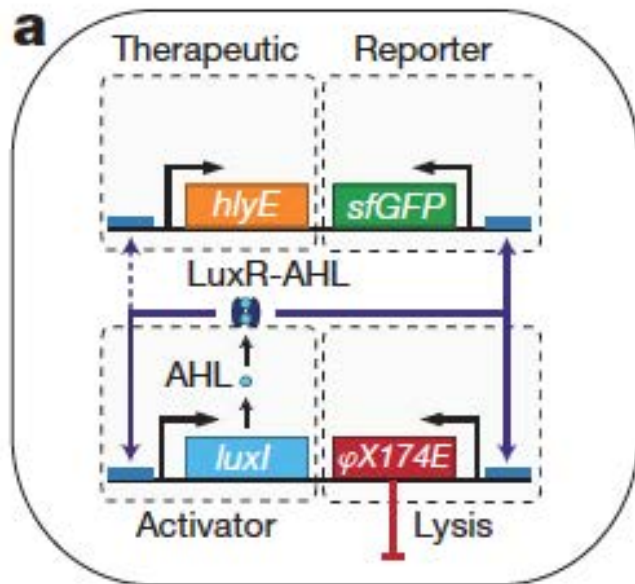
- Salmonella is engineered to produce anticancer proteins only in tightly packed colonies
- Lux quorum sensing system from *Vibrio fischeri*



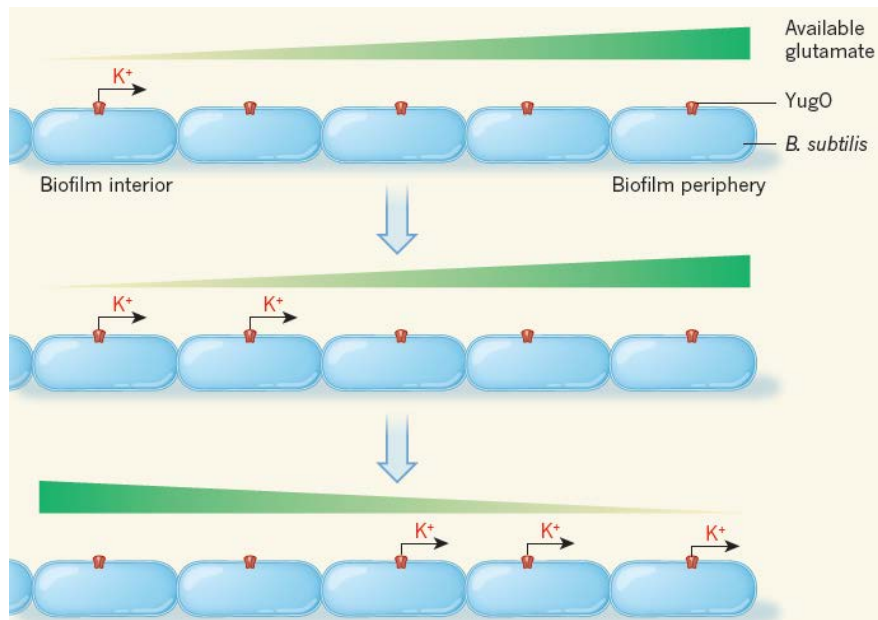
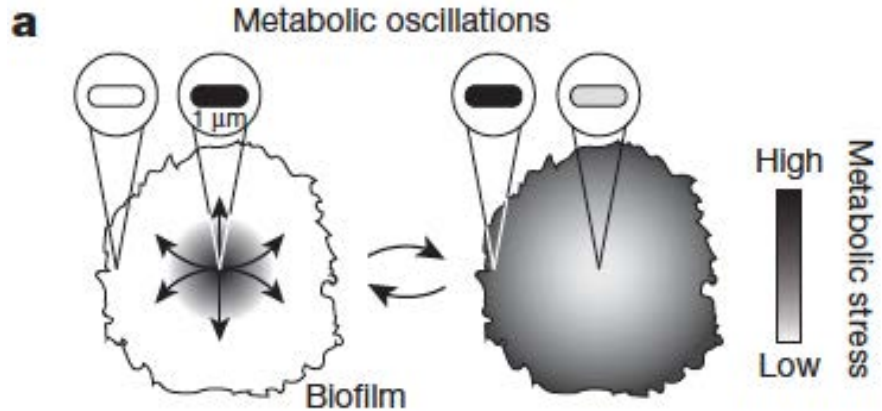
Forbes, *PNAS*, 2015

