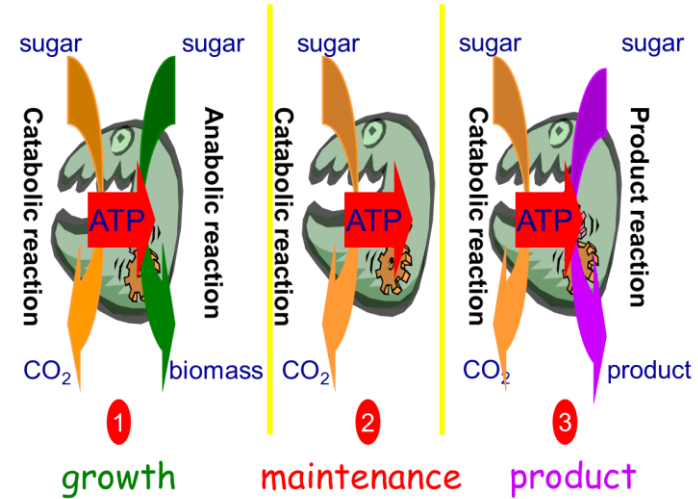
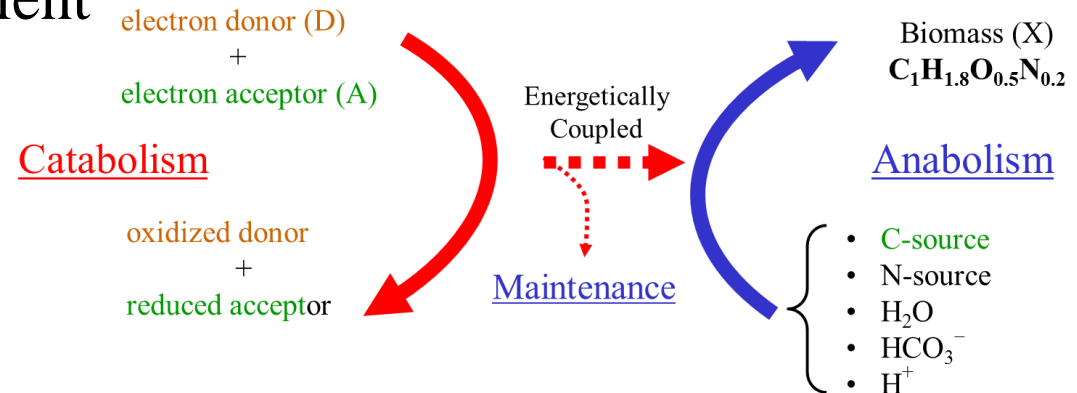


Thermodynamics of growth (To help us)

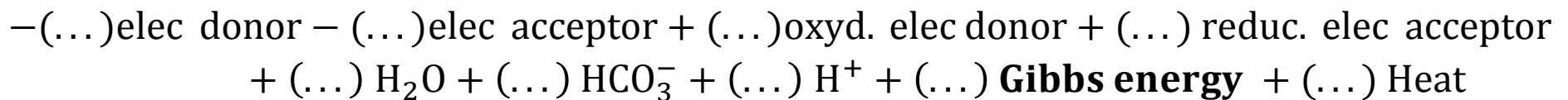
- Some thermodynamic fundamentals
- Thermodynamic analysis of anabolism and catabolism coupling
- Prediction of the **growth reaction stoichiometry**
- Prediction of maintenance coefficient m_S
- Prediction of μ^{\max}
- Prediction of growth Heat



Growth system definition



Catabolic reaction:



Thermodynamic fundamentals

From Energy of chemical bonds, the fraction available to do “work” is free energy:

$$\Delta G = \Delta H - T\Delta S$$

ΔG : change in free Gibbs Energy = energy available to do “work”

ΔH : change in Enthalpy

ΔS : change in Entropy

Each compound represents
Gibbs energy and Enthalpy

$\Delta G_f^\circ = \Delta G_f$ Gibbs energy of formation, under standard conditions [kJ.mole⁻¹]

$\Delta H_f^\circ = \Delta H_f$ Enthalpy of formation, under standard conditions [kJ.mole⁻¹]

(Available in Handbooks for many substances)

ΔG_f° Standard conditions:

298 [K], 1 [bar] gaseous

or 1 [mole.L⁻¹] dissolved compound

$$\Delta G_f = \Delta G_f^\circ + RT \ln \left(\frac{C}{C^\circ} \right)$$

R = gas constant 8.31410⁻³ [kJ.mole⁻¹.K⁻¹]

T = Absolute temperature in [K]

C = Concentration [mole.L⁻¹] (or for gas, partial pressure in [bar])

C⁰ = reference Conc. [mole.L⁻¹] (or p⁰=1 [bar])

Biochemical reference ΔG_f^{01} : pH = 7; 298 °K; 1 mole.L⁻¹; 1 atm

Standard Gibbs Energy and Enthalpy of formation ΔG_f^{01} at 298K, pH=7, 1bar, 1mole/L for relevant

Compound name	Composition	ΔG_f^{01} (kJ/mol)	ΔH_f (kJ/mol)
Biomass	CH _{1.8} O _{0.5} N _{0.2}	-67	-91
Water	H ₂ O	-237.18	-286
Bicarbonate	HCO ₃ ⁻	-586.85	-692
CO ₂ (g)	CO ₂	-394.359	-394.1
Ammonium	NH ₄ ⁺	-79.37	-133
Proton	H ⁺	-39.87	0
O ₂ (g)	O ₂	0	0
Oxalate ²⁻	C ₂ O ₄ ²⁻	-674.04	-824
Carbon monoxide	CO	-137.15	-111
Formate	CHO ₂ ⁻	-335	-410
Glyoxylate ⁻	C ₂ O ₃ H ⁻	-468.6	—
Tartrate ²⁻	C ₄ H ₄ O ₆ ²⁻	-1,010	—
Malonate ²⁻	C ₃ H ₂ O ₄ ²⁻	-700	—
Fumarate ²⁻	C ₄ H ₂ O ₄ ²⁻	-604.21	-777
Malate ²⁻	C ₄ H ₄ O ₅ ²⁻	-845.08	-843
Citrate ³⁻	C ₆ H ₅ O ₇ ³⁻	-1,168.34	-1,515
Pyruvate ⁻	C ₃ H ₃ O ₃ ⁻	-474.63	-596
Succinate ²⁻	C ₄ H ₄ O ₄ ²⁻	-690.23	-909
Gluconate ⁻	C ₆ H ₁₁ O ₇ ⁻	-1,154	—
Formaldehyde	CH ₂ O	-130.54	—
Acetate	C ₂ H ₃ O ₂ ⁻	-369.41	-486
Dihydroxyacetone	C ₃ H ₆ O ₃	-445.18	—
Lactate	C ₃ H ₅ O ₃ ⁻	-517.18	-687
Glucose	C ₆ H ₁₂ O ₆	-917.22	-1,264
Mannitol	C ₆ H ₁₄ O ₆	-942.61	—
Glycerol	C ₃ H ₈ O ₃	-488.52	-676
Propionate ⁻	C ₃ H ₅ O ₂ ⁺	-361.08	—
Ethylene glycol	C ₂ H ₆ O ₂	-330.50	—
Acetoine	C ₄ H ₈ O ₂	-280	—
Butyrate	C ₄ H ₇ O ₂ ⁻	-352.63	-535

Compound name	Composition	ΔG_f^{01} (kJ/mol)	ΔH_f (kJ/mol)
Propanediol	C ₃ H ₈ O ₂	-327	—
Butanediol	C ₄ H ₁₀ O ₂	-322	—
Methanol	CH ₄ O	-175.39	-246
Ethanol	C ₂ H ₅ O	-181.75	-288
Propanol	C ₃ H ₈ O	-175.81	-331
<i>n</i> -Alkane	C ₁₅ H ₃₂	+60	-439
Propane	C ₃ H ₈	-24	-104
Ethane	C ₂ H ₆	-32.89	-85
Methane	CH ₄	-50.75	-75
H ₂ (g)	H ₂	0	0
N ₂ (g)	N ₂	0	0
Nitrite ion	NO ₂ ⁻	-37.2	-107
Nitrate ion	NO ₃ ⁻	-111.34	-173
Iron II	Fe ²⁺	-78.87	-87
Iron III	Fe ³⁺	-4.6	-4
Hydrogen sulfide (g)	H ₂ S	-33.56	-20
Sulfide ion	HS ⁻	+12.05	-17
Sulfate ion	SO ₄ ²⁻	-744.63	-909
Thiosulfate ion	S ₂ O ₃ ²⁻	-513.2	-608

Note: pH = 7, 1 atm, 1 mol/L, 298 K.

Gibbs Energy and Heat of reactions

For a given REACTION: $\alpha A + \beta B \rightarrow \gamma C + \delta D_{(gas)}$
 or $-\alpha A - \beta B + \gamma C + \delta D_{(gas)}$

Gibbs Free Energy of a reaction:

$$\Delta G_R^0 = \delta \cdot \Delta G_{fD}^0 + \gamma \cdot \Delta G_{fC}^0 - \alpha \cdot \Delta G_{fA}^0 - \beta \cdot \Delta G_{fB}^0$$

2nd Law: $\Delta G_R < 0$

ΔG_R^0 = Standard Gibbs Free Energy of a reaction when all reactants are at 1 mole/L, 1atm

ΔG_R^{01} = Standard Gibbs Free Energy when all reactants are at 1 mole/L, 1atm and pH 7.

$$\Delta G_R = \Delta G_R^0 + RT \ln \frac{\left(\frac{C}{1M}\right)^\gamma \cdot \left(\frac{D}{1bar}\right)^\delta}{\left(\frac{A}{1M}\right)^\alpha \cdot \left(\frac{B}{1M}\right)^\beta}$$

Heat of the reaction:

$\Delta H_R > 0$ or $\Delta H_R < 0$

$$\Delta H_R^0 = \delta \Delta H_{fD}^0 + \gamma \Delta H_{fC}^0 - \alpha \Delta H_{fA}^0 - \beta \Delta H_{fB}^0$$

Diversity of microbial growth system

Depending on growth biosystem, a huge variation is observed :

- Biomass yield on substrate

$$Y_{SX}: 0.01 - 0.7 \text{ [C-moleX.moleS}^{-1}\text{]}$$

- Maximum growth rate μ^{\max} varies from : 0.001 to 1.5 [h⁻¹]
- Maintenance coefficients

$$m_S = 0.01 - 1 \text{ [moleS.C-moleX}^{-1}\text{.h}^{-1}\text{]}$$

This microbial bioprocess behavior diversity comes from huge environmental conditions, depending on:

C-source

Organic

Inorganic

e-donor

Organic

Inorganic

e-acceptor

Organic

Inorganic

Energy !

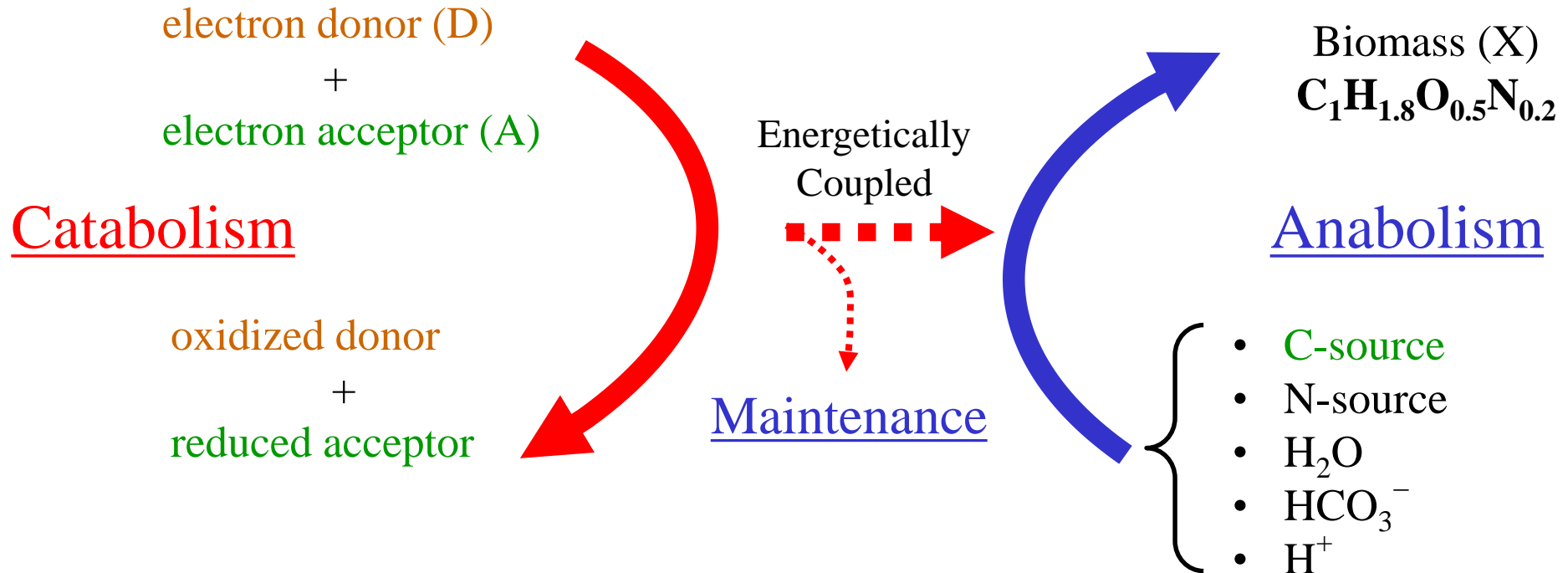
Why such variation?



Prof. J.J. Heijnen

Thermodynamics of growth

“The Energetic Anabolism/Catabolism coupling ”



3 arrows = 3 Gibbs Energy flux due to Anabolism/Catabolism coupling:

- 1 **Gibbs energy** needed in the **anabolic reaction**
- 2 **Gibbs energy** needed for **maintenance**
- 3 **Gibbs energy** produced by **catabolic reaction**

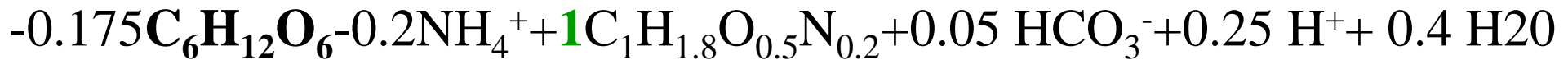
Gibbs energy required for anabolic reaction to produce 1 C-mole of biomass

All coefficients follow from conservation C , H, O, N and charge balances

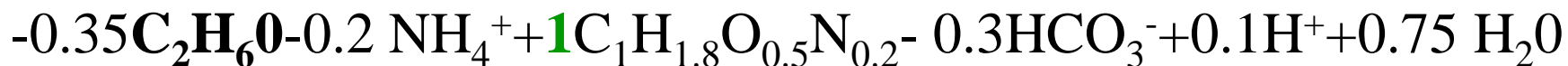
(Electron acceptor is absent!)

$$\Delta G_R^0 = \delta \cdot \Delta G_{fD}^0 + \gamma \cdot \Delta G_{fC}^0 - \alpha \cdot \Delta G_{fA}^0 - \beta \cdot \Delta G_{fB}^0$$

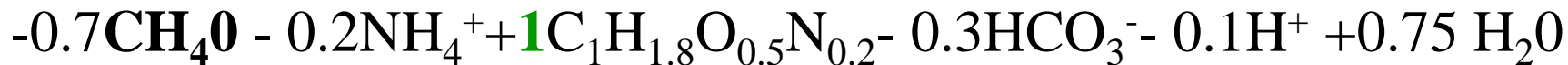
Case of Organic C-source (using ΔG_f^{01} table)