Synchronized cycles of bacterial lysis for in vivo delivery

Din, *Nature*, 2016



Electrical communication in bacterial communities

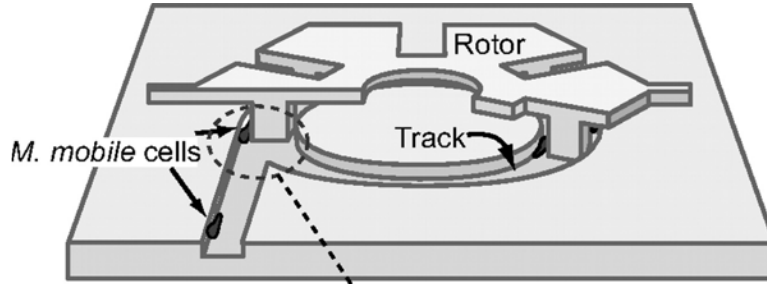


Bacillus subtilis biofilm

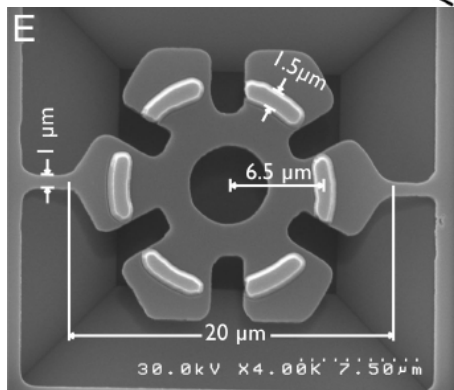
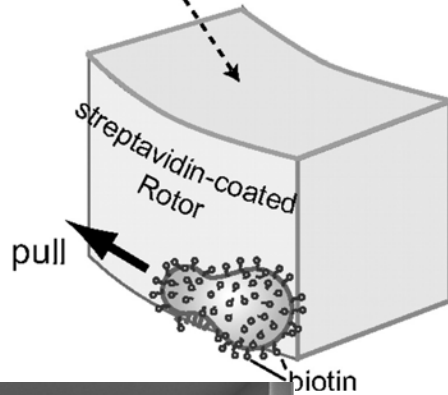


Prindle, *Nature*, 2016

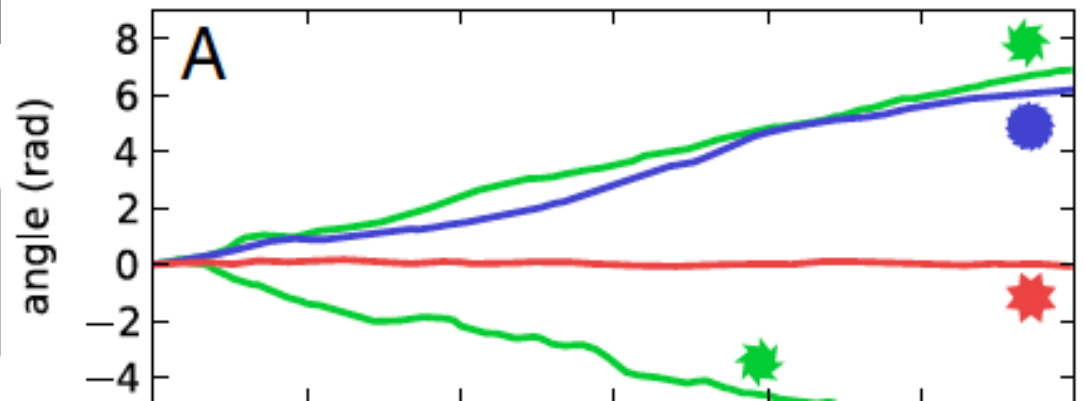
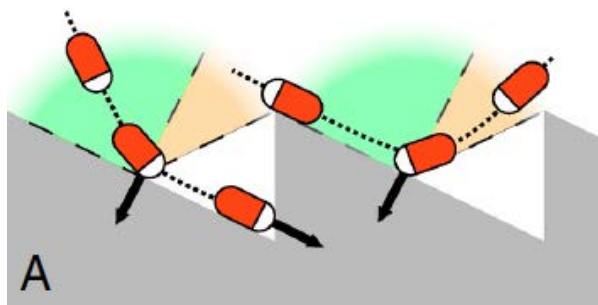
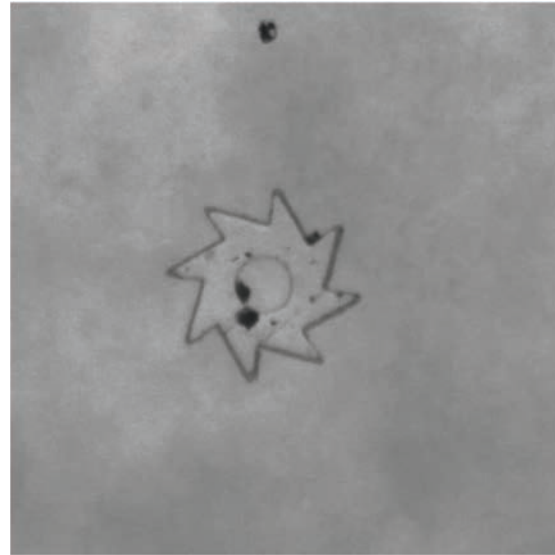
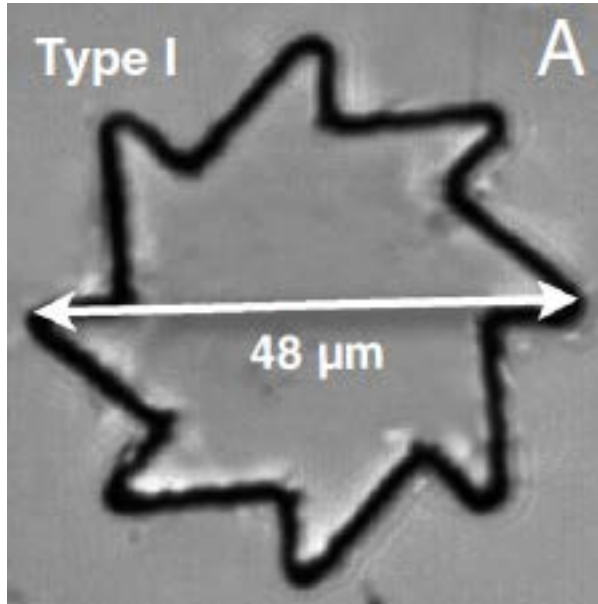
Motor powered by *Mycoplasma*