$$\Delta G_R^{01} = -24.8 \text{ [kJ.C_moleX}^{-1}\text{]}$$

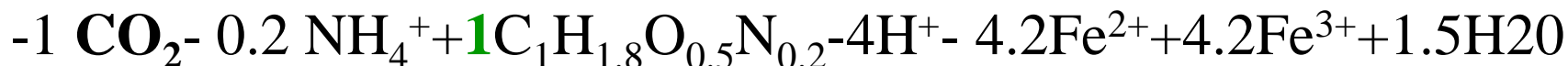


$$\Delta G_R^{01} = +14.63 \text{ [kJ.C_moleX}^{-1}\text{]}$$



$$\Delta G_R^{01} = -9.2 \text{ [kJ.C_moleX}^{-1}\text{]}$$

In case of Inorganic C-source



$$\Delta G_R^{01} = +341.56 \text{ [kJ.C_moleX}^{-1}\text{]}$$

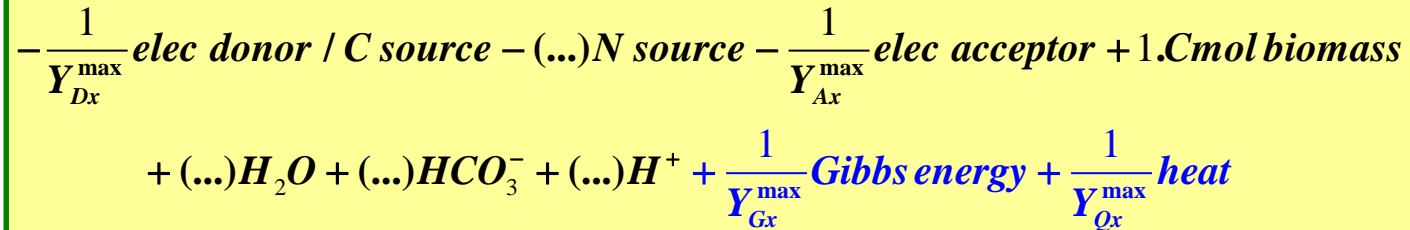
Note: Electron from $\text{Fe}^{2+}/\text{Fe}^{3+}$ donor has not enough energy to reduce CO_2 to biomass X. The reversed electron transfer (RET) mechanism is needed.

Gibbs energy required for GROWTH reaction to produce 1 C-mole of biomass

Free energy required **anabolic** reaction:

- Organic C-source $\Delta G \approx 0$
- CO_2 (inorganic C-source) $\Delta G \gg 0$

Overall Growth reaction:



Is highly irreversible, because of the large Gibbs energy required, Y_{GX}^{\max} :

$$1/Y_{GX}^{\max} = \mathbf{200- 4000 \text{ kJ}} \text{ for production of 1 C-mole X}$$

Y_{GX}^{\max} ? Issued from a data set for growth of different micro-organisms



The data set covers a wide range of MEDIUM :

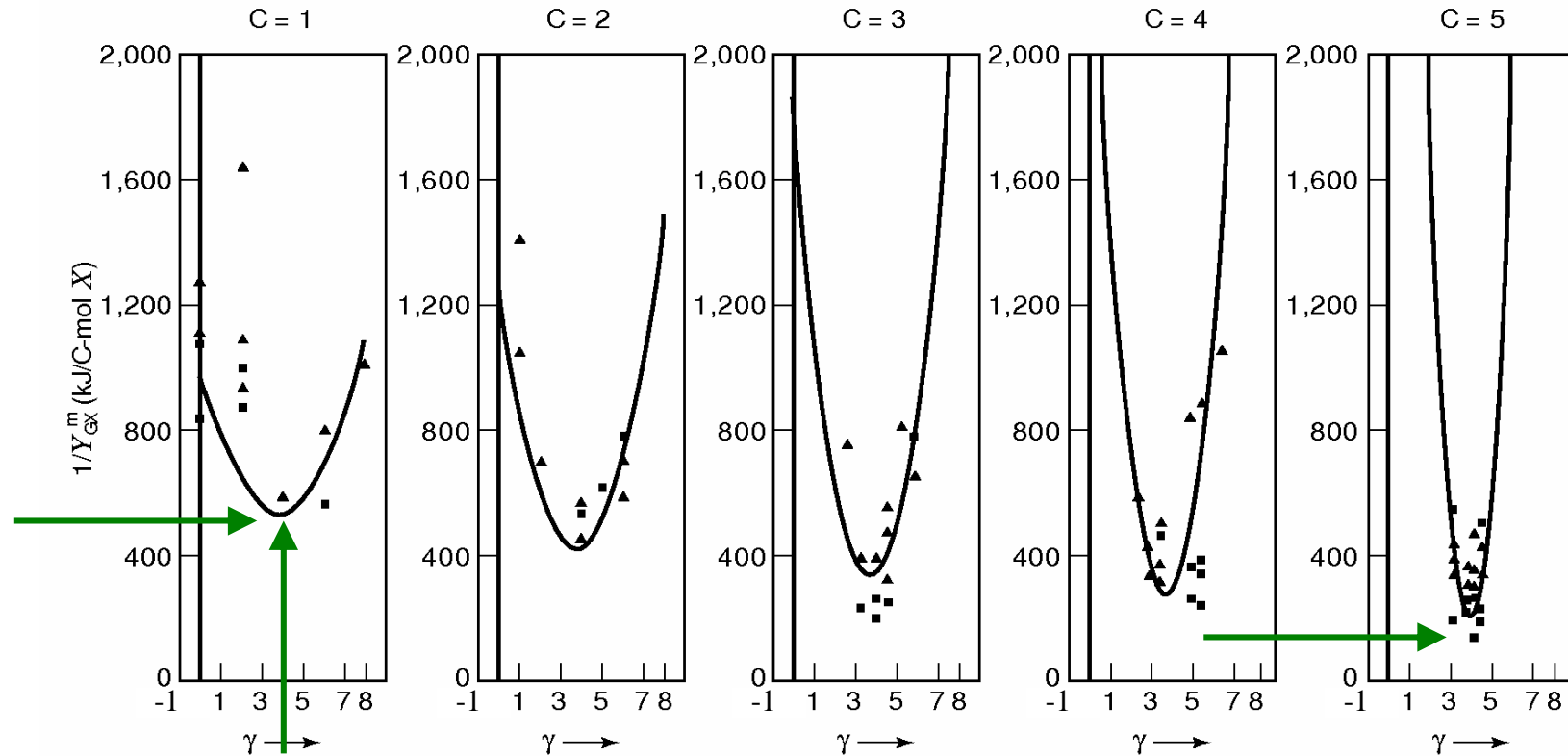
- Mineral media, **C-source limited**, unknown product formation excluded ...
- Wide variety of carbon sources:
 - **1 to 6 C atoms**
 - **0 – 8, γ_c degree of reduction** [e_mole/C_mole])
- Different **electron acceptors**
- Different electron donors with and without reversed electron transport RET requirement

MICROORGANISMS : Many different microorganisms

METABOLISM :

- **Heterotrophic and autotrophic growth**
- **Aerobic / denitrification / fermentation**

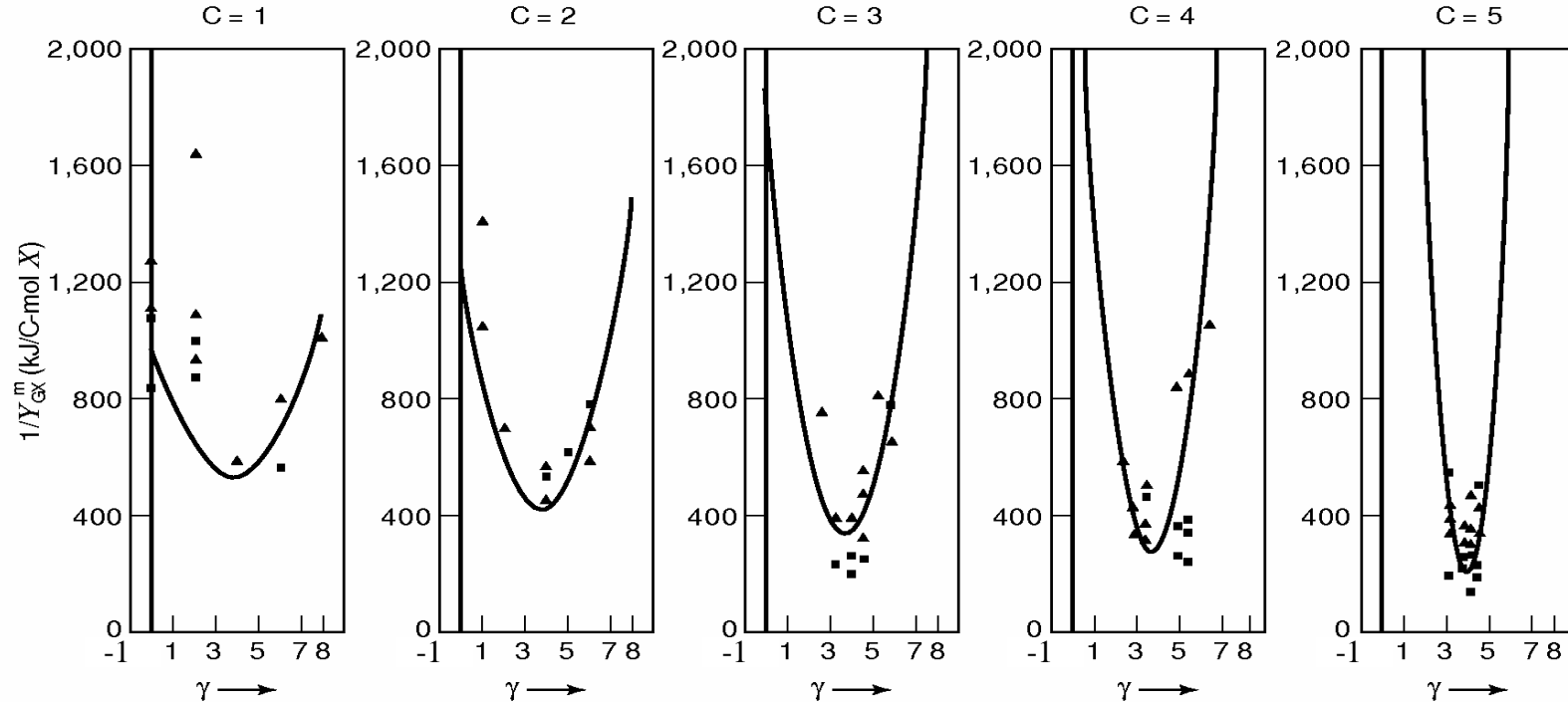
Gibbs energy needed for heterotrophic growth