Uyeda, *PNAS*, 2006



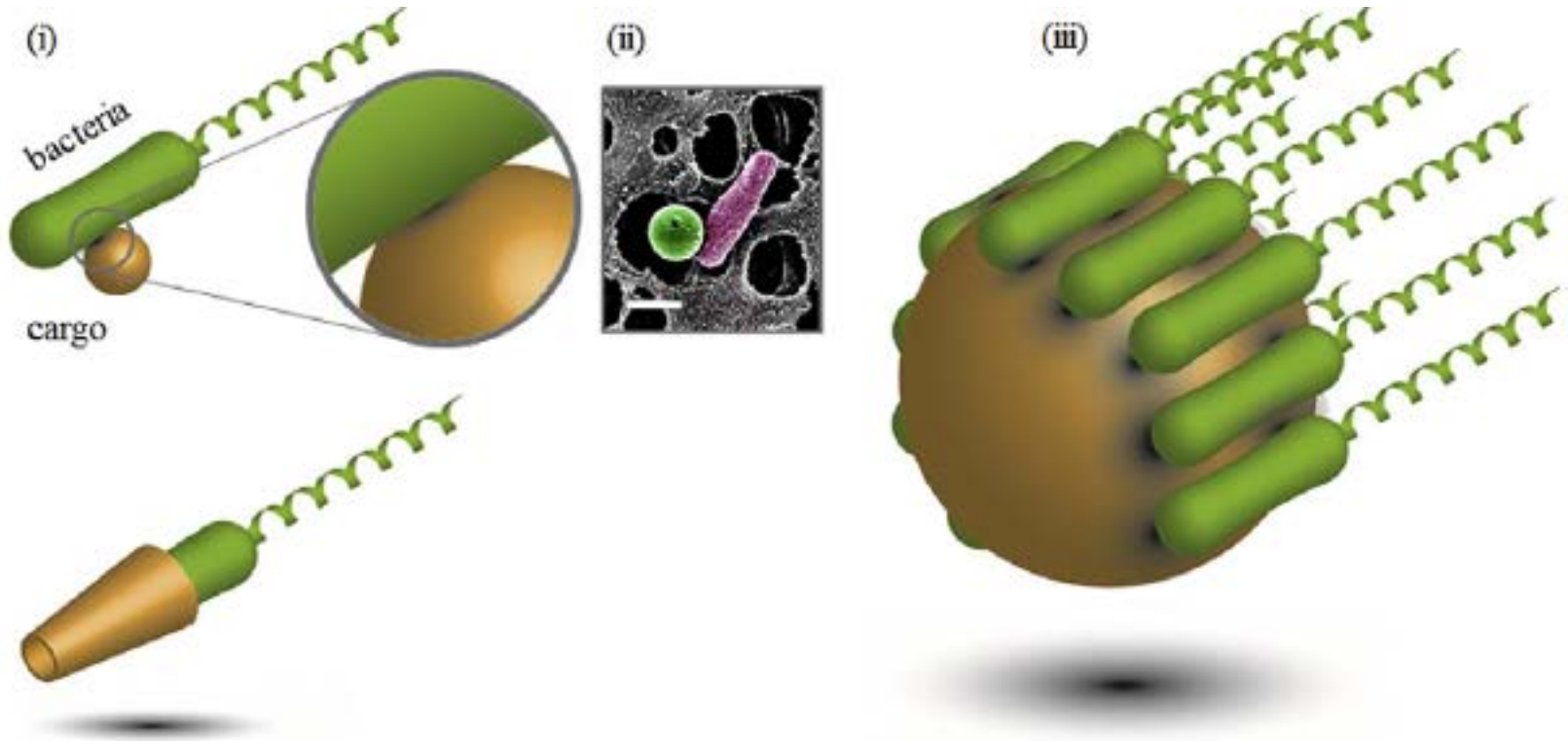
Bacterial ratchet motors



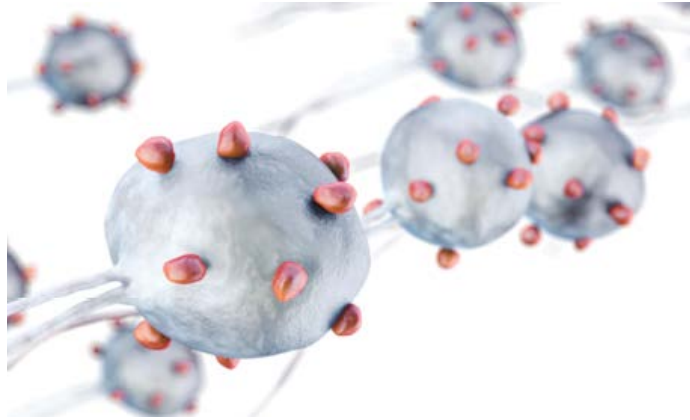
Sokolov, *PNAS*, 2009

Di Leonardo, *PNAS*, 2010

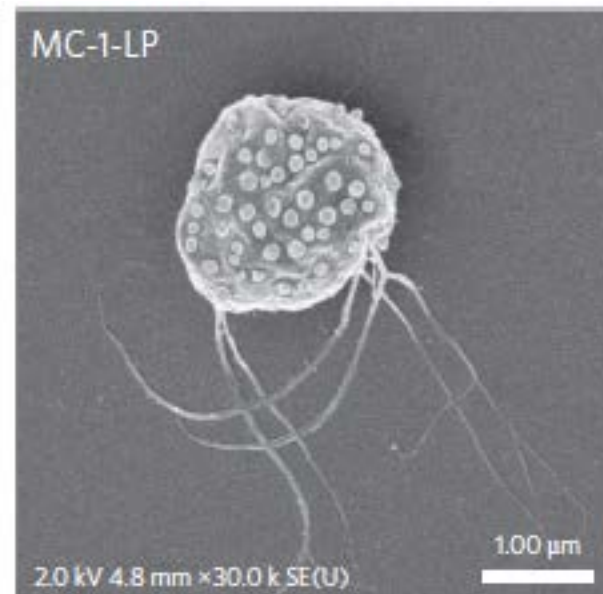