In heterotrophic growth, $1/Y_{GX}^{\max}$ depends only on C-source (organic):

- its **degree of reduction** (γ_c) [e mole/C_mole] (energy needs increase with γ deviating from 4) ?
- its number of **C-atoms** (C) (energy needs increase with smaller C content) ?

Gibbs energy needed for heterotrophic growth



In heterotrophic growth, $1/Y_{GX}^{\max}$ - its degree of reduction (γ_c) [e mole/C_mole]
 [kJ.C_moleX⁻¹] depends on : - its number of **C-atoms (C)**

$$\frac{1}{Y_{GX}^{\max}} = 200 + 18 * (6 - C)^{1.8} + \exp \left\{ \left[(3.8 - \gamma_c)^2 \right]^{0.16} (3.6 + 0.4 * C) \right\}$$

Gibbs energy needed for autotrophic growth

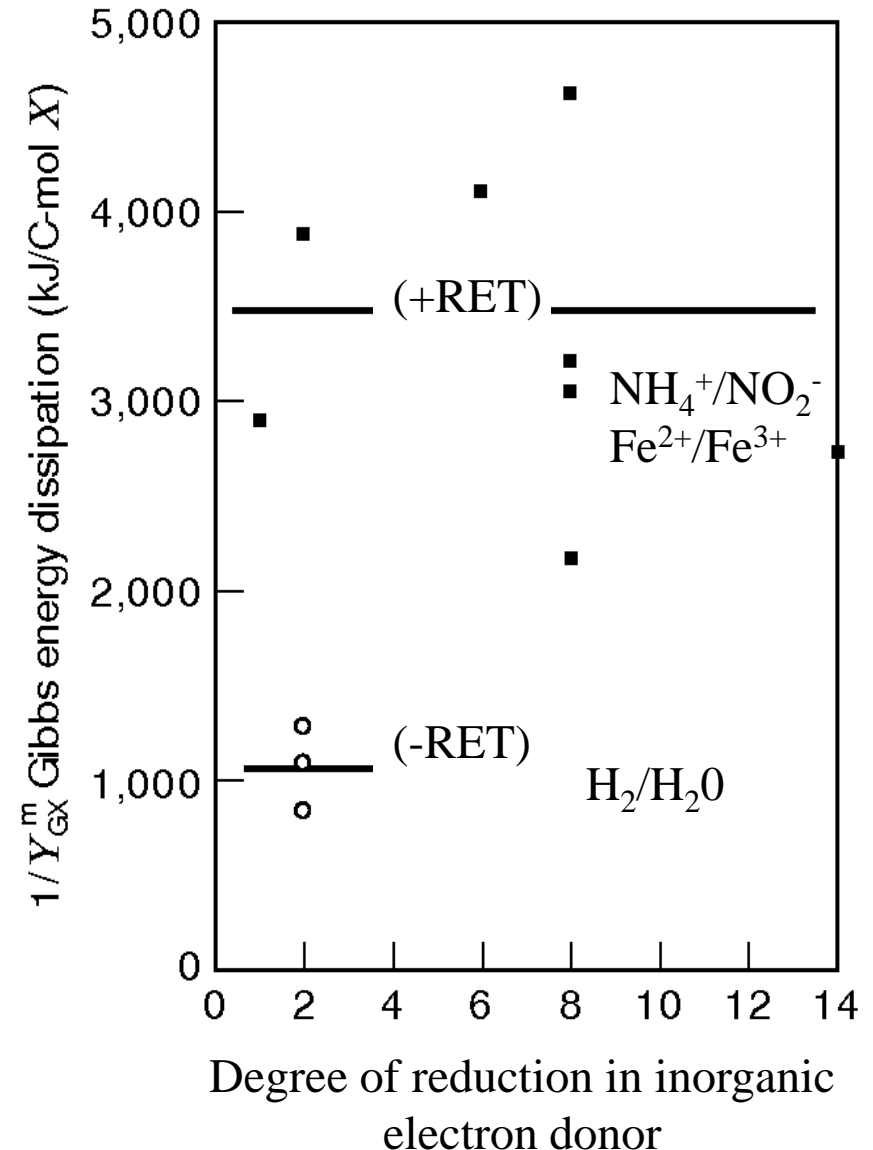
In autotrophic growth, with CO_2 as C-source, $1/Y_{\text{GX}}^{\text{max}}$:

- **Depends on the nature of electron donor** (if it requires or not RET (Reverse Electron Transfer) mechanism)
- **Does not depend on electron acceptor**

Explanation: more biochemical work has to be done with CO_2 as C-source, specially if RET is required:

$$\frac{1}{Y_{\text{GX}}^{\text{max}}} = 1000 \text{ (Without RET)}$$

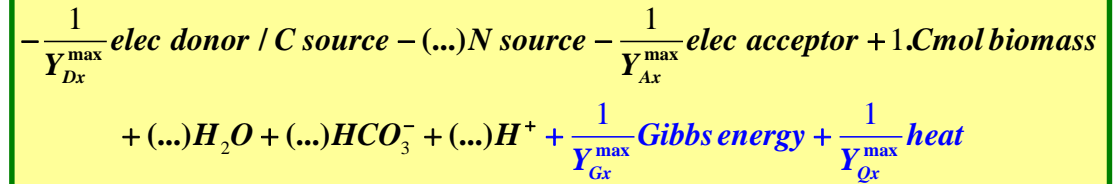
$$= 3500 \text{ (With RET)}$$



Gibbs energy needed for Growth of 1 C-mole biomass, $1/Y_{GX}^{\max}$ [kJ.C-mole X^{-1}]

Energy required for Overall Growth reaction,

2 cases:



Heterotrophic Growth on organic C-Source: \rightarrow Correlation for $1/Y_{GX}^{\max}$
[kJ.C-mole X^{-1}]

Which depends only on:

$$\frac{1}{Y_{GX}^{\max}} = 200 + 18 * (6 - C)^{1.8} + \exp \left\{ \left[(3.8 - \gamma_c)^2 \right]^{0.16} (3.6 + 0.4 * C) \right\}$$

- its degree of reduction (γ_c)
- its number of C-atoms (C)

Autotrophic growth on inorganic C-Source (CO_2) which depends on:

- Nature of electron donor
(and the need of RET)
- Does not depend on electron acceptor

$$\frac{1}{Y_{GX}^{\max}} = 1000 \text{ (Without RET)}$$

$$= 3500 \text{ (With RET)}$$

Gibbs energy needed for Maintenance of 1 C-mole biomass, m_G [kJ.C-mole⁻¹.hr⁻¹]

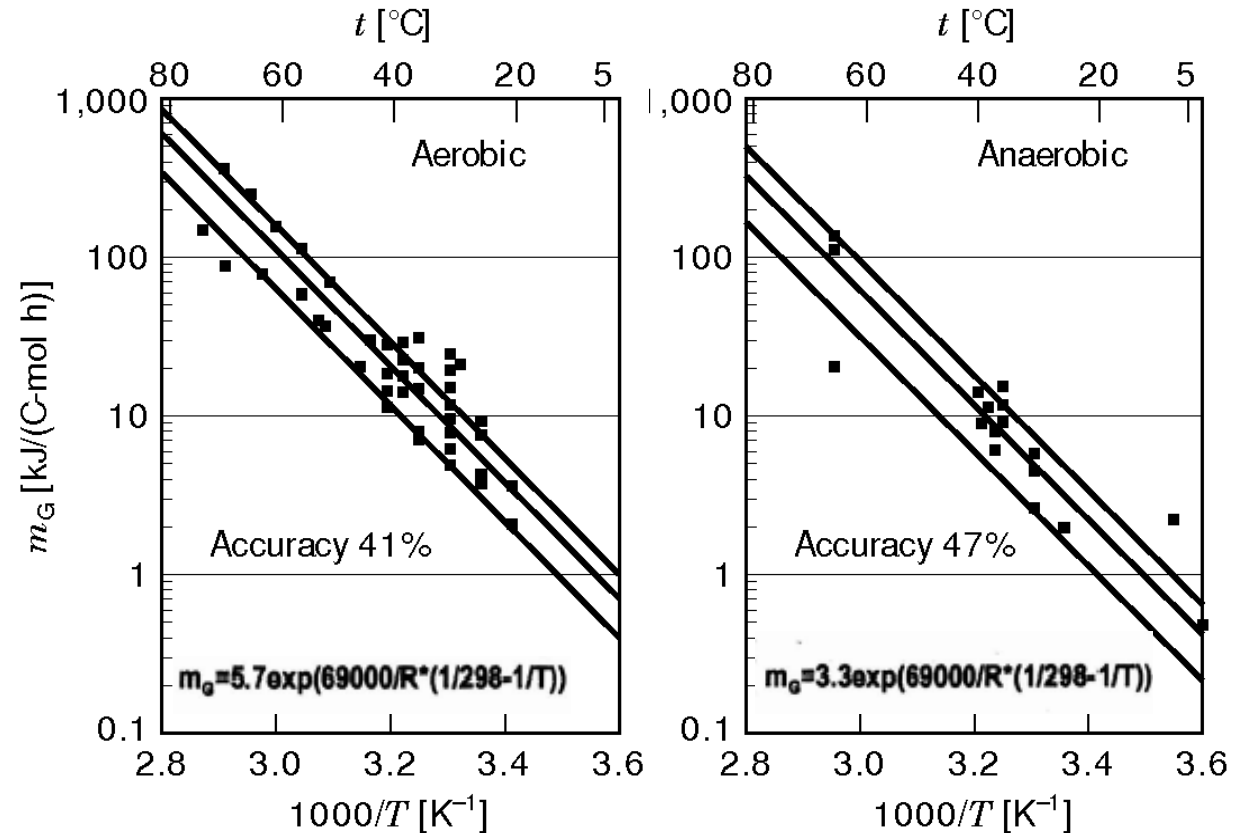
In micro-organisms, degradation processes occur with low rates. It concerns:

- Protein decay into amino acid
 - Leaks of ions over cell membranes e.g. Na⁺ influx
 - And many other processes
- Repair requires Gibbs energy from catabolic reaction for maintenance:

$$m_G = \frac{\text{kJ Gibbs energy}}{\text{C_moleX.hr}}$$

→ m_G correlation

$$m_G = 4.5 \exp\left(\frac{-69000}{R} \left(\frac{1}{T} - \frac{1}{298}\right)\right)$$



$R = 8.314$ J/mole K, $T =$ absolute T

- holds for many organisms
- holds for aerobic/anaerobic/denitrification growth
- **independently of C-source**
- **only Temperature-dependent**
- each 10 °C increase in temperature, m_G **doubles**

Summary Gibbs energy needed for growth and maintenance of 1 C-mole biomass, $1/Y_{GX}^{\max}$, m_G

For $1/Y_{GX}^{\max}$ [kJ.C-moleX⁻¹], 2 cases:

1. On organic C-source (**heterotrophic growth**), $\rightarrow 1/Y_{GX}^{\max}$ **correlation**

$$\frac{1}{Y_{GX}^{\max}} = 200 + 18 * (6 - C)^{1.8} + \exp\left\{\left[(3.8 - \gamma_c)^2\right]^{0.16} (3.6 + 0.4 * C)\right\}$$

2. For **autotrophic growth** on CO₂ as C-Source

$$\begin{aligned} \frac{1}{Y_{GX}^{\max}} &= 1000 \text{ (Without RET)} \\ &= 3500 \text{ (With RET)} \end{aligned}$$

For m_G [kJ.C-moleX⁻¹.hr⁻¹] $\rightarrow m_G$ **correlation:**

$$m_G = 4.5 \exp\left(\frac{-69000}{R} \left(\frac{1}{T} - \frac{1}{298}\right)\right)$$

Required Gibbs energy comes from catabolic reaction: ΔG_{Cat} [kJ.C-moleS⁻¹]:

Thus:

$$m_S = \frac{m_G}{-\Delta G_{cat}}$$

\rightarrow These are the 2 Gibbs Energy correlations!

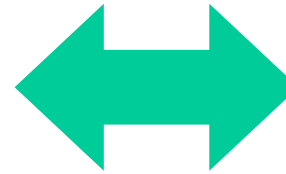
\rightarrow **Prediction of growth stoichiometry**

Prediction of growth stoichiometry

The growth stoichiometry prediction is based on :

1. Energetic coupling Anabolism - Maintenance / Catabolism

Gibbs energy needed for
Maintenance and Growth



Gibbs energy provided
by catabolism

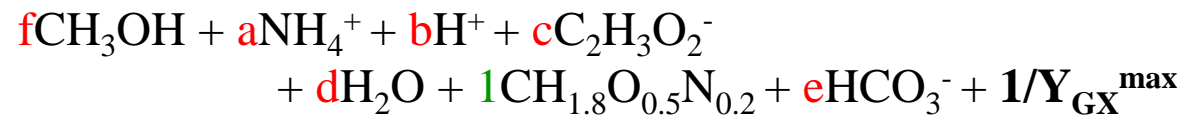
2. Gibbs energy balance

To calculate stoichiometric yields of the global growth equation, a new 6th balance is now available:

- 5 conservative C, H, O, N, Charges balances
- + **Gibbs energy balance... using $1/Y_{GX}^{\max}$ correlation**

Required information: N-source, C-source, e-donor, e-acceptor

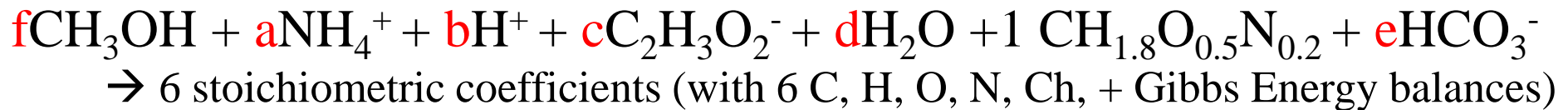
Ex: Assuming microorganism grows anaerobically on methanol as C-source and electron donor, with NH_4^+ as the N-source with Acetate production.



→ 6 balances for 6 stoichiometric coefficients !

Growth stoichiometry and q_i , Y_{ij} prediction (1)

Calculation of overall growth reaction stoichiometry: Assuming microorganism grows anaerobically on methanol as C-source and electron donor, with NH_4^+ as the N-source with acetate production.