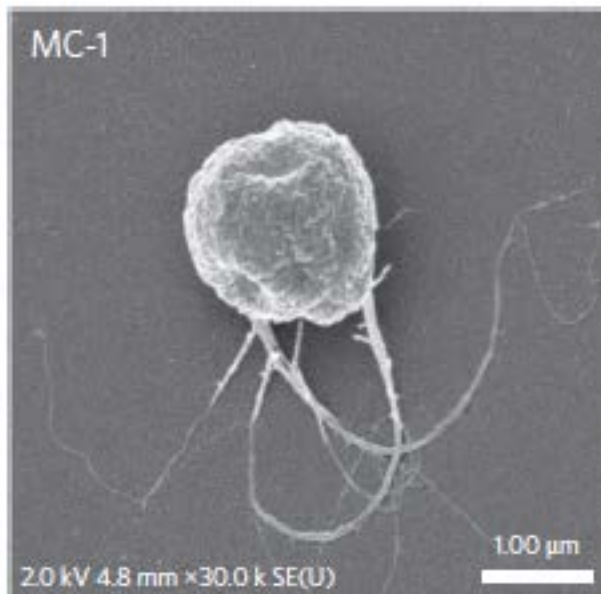
Techniques for Engaging with Cargo



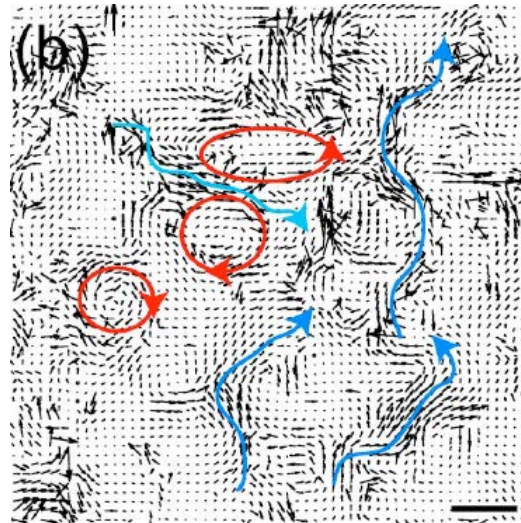
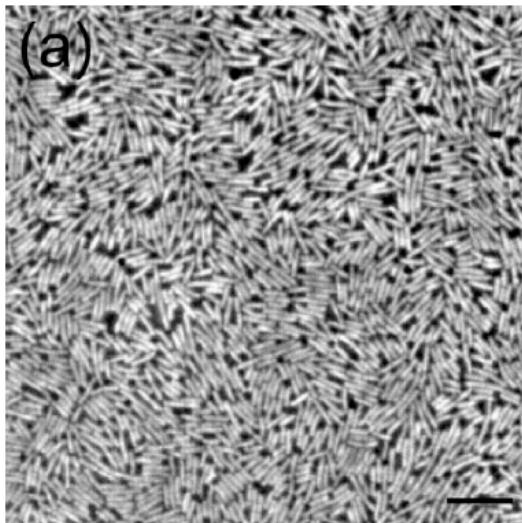
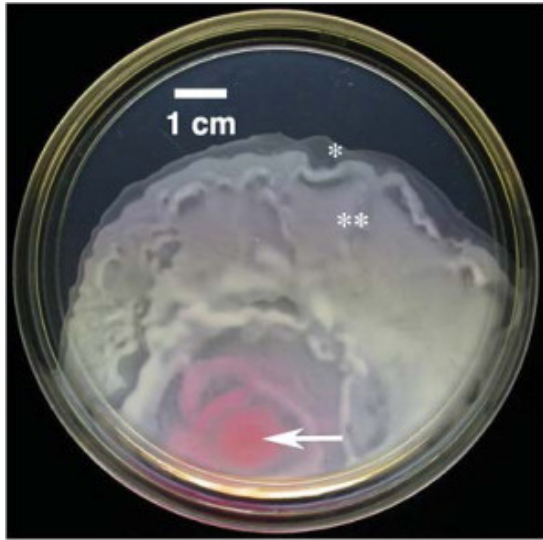
Liposomes for drug delivery