Information:

N-source NH_4^+

C-source methanol (CH_4O , $\gamma = 6$, $\text{C}=1$)

e-donor $\text{CH}_4\text{O}/ \text{HCO}_3^-$

e-acceptor $\text{HCO}_3^-/ \text{C}_2\text{H}_3\text{O}_2^-$ (acetate)

$T = 25^\circ\text{C} = 298\text{K}$

ΔG_f^{01} [kJ.mole⁻¹]

CH_3OH -175.39

NH_4^+ -79.37

$\text{C}_2\text{H}_3\text{O}_2^-$ -369.41

H_2O -237.18

$\text{CH}_{1.8}\text{O}_{0.5}\text{N}_{0.2}$ -67

HCO_3^- -586.85

Growth stoichiometry and q_i , Y_{ij} prediction (2)

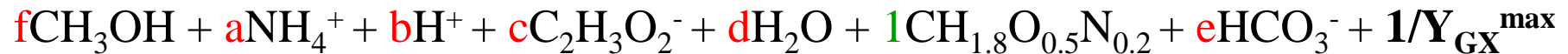
For solving stoichiometry of microbial growth:

Step 1. Calculate Gibbs energy required for growth of one C-mole of biomass using $1/Y_{GX}^{\max}$ correlation with $C=1$, $\gamma_C=6$.

$$\begin{aligned} \rightarrow 1/Y_{GX}^{\max} &= 200 + 326 + 172 \\ &= \mathbf{698} \text{ [kJ.C-mole}^{-1}\text{]} \end{aligned}$$

$$\frac{1}{Y_{GX}^{\max}} = 200 + 18 * (6 - C)^{1.8} + \exp\left\{\left[(3.8 - \gamma_C)^2\right]^{0.16} (3.6 + 0.4 * C)\right\}$$

Step 2. Calculate the stoichiometric coefficients using the 5 conservation balances (C, H, O, N, charge) + Gibbs energy balance



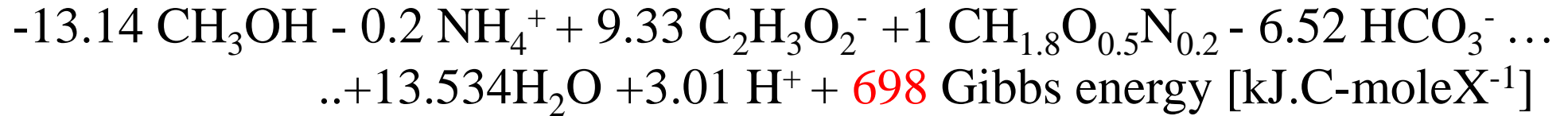
$$\text{C balance: } f+2c+1+e = 0 \quad \text{O balance: } f+2c+d+0.5+3e = 0 \quad \text{N balance: } a+0.2 = 0$$

$$\text{Charge balance: } a+ b- c- e = 0 \quad \text{H balance: } 4f+4a+b+3c+2d+1.8+e = 0$$

$$\text{Gibbs energy } (-175.39)f + (-79.37)a + (-39.87)b + (-369.41)c$$

$$\text{Balance: } +(-237.18)d + (-67)1 + (-586.85)e + \mathbf{698} = 0$$

Growth stoichiometry and q_i , Y_{ij} prediction (2)



GLOBAL GROWTH REACTION										
Electron donor couple:	CH3OH/HCO3-		C_Source:	CH3OH						
Electron acceptor couple:	HCO3-CH3COO-		N_Source:	NH4+						
Primary form:	$a.CH_3OH + b.NH_4^+ + c.CH_3COO^- + 1.C_1H_{1.8}O_{0.5}N_{0.2} + d.HCO_3^+ + e.H_2O + f.H^+ + \frac{1}{Y_{GX}^{max}} = (0)$ $-\left(1.C_1H_{1.8}O_{0.5}N_{0.2} + \frac{1}{Y_{GX}^{max}}\right) = a.CH_3OH + b.NH_4^+ + c.CH_3COO^- + d.HCO_3^+ + e.H_2O + f.H^+$									
	Biomass Production	Gibbs Energy requirement	CIH1.8OCI/YGXmax	CH3OH	NH4+	CH3COO-	HCO3-	H2O	H+	
Stoichiom. Coef.:	1	1	-(Known)	-13.1395	-0.2	9.329601	-6.51973	13.53947	3.00987	Check
C Bal:	1	0	-1	1	0	2	1	0	0	-1
H Bal:	1.8	0	-1.8	4	4	3	1	2	1	-1.8
O Bal :	0.5	0	-0.5	1	0	2	3	1	0	-0.5
N Bal :	0.2	0	-0.2	0	1	0	0	0	0	-0.2
Ch. Bal :	0	0	0	0	1	-1	-1	0	1	1.33E-15
ΔG_f^0 [kJ/mol]	-67.00	698.23	-631.231	-175.39	-79.37	-369.41	-586.85	-237.18	-39.87	-631.231
	Gamma:	CIH1.8OCI	CH3OH	NH4+	CH3COO-	HCO3-	H2O	H+		
		4.2	6	0	8	0	0	0		
	Stoichiom. Coef. :	1	-13.1395	-0.2	9.329601	-6.51973	13.53947	3.009867	Check	
	Gamma Bal.:	4.2	-78.8368	0	74.63681	0	0	0	-1.4E-14	
		$-13.14.(6) - 0.2.NH_4^+ + 9.33.(8) + 1.(4.2) - 6.52.HCO_3^- + 13.54.H_2O + 3.01.H^+ = (0)$								
Ultimate form:	$-13.14.CH_3OH - 0.2.NH_4^+ + 9.33.CH_3COO^- + 1.C_1H_{1.8}O_{0.5}N_{0.2} - 6.52.HCO_3^+ + 13.54.H_2O + 3.01.H^+ + \frac{1}{Y_{GX}^{max}} = (0)$									

Growth stoichiometry and q_i , Y_{ij} prediction (3)

Step 3. From m_G correlation

At $T=298^\circ\text{K}$, $m_G = 4.5$ [kJ.C-mole X^{-1} .h $^{-1}$]

$$m_G = 4.5 \exp\left(\frac{-69000}{R} \left(\frac{1}{T} - \frac{1}{298}\right)\right)$$

Step 4. Calculate ΔG_{cat}^{01} of catabolic reaction

Catabolic reaction:



$$\Delta G_{cat}^{01} = -1*(-175.39) - 0.5*(-586.85) + \dots + 1*(-237.18)$$

$$= -55.54 \text{ [kJ.moleS}^{-1}\text{]}$$

	ΔG_f^{01} [kJ.mole $^{-1}$]
CH ₃ OH	-175.39
NH ₄ ⁺	-79.37
C ₂ H ₃ O ₂ ⁻	-369.41
H ₂ O	-237.18
CH _{1.8} O _{0.5} N _{0.2}	-67
HCO ₃ ⁻	-586.85

Step 5. Calculate maintenance rates, m_S and other m_i

$$m_s = 4.5 / 55.54 = 0.081 \text{ [moleCH}_4\text{O.C-moleX}^{-1}\text{.h}^{-1}\text{]}$$

$$m_{\text{CO}_2} = 0.081 * 0.5 = 0.0405 \text{ [moleHCO}_3^-\text{.C-moleX}^{-1}\text{.h}^{-1}\text{]}$$

$$m_{\text{Ace}} = 0.081 * 0.75 = 0.0608 \text{ [moleAce.C-moleX}^{-1}\text{.h}^{-1}\text{]}$$

$$m_w = 0.081 * 1 = 0.081 \text{ [moleH}_2\text{O.C-moleX}^{-1}\text{.h}^{-1}\text{]}$$

$$m_{\text{H}^+} = 0.081 * 0.25 = 0.0202 \text{ [moleH}^+\text{C-moleX}^{-1}\text{.h}^{-1}\text{]}$$

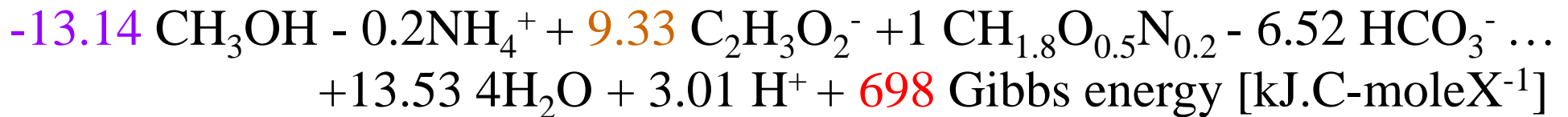
$$m_S = \frac{m_G}{-\Delta G_{cat}}$$

Growth stoichiometry and q_i , Y_{ij} prediction (4)

Step 6. Set-up linear expressions of specific rates with Herbert-Pirt Eq. (without non-catabolic product)

Global growth reaction (at μ rate):

$$-q_s = \frac{1}{Y_{SX}^{\max}} \mu + m_s$$



Catabolic reaction (at rate m_s)



Thus:

$$\text{If } m_s = 4.5 / 55.54 = 0.081 \text{ [moleCH}_4\text{O.C-moleX}^{-1}\text{.h}^{-1}\text{]}$$

$$-q_{\text{meOH}} = 13.14 \mu + 0.081 \text{ [moleCH}_4\text{O.C-moleX}^{-1}\text{.h}^{-1}\text{]}$$

$$\text{If } m_{\text{Ace}} = 0.081 * 0.75 = 0.0608 \text{ [moleAce.C-moleX}^{-1}\text{.h}^{-1}\text{]}$$

$$q_{\text{Acetate}} = 9.33 \mu + 0.0608 \text{ [moleAcetate.C-moleX}^{-1}\text{.h}^{-1}\text{]}$$

$$q_i = 1/Y_{iX}^{\max} \mu + m_i \text{ [moleC}_i\text{.C-moleX}^{-1}\text{.h}^{-1}\text{]}$$

Growth stoichiometry and q_i , Y_{ij} prediction (5)

Step 6. Linear expressions of specific rates q_i with Herbert-Pirt Eq.
 (without non-catabolic product) [$\text{moleC}_i \cdot \text{C-moleX}^{-1} \cdot \text{h}^{-1}$]

$$\begin{aligned}
 q_i &= 1/Y_{iX}^{\max} \mu + m_i & -q_{\text{NH}_4^+} &= 0.2 \mu \\
 -q_{\text{meOH}} &= 13.14 \mu + 0.081 & -q_{\text{HCO}_3^-} &= 6.52 \mu + 0.0405 \\
 q_{\text{Acetate}} &= 9.33 \mu + 0.0608 & q_{\text{H}^+} &= 3.01 \mu + 0.0202 \\
 q_{\text{H}_2\text{O}} &= 13.53 \mu + 0.081 & &
 \end{aligned}$$

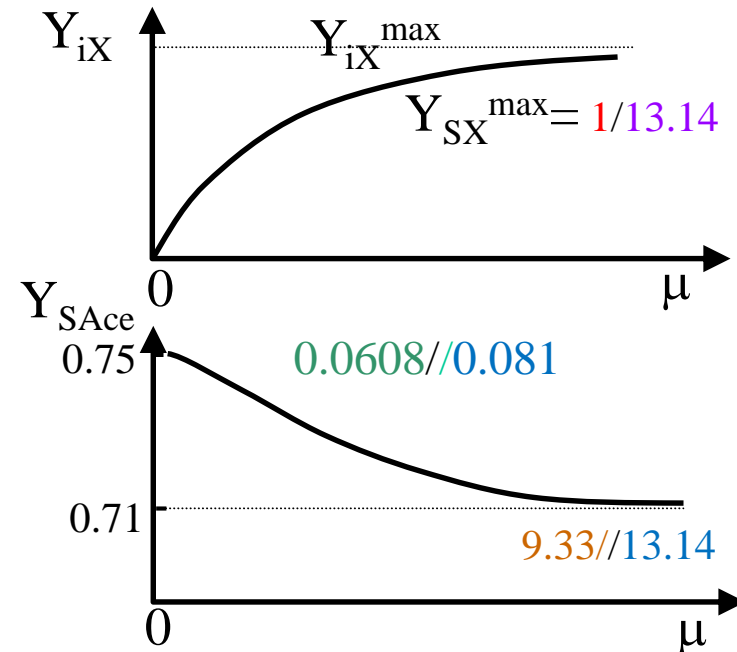
Step 7. Calculate yields Y_{ij}

Biomass yield on methanol

$$Y_{sX}(\mu) = \left| \frac{\mu}{q_s} \right| = \frac{\mu}{13.14\mu + 0.081}$$

Acetate yield on methanol

$$Y_{sAce}(\mu) = \left| \frac{q_{ace}}{q_s} \right| = \frac{9.33\mu + 0.061}{13.14\mu + 0.081}$$



→ All q_i and Y_{ij} are given and depend on only ONE unknown: μ rate!

The two Gibbs energy correlations

$1/Y_{GX}^{\max}$, m_G

$$m_G = 4.5 \exp\left(\frac{-69000}{R} \left(\frac{1}{T} - \frac{1}{298}\right)\right)$$

$$\frac{1}{Y_{GX}^{\max}} = 200 + 18 * (6 - C)^{1.8} + \exp\left\{\left[(3.8 - \gamma_c)^2\right]^{0.16} (3.6 + 0.4 * C)\right\}$$

Allows to estimate growth yields Y_{ij} and q_i for arbitrary growth system, knowing:

C_{source} , N_{source} ,

e-donor, e-acceptor,

T and **growth rate μ**

Average relative error of 13% shows pretty good predictive quality!

Strong deviation were only found for particular microbial metabolism (rare or special catabolism or anabolism)

→ μ kinetic is still required !!!

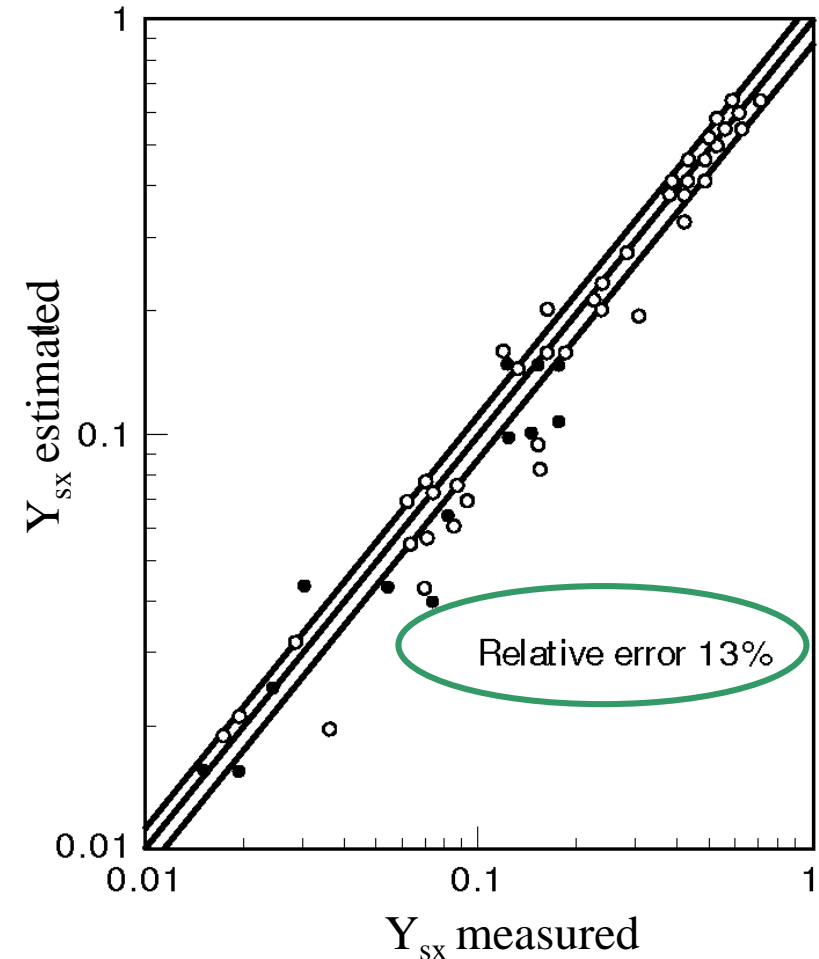


Figure 7. Comparison of measured and predicted biomass yield Y_{sx} (solid circles, fermentative; open circles, aerobic growth systems).

“ μ^{\max} or q_S^{\max} ” prediction for μ kinetic (1)

For different microorganisms, using different C-sources, e-donors, e-acceptors: $\mu^{\max} = 0.001$ to 1 h^{-1}

Recall: From Herbert-Pirt Eq. $-q_S = \frac{1}{Y_{SX}^{\max}} \mu + m_S$ Hyperbolic Eq. $q_S = q_S^{\max} \frac{C_S}{K_S + C_S}$

Thus $\mu = \left[\frac{(-q_S^{\max}) C_S}{K_S + C_S} - (m_S) \right] \cdot Y_{SX}^{\max}$ or $\mu = \mu^{\max} \frac{C_S - C_S^{\min}}{C_S + K_S}$; $C_S^{\min} = m_S K_S Y_{SX}^{\max} / \mu^{\max}$

$$-k_d = -m_S \cdot Y_{SX}^{\max}$$

And μ^{\max} is linked to q_S^{\max} and q_G^{\max} ...

$$\mu^{\max} = (q_S^{\max} - m_S) Y_{SX}^{\max}$$

$$\mu^{\max} = (q_G^{\max} - m_G) Y_{GX}^{\max}$$

→ ??? What determines μ^{\max} or q_G^{\max} ???