Martel, *Nat Biotec*, 2016



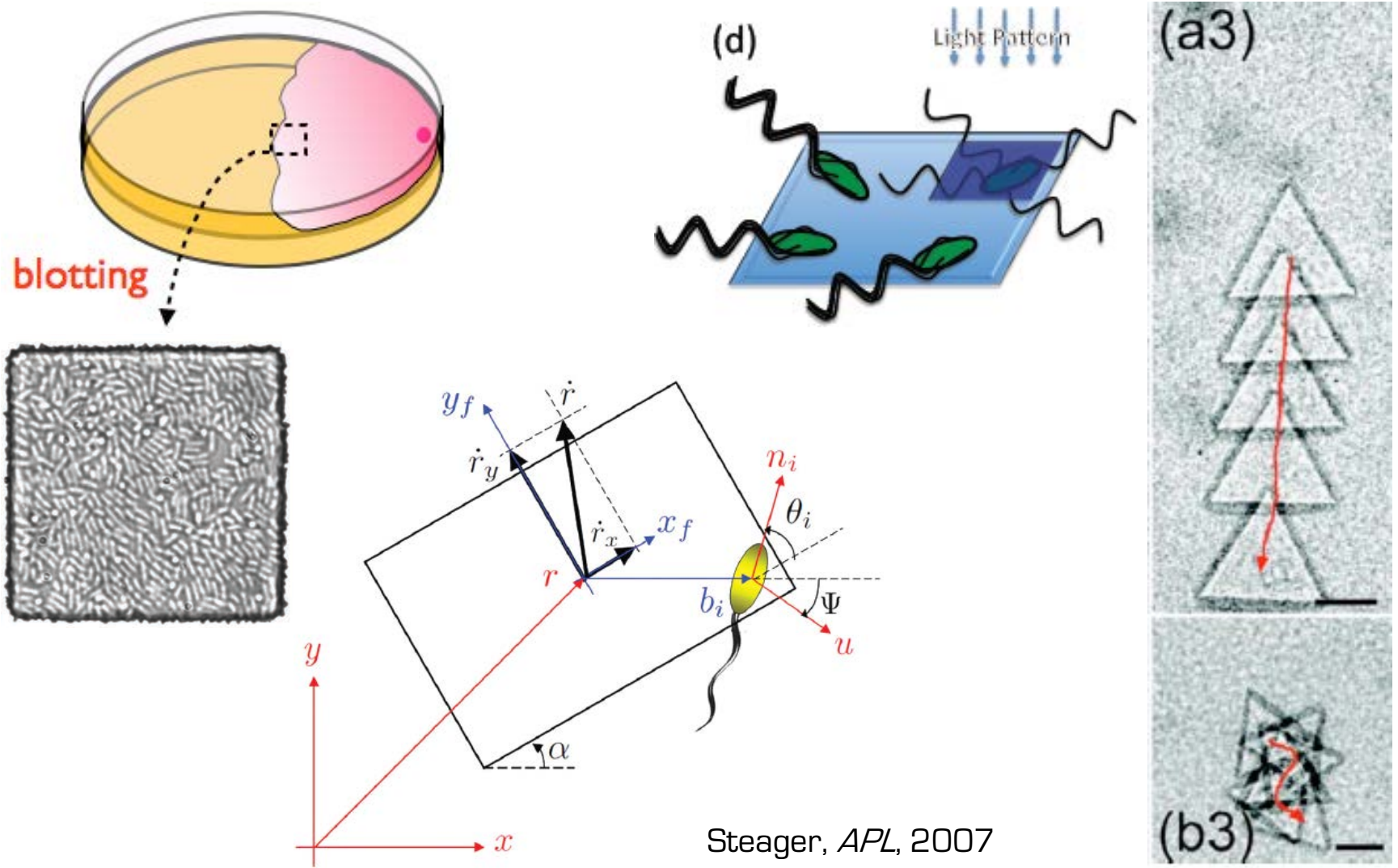
Bacterial Carpets



Serratia marcescens

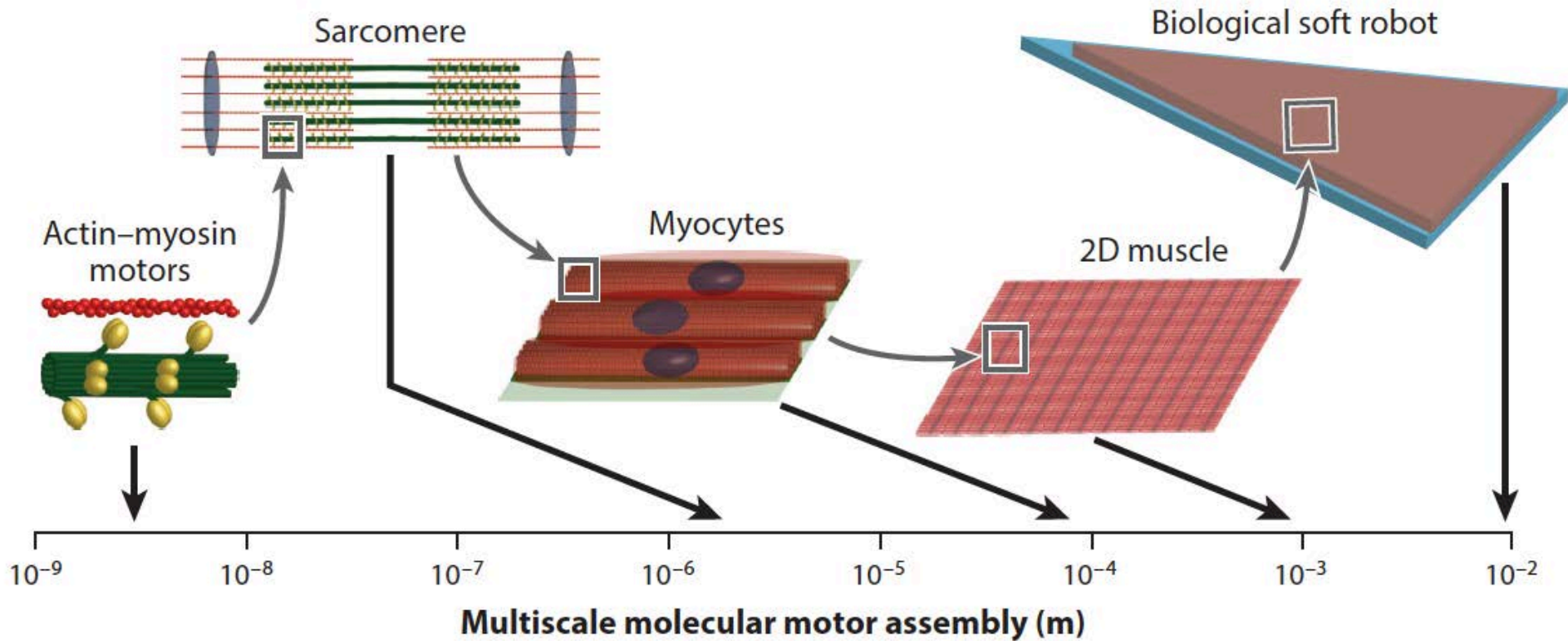
Darnton, *Biophys J*, 2004

Blotting Swarming Bacteria



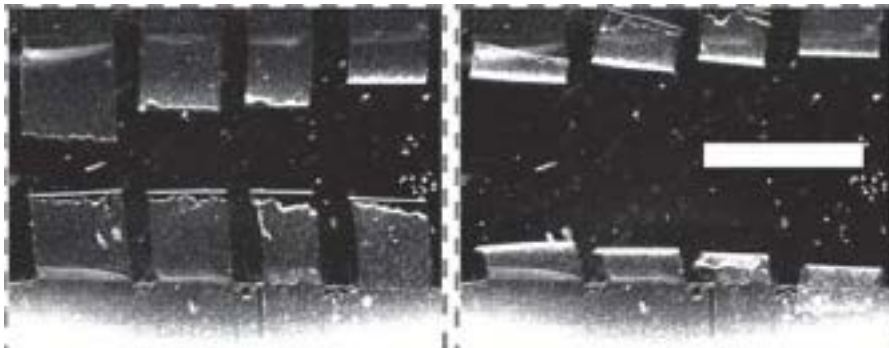
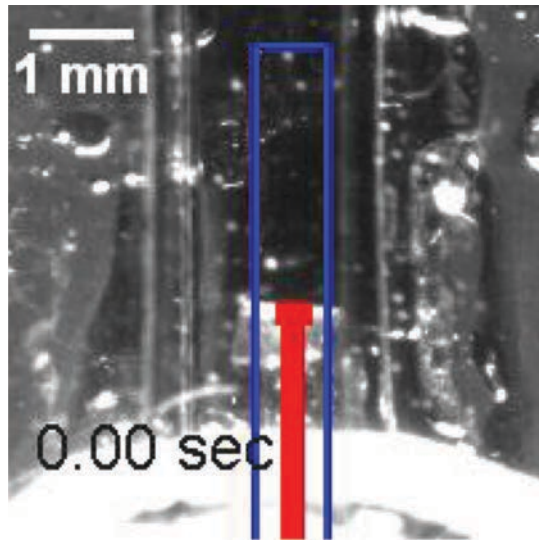
Steager, *APL*, 2007

Biological Soft Robot



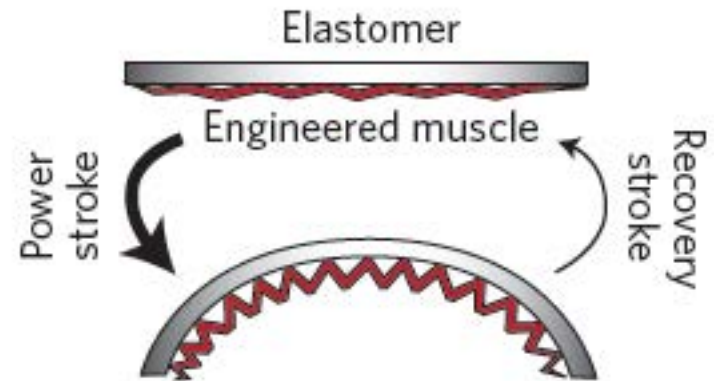
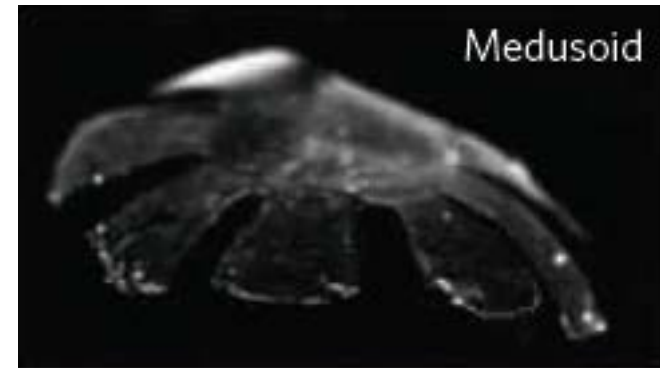
A Case Study: Muscular Thin Films

Heart on a chip



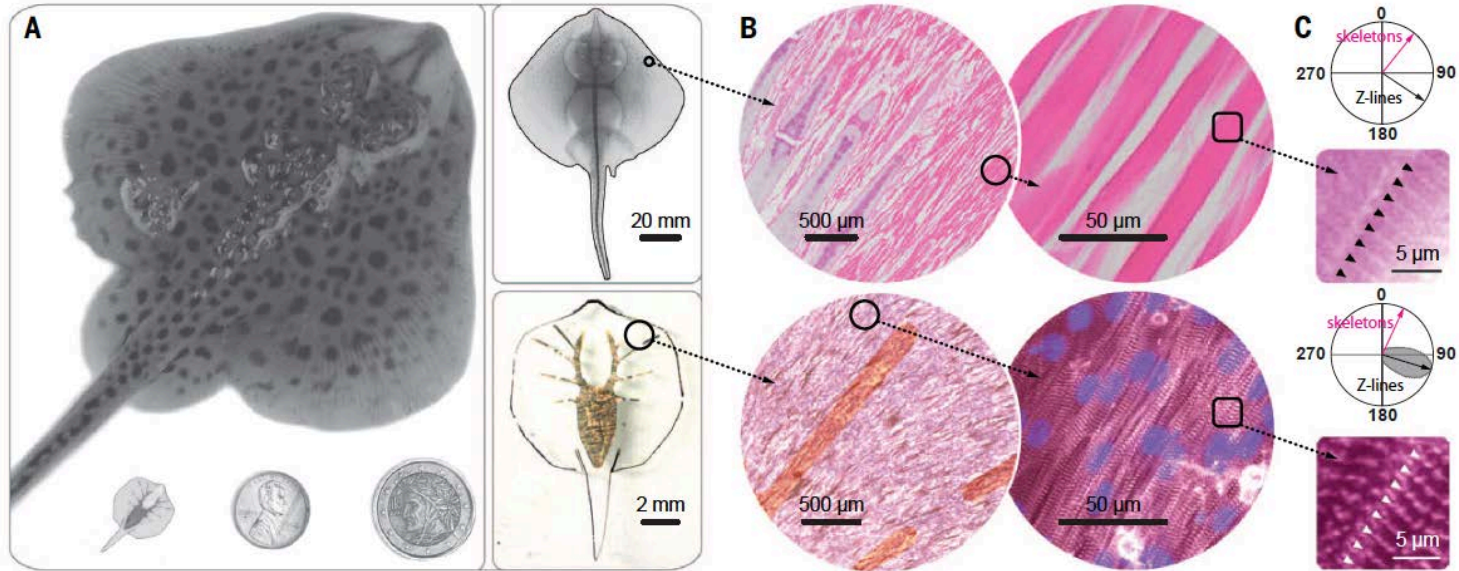
A. Grossberg *et al.*, **Lab Chip**, 2011