“ μ^{\max} or q_S^{\max} ” prediction for μ kinetic (2)

Hypothesis: ”Universal Microbial Machinery is somewhat limited”

Rate of energy production is limited to a maximum because of a maximal electron processing capacity by the electron transport chain in biomass cells, at 3 moles of electrons per C-moleX per hour (298°K)

Maximum Electron Transfer Capacity of the biomass: [e-mole.CmoleX⁻¹.h⁻¹]

$$METC = 3 \cdot \exp \left[\frac{-69000}{R} \left(\frac{1}{T} - \frac{1}{298} \right) \right]$$

METC is used for catabolism for Gibbs energy production required for growth and maintenance. The amount of electrons depends on the donor couple, γ_D , mole of electrons to be donated :

$$\gamma_D = \gamma_{Red} - \gamma_{Oxy}$$

Examples

$$C_6H_{12}O_6 / HCO_3^- \quad \gamma_D = 24 - 0 = 24$$

$$C_6H_{12}O_6 / C_2H_4O_2 \quad \gamma_D = 24 - 8 = 16$$

$$H_2S/S^0 \quad \gamma_D = 8 - 6 = 2$$

$$NH_4^+/NO_2^- \quad \gamma_D = 0 - (-6) = 6$$

“ μ^{\max} or q_S^{\max} ” prediction for μ kinetic (3)

1. Max. Electron Transfer Capacity
[e-mole.CmoleX⁻¹.h⁻¹]
2. Amount of transferred e-mole γ_D
[e-mole.moleS⁻¹]
3. Gibbs energy of catabolic reaction Δg_{cat}
[kJ.moleS⁻¹]

$$METC = 3 \cdot \exp \left[\frac{-69000}{R} \left(\frac{1}{T} - \frac{1}{298} \right) \right]$$

$$\gamma_D = \gamma_{Red} - \gamma_{Oxy}$$

→ Maximum specific Gibbs Energy production q_G^{\max} [kJ.C_moleX⁻¹.h⁻¹]

$$q_G^{\max} = \frac{3 \cdot (-\Delta G_{cat})}{\gamma_D} \exp \left(\frac{-69000}{R} \left(\frac{1}{T} - \frac{1}{298} \right) \right)$$

The specific energy rate for growth production is $q_G^{\max} - m_G$. From stoichiometry of global growth reaction: $Y_{SX}^{\max} = Y_{GX}^{\max} / Y_{GS}^{\max}$, then:

$$\mu^{\max} = (q_G^{\max} - m_G) Y_{GX}^{\max}$$

$$\mu^{\max} = (q_S^{\max} - m_S) Y_{SX}^{\max}$$

$$\text{With } Y_{SX}^{\max} = \frac{Y_{GX}^{\max}}{Y_{GS}^{\max}}$$

$$\begin{aligned} (q_G^{\max} - m_G) \cdot Y_{GX}^{\max} &= (q_G^{\max} - m_G) \cdot Y_{SX}^{\max} \cdot Y_{GS}^{\max} \\ &= (q_G^{\max} \cdot Y_{GS}^{\max} - m_G \cdot Y_{GS}^{\max}) \cdot Y_{SX}^{\max} \\ &= (q_S^{\max} - m_S) \cdot Y_{GX}^{\max} = \mu^{\max} \end{aligned}$$

“ μ^{\max} or q_S^{\max} ” prediction for μ kinetic (4)

By knowing Y_{GX}^{\max} and m_G

$$\frac{1}{Y_{GX}^{\max}} = 200 + 18 * (6 - C)^{1.8} + \exp\left\{\left[(3.8 - \gamma_c)^2\right]^{0.16} (3.6 + 0.4 * C)\right\}$$

$$m_G = 4.5 \exp\left(\frac{-69000}{R} \left(\frac{1}{T} - \frac{1}{298}\right)\right)$$

With: $\mu^{\max} = (q_G^{\max} - m_G) \cdot Y_{GX}^{\max}$

With Maximum Gibbs Energy

Capacity : $\frac{\left[\frac{\text{e-mole}}{\text{CmoleX.h}}\right] \cdot \left[\frac{\text{kJ}}{\text{moleS}}\right]}{\left[\frac{\text{e-mole}}{\text{moleS}}\right]} = \left[\frac{\text{kJ}}{\text{CmoleX.h}}\right]$

$$q_G^{\max} = \frac{3 \cdot (-\Delta G_{cat})}{\gamma_D} \exp\left(\frac{-69000}{R} \left(\frac{1}{T} - \frac{1}{298}\right)\right)$$

→ Predicted maximal specific growth rate μ^{\max} is:

$$\mu^{\max} = \left(\frac{3 \cdot (-\Delta G_{cat})}{\gamma_D} - 4.5\right) \cdot Y_{GX}^{\max} \exp\left(\frac{-69000}{R} \left(\frac{1}{T} - \frac{1}{298}\right)\right)$$

Predicted μ^{\max} (25 °C) [h⁻¹]

Glucose	Glc ,O ₂ → CO ₂ , H ₂ O	1.5	Glc → ethanol, CO ₂	0.10
Acetate	Acetate, O ₂ → CO ₂ , H ₂ O	0.7	Acetate → CH ₄ , CO ₂	0.015
CO ₂ (+RET)	NH ₄ ⁺ + O ₂ → NO ₂ ⁻	0.04		

Heat aspects in aerobic biosystems

1) Heating value of sludge (organic matter oxidation)

1 e-mole transferred (organic \rightarrow O₂) = 115 kJ

As 1 e-mole \equiv 8 gram COD \equiv 1 γ unit

Thus 1 g COD = 115/8 = **14.4 kJ**

\rightarrow 1 g biomass org. matter. = 1.366 g COD = 19.7 kJ

2) Heat production (aerobic bioprocess) $\Delta T = f(\text{BOD}) = f(Y_{\text{COD}})$

1 g consumed O₂ (BOD) \equiv **14.4 kJ** heat produced

Reactor Temperature depends on Y_{COD} of the growth

$\Delta T = 1.71 \Delta \text{COD}$ ($Y_{\text{COD}} = 0.50$) or $\Delta T = 0.86 \Delta \text{COD}$ ($Y_{\text{COD}} = 0.75$)

Where ΔCOD = Removed COD in g/L of wastewater

\rightarrow For a given substrate consumption, the worst efficient substrate for the growth, will spoil the greatest energy into heat...;-(!

Calorimetry $Q = m.C.(\Delta T)$ (with C = Specific heat capacity of water : 4.18 [J.g⁻¹.K⁻¹], 1L= 1000g of water)

$\Delta T = Q/m.C = [\text{BOD}] \times 14.4 \times 10^3 / (m.C) = [(1 - Y_{\text{COD}}) \cdot \Delta \text{COD}] \cdot 14.4 \times 10^3 / (m.C)$

$= [(1 - 0.75) \cdot \Delta \text{COD}] \times 14.4 \times 10^3 / (1000 \times 4.18) = 0.86 \cdot \Delta \text{COD}$

Heat Generation by Microbial Growth

Total rate of heat evolution in a **batch fermentation** is given [kJ.hr⁻¹] by

$$Q = V_l \cdot C_x \cdot \frac{1}{Y_{HX}} \cdot \mu$$

$1/Y_{HX}$ coming from global growth equation
 V_l is the liquid volume, C_x is biomass concentration

$$Q = V_l \cdot C_x \cdot \frac{1}{Y_{HX}} \cdot \mu = \frac{1}{Y_{HX}} \cdot [(q_x \cdot C_x) \cdot V_l] = R_H$$

In aerobic fermentations, the rate of **metabolic heat production** Q [kJ.hr⁻¹] can be roughly correlated to the **oxygen uptake rate** R_{O_2} :

$$Q = 0.12 \times R_{O_2}$$

With: Q [kcal.hr⁻¹], and R_{O_2} [mMole O₂.hr⁻¹]

→ If temperature increases above 70°C the bioprocess stops, even for thermophile growth. **Cooling becomes necessary!**

Not the case in WWTP (dilution and low organic load), but in industrial fermentation processes (Ex: Single Cell Protein processes (Yeast))

Heat Generation by Microbial Growth

Cooling: Metabolic heat released during a fermentation can be removed by circulating cooling water through a cooling coil within the fermenter, or a cooling jacket surrounding the fermenter.

- Temperature control may become a critical limitation on reactor design (particularly for scaling up)
- Ability to estimate heat removal is essential to proper reactor design

Cooling Coils



Water-Jacketed Fermenter