Artificial Jellyfish



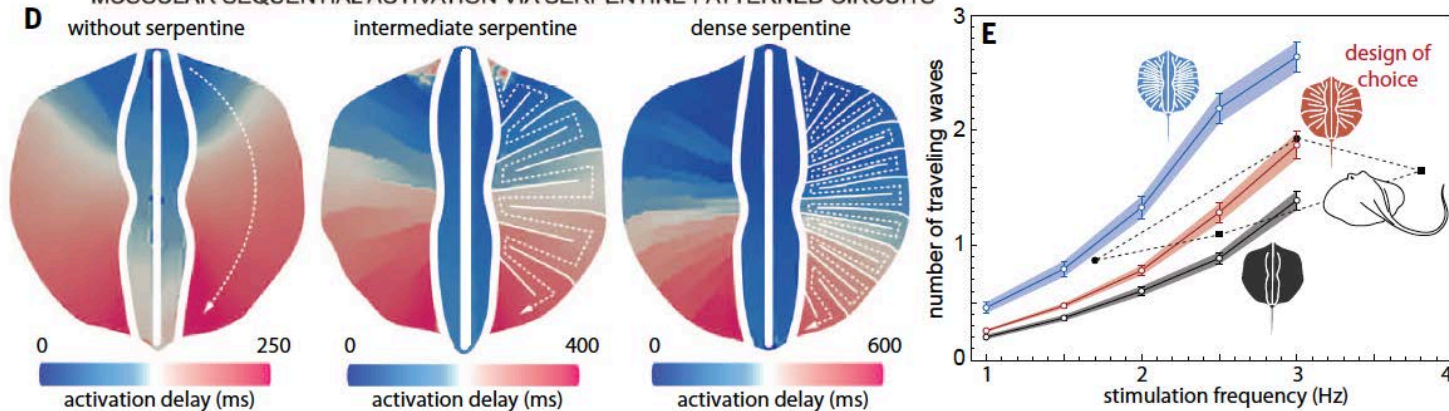
J. C. Nawroth *et al.*, **Nat Biotech**, 2012

Tissue-engineered Soft Robotic Ray

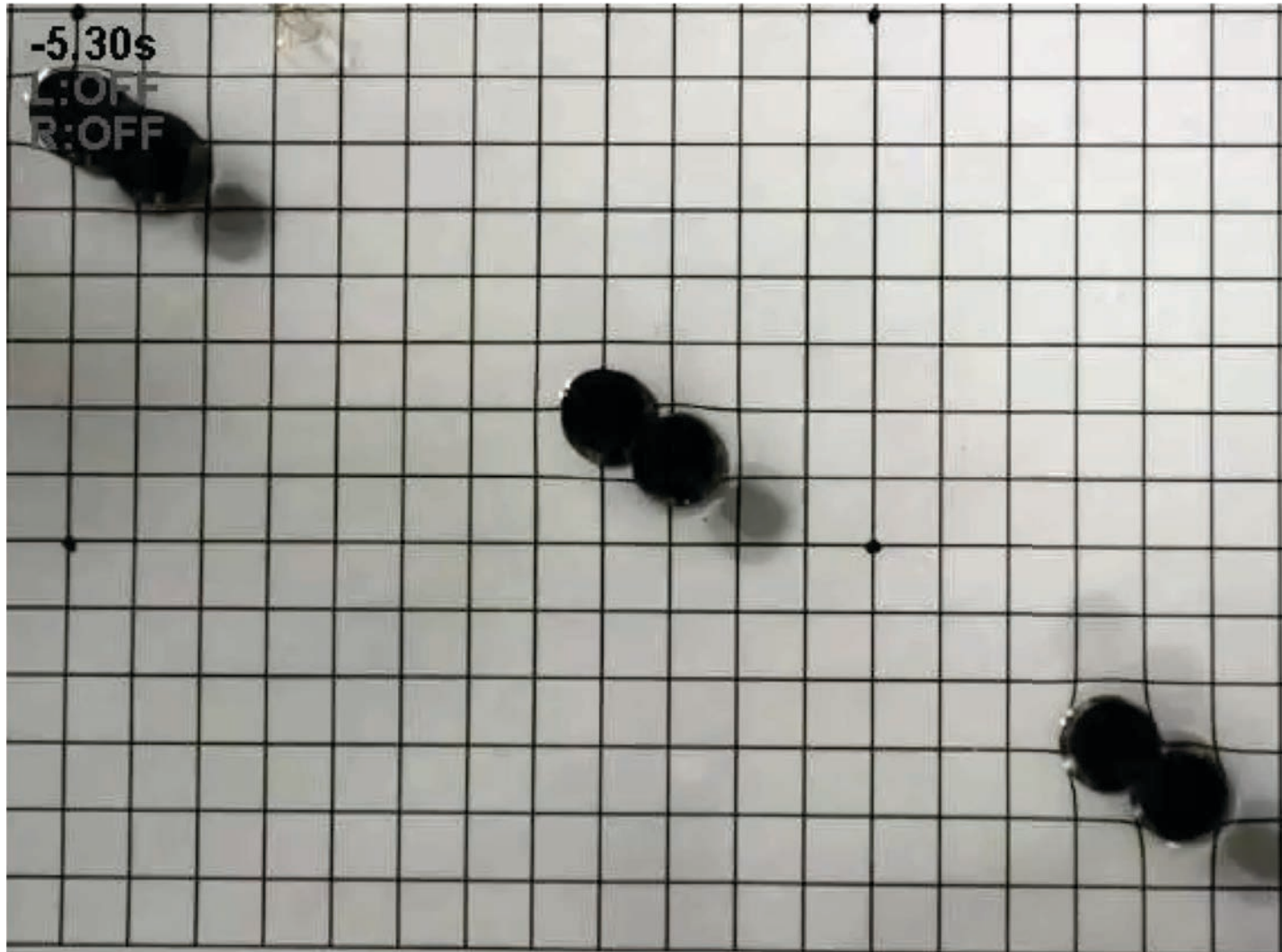


MUSCULOSKELETAL ARCHITECTURE

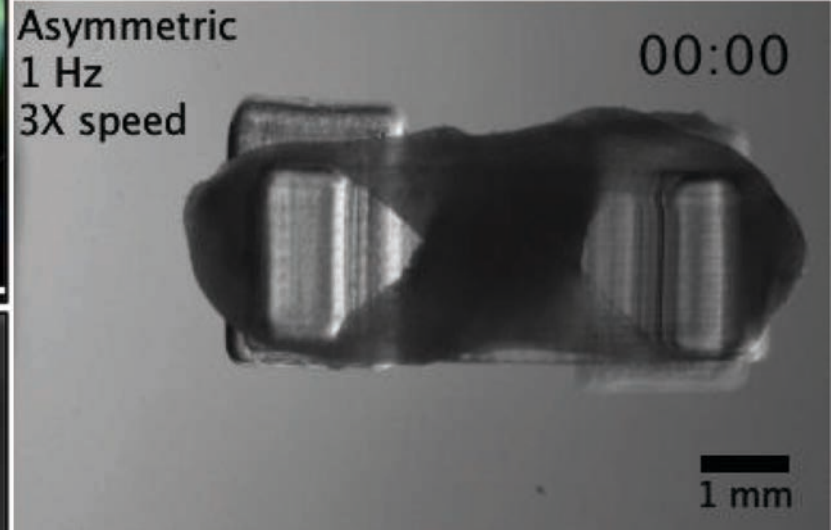
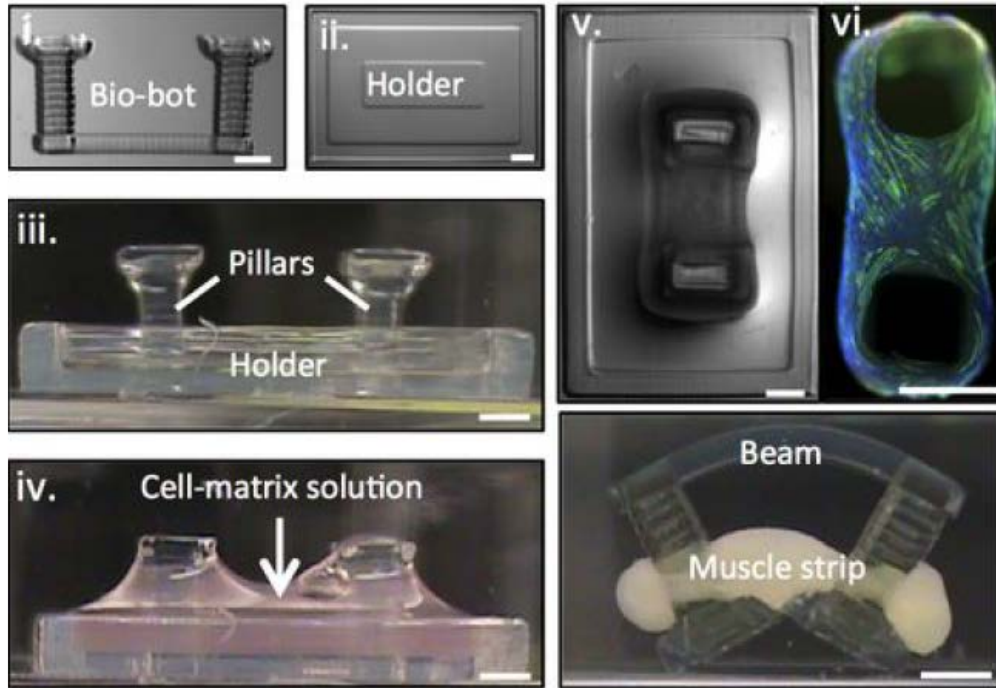
MUSCULAR SEQUENTIAL ACTIVATION VIA SERPENTINE PATTERNED CIRCUITS



Tissue-engineered Soft Robotic Ray



Engineered Skeletal Muscle Bioactuators



Summary

- Microrobotics as an emerging field
- Many unsolved issues
- A solid understanding of nanoscale phenomena is the key
- Microtechnology, materials science, robotics
- Primary application areas are medicine and basic life sciences